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RADC-TR-75-89 Final Technical Report

April 1975



INVESTIGATION OF MICROCIRCUIT SEAL TESTING

Texas Instruments Incorporated

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The purpose of this investigation was to dete	rmine the detection ranges						

The purpose of this investigation was to determine the detection ranges of Test Conditions A, B, C, and E of Method 1014, MIL-STD-883. Also to examine test variables and modifications of the methods for possible expansion of the detection ranges, and to improve the overall test results.

This report discusses the various tests conducted and the results of these tests. In addition to the standard test conditions, various exposure pressures and times of both helium and radioisotope tracer gases are

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examined. Surface absorption, gettering materials, and controlled orifice helium testing are each examined and discussed. Also the gross leak bubble and weight gain test methods are evaluated for sensitivity and effectiveness using various pressures, pressurization times, and fluids for the purpose of optimizing test conditions and defining reject criteria.

Based on the data analysis of this testing, recommendations of leak rate limits and parameter conditions are made which will provide the highest degree of reliability in the most cost-effective manner.

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EVALUATION

The purpose of this effort was to evaluate hermeticity testing, primarily the determination of the sensitivity ranges for the helium, radioisotope, fluorocarbon bubble and weight gain test techniques of MIL-SID-683. A main objective was to establish a single test that would ensure coverage of the complete hermeticity range required for microelectronics devices used in Air Force equipment. The evaluation showed that no single test is effective over the entire fine and gross leak rate ranges for all packages. However, it did indicate for certain packages, a weight gain test will suffice.

This study utilized packages and fabricated leaks of various shapes, volumes and materials categorized by leak range to determine test conditions and sensitivities. The same test sample was used to evaluate all test procedures. The program results, detailed in this report, are considered highly successful in defining leak testing as it is known today, thereby, providing a sound technical basis for revising existing hermetic seal testing procedures. The findings and recommendations of this evaluation are useful as a whole, but in the following areas are considered significant:

- a. Tightened helium and radioisotope test reject limits.
- b. Verification of the Howl and Mann equation, using molecular flow, to define gas behavior within specified limits of leak range and package volume.
- c. Radioisotope and helium leak detection techniques are comparable if proper test conditions and equipment operation are utilized.
- d. Weight gain testing, the most effective of the gross leak test methods, is the only hermetic seal test required for packages whose internal volume is greater than 0.4cc.

In the area of leak testing at high temperature, the report results are unfavorable. However, in-house testing at RADC/RBRM indicates that a problem may exist in certain type packages. Also the data indicates that the proper gettering material could enhance test results. Therefore evaluations in these two areas will continue.

RADC, the preparing activity of MIL-STD-883, is responsible for studying and updating the microcircuit quality and reliability assurance procedures to provide reliable, accurate and cost effective test methods. Results of this effort will be factored into Methods 1014, 5004 and 5005 of MIL-STD-883.

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TABLE OF CONTENTS

Section		Title	Page
I.	INTROI	DUCTION	. 1
II.	SCREEN	NING AND FABRICATING LEAKERS	. 3
III.	EVALU	ATION OF HELIUM METHOD	. 55
IV.	EVALU.	ATION OF RADIOISOTOPE	71
V.	TEST R	ESULTS OF CONDITIONS A AND B	. 75
	1. Sen	sitivity of Test Conditions A and B	. 76
	A.	TO-84 Package (0.006 cc Internal Volume)	. 76
	В.	C-PAK (0.012 cc Internal Volume)	. 78
	C.	C-DIP (0.014 cc Internal Volume)	. 78
	D.	MOS DIP (0.041 cc Internal Volume)	. 79
	E.	TO-100 (0.086 cc Internal Volume)	. 79
	F.	Ceramic Package (0.45 cc Internal Volume)	. 80
	G.	TO-3 (1.07 cc Internal Volume)	. 81
	2. Cor	ndition A Repeatability (Table V)	. 83
	A.	TO-84	. 83
	В.	C-PAK	. 83
	C.	C-DIP	. 83
	D.	MOS DIP	. 83
	E.	TO-100	. 83
	F.	1 X 1 Ceramic	. 83
	G.	TO-3	. 84
	3. Cor	ndition B Repeatability (Table X)	. 84
	A.	TO-84	. 84
	В.	C-PAK	. 84
	C.	C-DIP	. 84
	D.	MOS DIP	. 84
	E.	TO-100	. 85
	F.	1 X 1 Ceramic	. 85
	G.	TO-3	. 85
VI.	SURFAC	CE ABSORPTION	. 87
VII.	TEMPEI	RATURE PRECONDITIONING	. 89
VIII.	GETTEI	RING EVALUATION	. 91
IX.	CONTRO	OLLED ORIFICE EVALUATION	. 95
X.	INTROD	DUCTION TO GROSS LEAK TEST CONDITIONS C AND E	. 97
XI.	EVALU	ATION OF TEST CONDITION C	. 99

TABLE OF CONTENTS (Continued)

Section	T	itle															Page
XII.	EVALUATION OF CONDITION E			•													107
XIII.	SUMMARY											•		•			115
XiV.	RECOMMENDATIONS		•	•	•	•	•	•	•	٠	•	•	•		•	•	121
APPENE	DIX																
	MICROCIRCUIT SEAL TESTING DA	TA.															123

LIST OF ILLUSTRATIONS

Figure	Title	Page
1.	Fluid Flow versus Leak Rate	. 4
2	Examples of MOS Dual In-Line Device, Large Volume Glass Standard Sample,	
	and Small Volume Glass Standard Sample	. 8
3.	TO-84 Time/Pressure Sequence-Bomb Pressure = 30 psig	. 10
4.	TO-84 Time/Pressure Sequence-Bomb Pressure = 45 psig	. 11
5.	TO-84 Time/Pressure Sequence-Bomb Pressure = 60 psig	. 12
6.	TO-84 Time/Pressure Sequence-Bomb Pressure = 75 psig	. 13
7.	TO-84 Time/Pressure Sequence-Bomb Pressure = 90 psig	. 14
8.	C-PAK Time/Pressure Sequence-Bomb Pressure = 30 psig	. 15
9.	C-PAK Time/Pressure Sequence-Bomb Pressure = 45 psig	. 16
10.	C-PAK Time/Pressure Sequence-Bomb Pressure = 60 psig	. 17
11.	C-PAK Time/Pressure Sequence-Bomb Pressure = 75 psig	. 18
12.	C-PAK Time/Pressure Sequence-Bomb Pressure = 90 psig	. 19
13.	C-DIP Time/Pressure Sequence-Bomb Pressure = 30 psig	. 20
14.	C-DIP Time/Pressure Sequence-Bomb Pressure = 45 psig	. 21
15.	C-DIP Time/Pressure Sequence-Bomb Pressure = 60 psig	. 22
16.	C-DIP Time/Pressure Sequence-Bomb Pressure = 75 psig	. 23
17.	C-DIP Time/Pressure Sequence-Bomb Pressure = 90 psig	. 24
18.	MOS DIP Time/Pressure Sequence-Bomb Pressure = 30 psig	. 25
19.	MOS DIF Time/Pressure Sequence-Bomb Pressure = 45 psig	. 26
20.	MOS DIP Time/Pressure Sequence-Bomb Pressure = 60 psig	. 27
21.	MCS DIP Time/Pressure Sequence-Bomb Pressure = 75 psig	. 28
22.	MOS DIP Time/Pressure Sequence-Bomb Pressure = 90 psig	. 29
23.	TO-100 Time/Pressure Sequence-Bomb Pressure = 30 psig	. 30
24.	TO-100 Time/Pressure Sequence-Bomb Pressure = 45 psig	. 31
25.	TO-100 Time/Pressure Sequence-Bomb Pressure = 60 psig	
26.	TO-100 Time/Pressure Sequence-Bomb Pressure = 75 psig	. 33
27.	TO-100 Time/Pressure Sequence-Bornb Pressure = 90 psig	. 34
28.	1 X 1 Ceramic Time/Pressure Sequence-Bomb Pressure = 30 psig	. 35
29.	1 X 1 Ceramic Time/Pressure Sequence-Bomb Pressure = 45 psig	. 36
30.	1 X 1 Ceramic Time/Pressure Sequence-Bomb Pressure = 60 psig	. 37
31.	1 X 1 Ceramic Time/Pressure Sequence-Bomb Pressure = 75 psig	. 38
32.	1 X 1 Ceramic Time/Pressure Sequence-Bomb Pressure = 90 psig	. 39
33.	TO-3 Time/Pressure Sequence-Bomb Pressure = 30 psig	. 40
34.	TO-3 Time/Pressure Sequence-Bomb Pressure = 45 psig	. 41
35.	TO-3 Time/Pressure Sequence-Bomb Pressure = 60 psig	. 42

LIST OF ILLUSTRATIONS (Continued)

Figure	Title	Page
36.	TO-3 Time/Pressure Sequence-Bomb Pressure = 75 psig	43
37.	TO-3 Time/Pressure Sequence-Bomb Pressure = 90 psig	. 44
38.	Large Glass Time/Pressure Sequence-Bomb Pressure = 30 psig	45
39.	Large Glass Time/Pressure Sequence-Bomb Pressure = 45 psig	46
40.	Large Glass Time/Pressure Sequence-Bomb Pressure = 60 psig	. 47
41.	Large Glass Time/Pressure Sequence-Bomb Pressure = 75 psig	. 48
42.	Large Glass Time/Pressure Sequence-Bomb Pressure = 90 psig	. 49
43.	Small Glass Time/Pressure Sequence-Bomb Pressure = 30 psig	50
44.	Small Glass Time/Pressure Sequence-Bomb Pressure = 45 psig	51
45.	Small Glass Time/Pressure Sequence-Bomb Pressure = 60 psig	52
46.	Small Glass Time/Pressure Sequence-Bomb Pressure = 75 psig	53
47.	Small Glass Time/Pressure Sequence-Bomb Pressure = 90 psig	54
48.	Effects of Pressure Increase for 0.01 cc Volume	57
49.	Effects of Pressure Increase for 0.10 cc Volume	58
50.	Effects of Pressure Increase for 1.00 cc Volume	59
51.	Effects of Pressure Increase for 10.00 cc Volume	60
52.	Effects of Time Out of Bomb on Indicated Leak	61
53.	R Values versus Calculated L Values	62
54.	Typical Decay Rates	63
55.	Graphical Comparisons of (a) Volume Changes, (b) Pressure Changes,	
	(c) Bomb Time Changes, and (d) Readout Time Changes of the	
	Helium Leak Rate Formula	64
56.	Temperature and Leak Rates	90
57.	Block Diagram of Controlled Orifice Test Setup	95

LIST OF TABLES

Table	Title .	Page
I.	RADC Microcircuit Leak Rate Values	. 5
II.	Calculated Internal Volume of Typical Devices	. 7
III.	Helium Time Pressure Matrix	. 55
IV.	Helium Evaluation - Number of Rejects at Test Conditions	. 66
V.	Test Condition A Repeatability	. 67
VI.	MS-90 UFT - Device Preconditioning	. 68
VII.	MS-90 UFT Helium Evaluation — Number of Rejects	
	$R > 5 \times 10^{-8}$ and 5×10^{-7}	. 69
VIII.	Krypton-85 Matrix	. 71
IX.	Radioisotope Test Results - Number of Units Detected as Rejects	. 72
X.	Test Condition B Repeatability	. 74
XI.	Comparison of Rejects Detected by Test Condition A	
	and Test Condition B, using a Common Baseline	
	Q and L > 5 X 10^{-7} for volume ≤ 0.1 cc	
	Q and L > 5 X 10^{-6} for volume > 0.1 cc	. 75
XII.	Rejects per Failure Criteria of MIL-STD-883, Condition A	
	and Condition B	. 76
XIII.	Test Conditions A and B, Overkill and Escape Rates	
	When L and Q = 5 X 10^{-7} on Volumes of <0.1 cc	
	and 5 X 10^{-6} on Volumes > 0.1 cc	. 77
XIV.	Surface Absorption on 1 X 1 Ceramic Lids with Epoxy Sealant	
	(All Data X 10 ⁻⁸ atm cc/sec)	. 80
XV.	Test Condition Limits Required to Achieve Minimum Escape Rates	. 82
XVI.	Overkill and Escape Rates with Getters Using Helium	. 91
XVII.	Overkill and Escape Rates with Getters Using Krypton-85	. 92
XVIII.	Overkill and Escape Rates Using Controlled Orifice Helium Testing	. 90
XIX.	RADC Microcircuit Leak Rate Values (Condition C and E)	. 98
XX.	C ₁ Escape and Overkill Rates in FC-40 and PP-9	. 100
XXI.	Comparison of FC-40 and PP-9 on Total Sample Population	. 101
XXII.	C ₁ Gross Leak Repeatability	. 102
XXIII.	C ₂ Escapes and Overkill Rates in FC-78/FC-40 and PP-1/PP-9	. 104
XXIV.	C_2 Gross Leak Repeatability	. 105
XXV.	Comparison of Test Fluids FC-78/FC-40 and PP-1/PP-9	. 105
XXVI.	Comparison of Fluids at 60 psig with a Reject Limit	
	Equal to L of 2 X 10^{-6} which is 4.8 Mg Gain	. 110
XXVII.	Escape and Overkill Rates at Varying Pressures and Limits, TO-84	. 110

LIST OF TABLES (Continued)

Table	Title	Page
	Escape and Overkill Rates at Varying Pressures and Limits, C-PAK	110
XXVIII.	Escape and Overkill Rates at valying Hessares and Limits, CDIP	111
XXIX.	Escape and Overkill Rates at Varying Pressures and Limits, C-DIP	111
XXX.	Escape and Overkill Rates at Varying Pressures and Limits, MOS DIP	111
XXXI.	Facane and Overkill Rates at Varying Pressures and Limits, TO-100	111
	Escape Rates at Varying Pressures and Limits, 1 X 1 Ceramic	112
XXXII.	Escape and Overkill Rates at Varying Pressures and Limits, TO-3	112
XXXIII.	Escape and Overkill Rates at Varying Pressures and Limits, Class	112
XXXIV.	Escape and Overkill Rates at Varying Pressures and Limits, Glass	113
XXXV.	Weight Gain, Escape and Overkill Rates at Fill Rate and Optimum Limits	113
XXXVI.	Comparison of Results at 90 psig With Vacuum and 105 psig	
712171 7 1.	Without Vacuum	. 114
xxxvii.	Fine-Leak Testing Followed by Gross-Leak Testing	. 119

SECTION I

INTRODUCTION

This investigation was conducted under Rome Air Development Center Contract No. F30602-73-C-0150 to determine the sensitivity ranges of Conditions A, B, and C of Method 1014 and proposed Condition E to determine if the ranges could be extended by changes in test parameters or preconditioning of the test devices.

Seven microcircuit package types were screened to secure devices having leak rates ranging from $>10^{-3}$ $<10^{-8}$ atmospheric cm³ per second. The leak rates were confirmed by Test Conditions A and B and by a weight gain technique.

All the test samples were subjected to a matrix of test times and pressures in helium and measured with mass spectrometers. Veeco Model MS-12 and MS-90 UFT machines were used to determine if pump-down rates had significant effects on the resultant data. Test times ranged from 2 to 8 hours and pressures from 30 to 90 psig. Curves were constructed for each package at each test condition utilizing the formula in Method 1014 of MIL-STD-883. This permitted the formula to be tested for validity and if valid, provided a base for testing the effects of the various conditions.

All the test samples were then subjected to a matrix of test conditions utilizing radioisotope techniques. Tests were conducted with zero, one, and three wash cycles and with three levels of specific activity: 277, 600, and 1397 microcuries per cm³. IsoVac Mark IV and CEC 24-510 machines were used for this part of the investigation. Tests were conducted at three different storage pressure levels to determine possible effects on the results.

Helium tests were then conducted utilizing a controlled orifice to determine if such a method would extend Test Condition A to cover the gross leak range. Special fixtures were fabricated to permit each device to be tested for gross leak, then immediately for fine leak.

Temperature preconditioning was also evaluated using both helium and radioisotope conditions. Two packages, one metal and one ceramic, were pressurized while maintaining temperatures of 50°C, 75°C, 100°C, and 125°C. The devices were read immediately upon removal from pressurization in each case.

Pre-encapsulated polyimide as well as bombed-in fluorocarbons (FC-48 and PP-9) and vacuum pump oil were tested as possible gettering materials. This was to determine if either the helium or radioisotope range could be extended to cover the entire gross leak range.

Case and sealing materials were also evaluated to determine their gettering characteristics for either helium or krypton-85. This portion of the study was performed to learn whether or not acceptable devices were being rejected in some cases because of the absorption ability of these materials.

 C_1 bubble test was conducted on all test samples using FC-40 and PP-9 to evaluate the fluids, repeatability of the test, and sensitivity of the test.

C₂ bubble test was performed on all test samples using FC-78/FC-40 and PP-1/PP-9 fluid combinations. This was to determin. the best fluid combination, sensitivity, and repeatability of the condition.

All the test samples were subjected to a series of weight gain tests. Tests were conducted on each package type using FC-77, FC-78, PP-1, and PP-2 as the indicator fluid. This was to determine if all the fluids were acceptable and if not, which was the best. Each package type was subjected to a test at 30, 60, and 90 psig to determine possible effect upon the results. The condition was also evaluated to determine if the vacuum step is necessary.

SECTION II

SCREENING AND FABRICATING LEAKERS

Phase I of the project was devoted to selection of samples from production line hermetic seal rejects and fabrication of glass "standard leakers." The test devices were first categorized into leak-range decades utilizing the radioisotope technique of Condition B, Method 1014 of MIL-STD-883. This technique provided device categories of 10^{-8} , 10^{-7} , 10^{-6} , and $>10^{-6}$ atm cc,'s and "nonleakers." Condition B resulted in some gross leakers being detected as fine leaker and therefore being grouped in the fine-leak ranges. The ">10^{-6}" and "nonleaker" categories were then subjected to an FC-75 weight gain test utilizing the fluid fill rate data published by Ray theon in "Ray theon Weight Test Method for Detecting Gross Leaks in Small Internal Volume Semiconductor Packages." The Ray theon data has been verified by Texas Instruments (Figure 1). This method provided leak-range classifications of 10^{-5} , 10^{-4} , and $>10^{-3}$ atm cc/s. Each test device was then assigned a serial number and grouped as shown in Table I.

Glass "standard leakers" were fabricated by drawing glass tubing down into orifice sizes. The "standard leakers" were fabricated from thin-wall and thick-wall glass tubing of 1/4 inch O.D. The procedure for fabricating the thin-wall tubing was as follows:

The tubing was cut into 6-inch lengths and heated with a torch, a distance 2 inches from one end until the tubing was soft.

The tubing was then pulled so as to cause the tubing to "neck down" and separate. The pull rate was controlled so as to produce a neck 1/2- to 3/4-inch long with an orifice of varying size. There is no control on the size of orifice produced in this manner; therefore, several units were required to produce one acceptable unit.

The units were then connected to a dry nitrogen supply with a controlled pressure that could be varied from 0 to 100 psig. The orifice end was submerged in isopropanol and the pressure inside the unit increased until the pressure required to initiate bubbling was obtained. This pressure was recorded and used to determine the leak rate.

The open ends of the units were then heated with a torch and sealed approximately one inch from the neck. The open end which extended beyond the seal was cut off and discarded.

*Pyrex glass

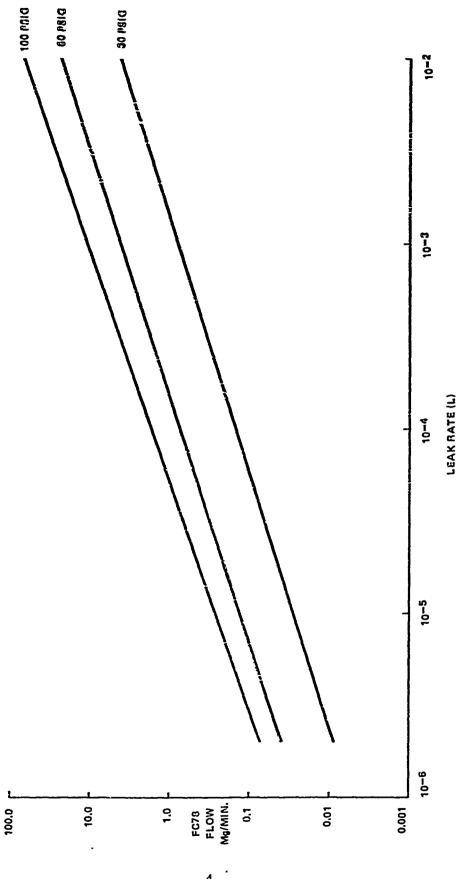


Figure 1. Fluid Flow versus Leak Rate

mention with the state of the s

Table I. RADC Microcircuit Leak Rate Values

No. Leak Rate Units SN Leak Rate Units SN Leak Rate	Nc. Units 11 12 20 15 15 18 9	5N 1-11 12-24 25-44 45-59 60-74 75-93 93-102					
Leak Race Units SN Leak Rate Units SN Leak Rate Nordeakers 10 40-49 Nordeakers 10 1-10 Nordeakers 10 ⁻⁸ 5 1-9 10 ⁻⁸ 14 11-24 10 ⁻⁸ 10 ⁻⁷ 12 10-21 10 ⁻⁷ 20 25-44 10 ⁻⁷ 10 ⁻⁶ 18 22-39 10 ⁻⁶ 12 45-57 10 ⁻⁶ 10 ⁻⁵ 15 50-64 10 ⁻⁵ 12 58-79 10 ⁻⁵ 10 ⁻⁴ 7 65-71 10 ⁻⁴ 14 71-84 10 ⁻⁴ >10 ⁻³ 29 72-99 >10 ⁻³ 19 85-103 >10 ⁻³	11 12 20 15 15 18 9	1-11 12-24 25-44 45-59 60-74 75-93					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	12 20 15 15 18	12-24 25-44 45-59 60-74 75-93					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20 15 15 18 9	25-44 45-59 60-74 75-93					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	15 15 18 9	45-59 60-74 75-93					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	15 18 9	60-74 75-93					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	18 9.	75-93					
>10 ⁻³ 29 72-99 >10 ⁻³ 19 85-103 >10 ⁻³	9.						
		93-102					
Total 100 Total 103 Total	102						
		i i					
24 by 24 All Ceramic with Gettering (C-PAK) MOS Dual In-Line (MOS DIP) Ceramic 1	Ceramic 1 Inch by 1 Inch						
No. No.	No.	T					
Leak Rate Units SN Leak Rate Units SN Leak Rate	Units	SN					
Nonleakers 12 1-12 Nonleakers 10 1-10 Nonleakers							
10 ⁻⁸ 12 13-24 10 ⁻⁸ 15 11-25 10 ⁻⁸							
10 ⁻⁷ 21 25-45 10 ⁻⁷ 18 26-43 10 ⁻⁷							
10 ⁻⁶ !5 46-60 10 ⁻⁶ 7 44-50 10 ⁻⁶	71	1-71					
10 ⁻⁵ 6 61-66 10 ⁻⁵ 23 51-73 10 ⁻⁵							
10 ⁻⁴ 8 94-101 10 ⁻⁴ 6 74-79 10 ⁻⁴							
>10 ⁻³ 27 67.93 >10 ⁻³ 22 80.101 >10 ⁻³	Units d	id not fit					
Total 101 Total 101	distribu	ıticı.					
	½ by ¼ All Ceramic (C-PAK)						
No. No. Units		SN					
	10 9	8-107					
10 ⁻⁸ 15 1-15 10 ⁻⁷ 4 1-4 10 ⁻⁸	8 9	0.97					
	19 7	11-89					
1	16 6	55- 7 0					
	6 53-54; 110-						
10 ⁻⁴ 19 96-115 >10 ⁻³ 11 40-51 10 ⁻⁴ 2	20 3	33 52					
>10 ⁻³ 6 20.25 >10 ⁻³ 3	32	1-32					
Total 101 Total 17 34 Total 11	13						

The thick wall units were produced as follows:

The tubing was cut into 6-inch lengths and the heat applied with a torch to the end of the tubing. The units were slowly rotated while being heated, causing the tubing to shrink until the inside diameter was of the desired size.

The units were then checked for bubbling in the same manner as the thin-wall units. If the unit did not produce the desired value, it was reheated and checked again.

After obtaining the desired value, the units were sealed by heating the tubing and twisting so as to seal the unit 1 inch from the orifice end. The open end which extended beyond the seal was cut off.

The thin-wall leakers produced by this method were classed as large-volume units and the thick-wall units were classed as small-volume units.

The leak sizes were then verified by helium mass spectrometer techniques. After sealing, the fine leakers were further verified by Test Condition A, Meth 1914, MIL-STD-883 and the gross leakers by the weight gain techniques. The categories fabrical are included in Table I.

Effort was also devoted to the evaluation of laser drilling as a means of creating microelectronic package leakers of specific leak rates. The laser is controlled by a Texas Instruments 960A computer which controls the beam diameter as well as the number of pulses. The application of this laser does not require as close a tolerance on the beam diameter as would be required to drill deep holes with very small diameters. Two types of material and package types were used during this investigation: the TO-100 which is metal, and the 1 X 1 ceramic.

The laser would penetrate the TO-100 packages; however, the beam could not be focused to produce a hole smaller than 0.015 inch in diameter. It was felt that since the energy of the LASER beam was not uniform over the entire beam spot, that if the correct number of pulses were applied, the "hot spots" would burn through, producing a much smaller hole. Due to the tolerance of the material thickness and the lack of precise control of the laser beam, this could not be achieved. The large 1 inch by 1 inch ceramic packages obtained from the production lines were nonleakers. An attempt was made to create leakers by using the laser drill. The ceramic was so thick that after drilling half way through the material, the beam was adjusted so as to penetrate the material. This produced a hole 0.015 inch in diameter which was considered too large for use in this study. It can be concluded that for laser drilling to be effective in producing standard leakers, that the laser should be designed to drill deep holes and maintain control on the diameter of the beam to within 0.5 micrometers. Since the fabrication of leakers from glass tubing had proved to be a successful and controlleble process, further attempts at laser drilling were not made.

The internal volume of the devices was calculated by opening each package and measuring the internal dimensions. The measurements were made using a microscope with a scale scribed on the lens. The calculations were verified by drilling a small hole in the package and filling the unit with FC-78. The volume of FC-78 was determined by measuring the weight gained by the device. This information is included in Table II.

Table II. Calculated Internal Volume of Typical Devices

Package	Volume
TO-84	0.0060 cc
1/4 by 1/4 All Ceramic (C-PAK)	0.0120 cc
Ceramic Dual In-Line (C-DIP)	0.0145 cc
*MOS Dual In-Line	0.0412 cc
TO-100	0.0858 cc
Ceramic 1 Inch by 1 Inch	0.4475 cc
TO-3	1.0712 cc
*Large Volume Glass Standard	1.3100 cc
*Small Volume Glass Standard	0.0320 cc

^{*}See Figure 2

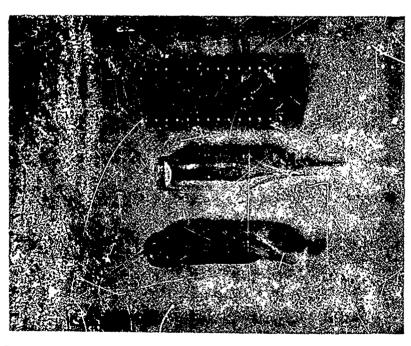


Figure 2. Fxamples of MOS Dual In-Line Device, Large Volume Glass Standard Sample, and Small Volume Glass Standard Sample

Prior to initiation of evaluation of the test methods, each device's leak rate was measured by radioisotope and helium techniques. The leak rate in terms of Q_s for the radioisotope technique and R for the helium technique was recorded. The R value was converted to L value using the graphs (Figures 3 through 47) and the gross leak data. The gross leak data was used to indicate that the device was on the portion of the curve that indicated a leak rate greater than the spectrometer was able to detect due to gas escape rate. Pressurization values and bomb times were determined by the equations below. The reject criteria for comparison purposes were based upon calculated leak rates (L, Q) of 5 X 10^{-7} to provide a common data baseline.

Helium equation:

$$R_1 = \frac{LP_E}{P_O} \left(\frac{M_A}{M}\right)^{1/2} \left\{ 1 - e^{-\left[\frac{Lt_1}{VP_O} \left(\frac{M_A}{M}\right)^{1/2}\right]} \right\} e^{-\left[\frac{Lt_2}{VP_O} \left(\frac{M_A}{M}\right)^{1/2}\right]}$$
(1)

where

 R_1 = the measured leak rate of tracer gas (He) through the leak in atm cc/s

L = the equivalent standard leak rate in atm cc/s

P_E = the pressure of exposure in atmospheres absolute

 P_0 = the atmospheric pressure in atmospheres absolute (1)

 M_A = the molecular weight of air in grams (28.7)

M = the molecular weight of the tracer gas (He) in grams (4)

 t_1 = the time of exposure to P_F , in seconds

t₂ = the dwell time between release of pressure and leak detection, in seconds

V = the internal volume of the device package cavity in cubic centin eters

Radioisotope equation:

$$Q_{S} = \frac{R}{SKTPt}$$
 (2)

The parameters of Equation (2) are defined as follows:

- Q_s = The maximum leak rate allowable, in atm cc/s, for the devices to be tested.
- R = Counts per minute above the ambient background after activation if the device leak rate were exactly equal to Q_s .
- s = The specific activity, in microcuries per atmosphere cm³, of the Krypton-85 tracer gas in the activation system.
- k = The overall counting efficiency of the scintillation crystal in counts per minute per microcurie of Krypton-85 in the internal void of the specific component being evaluated.

This factor depends upon component configuration and dimensions of the scintillation crystal.

- T = Soak time, in hours, that the devices are to be activated.
- $\overline{P} = P_e^2 P_i^2$, where P_e is the activation pressure in atmospheres absolute and P_i is the original internal pressure of the devices in atmospheres absolute. The activation pressure (P_e) may be established by specification or if a convenient soak time (T) has been established, the activation pressure (P_e) can be adjusted to satisfy Equation (2).
- t = Conversion of hours to seconds and is equal to 3600 seconds per hour.

Applying the parameters defined by solution of Equation (2), the actual leak rate of the device can be calculated as follows:

$$Q = \frac{\text{(Actual Readout in Net Counts Per Minute) X } Q_s}{R}$$
 (3)

where Q = actual leak rate of the device, Q_s and R are as defined above.

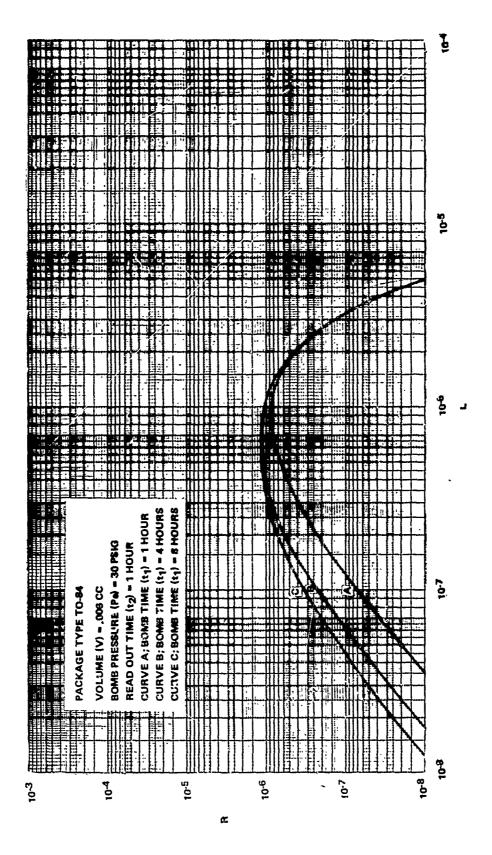


Figure 3. TO-84 Time/Pressure Sequence-Bomb Pressure = 30 psig

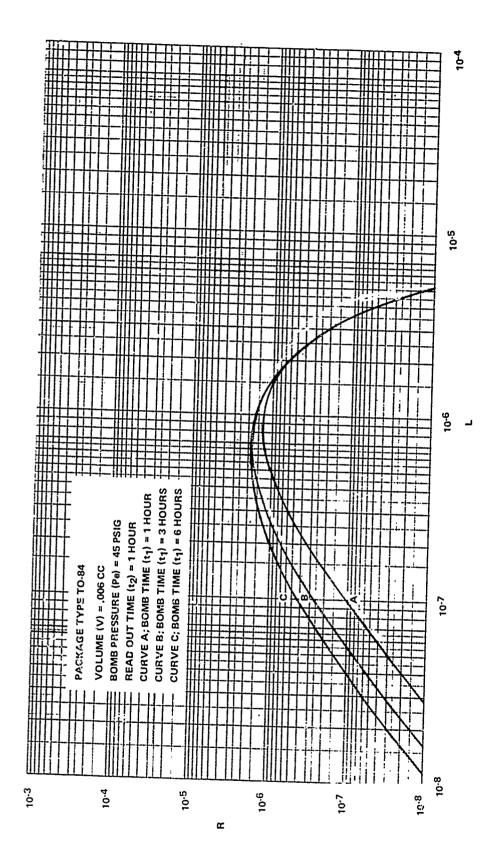


Figure 4. TO-84 Time/Pressure Sequence-Bomb Pressure = 45 psig

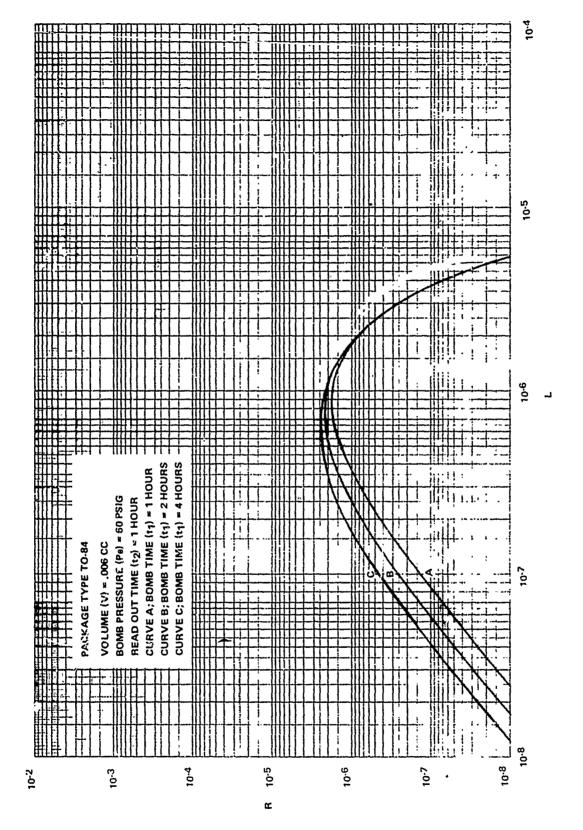
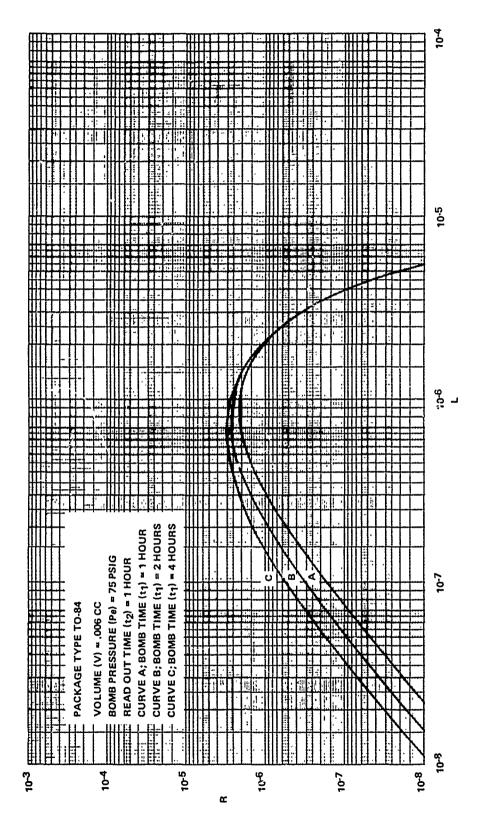


Figure 5. TO-84 Time/Pressure Sequence-Bomb Pressure = 60 psig



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Figure 6. TO-84 Time/Pressure Sequence-Bomb Pressure = 75 psig

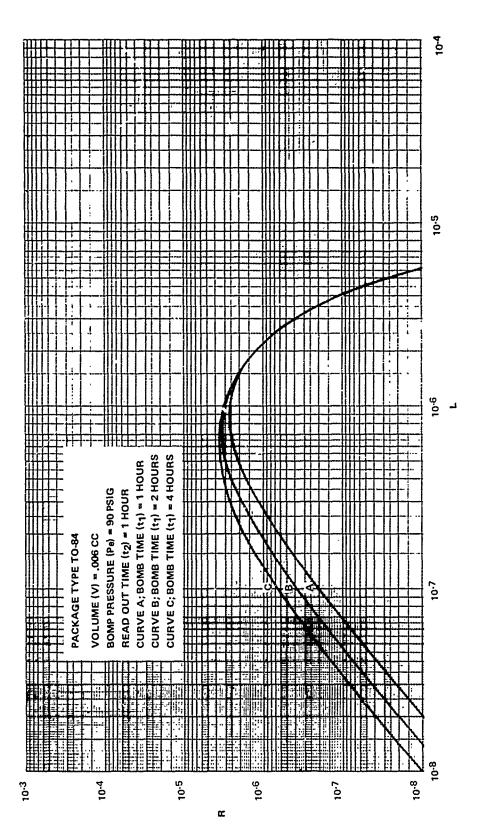


Figure 7. TO-84 Time/Pressure Sequence-Bomb Pressure = 90 psig

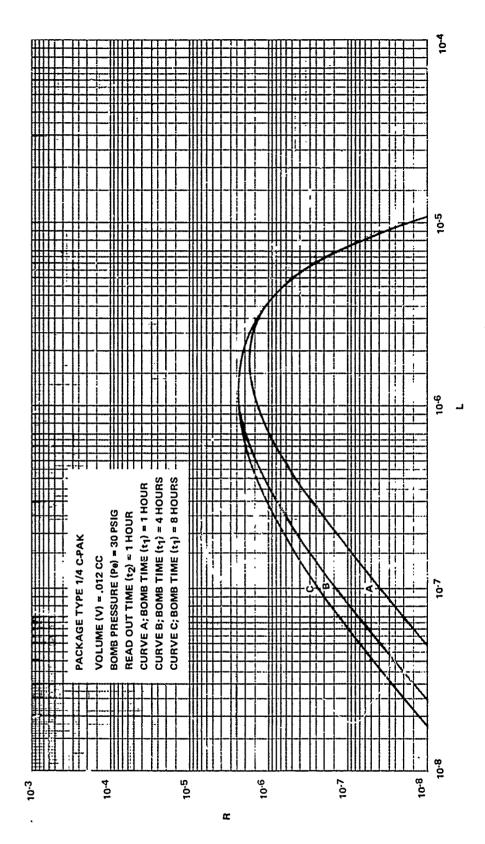


Figure 8. C-PAK Time/Fressure Sequence-Bomb Pressure = 30 psig

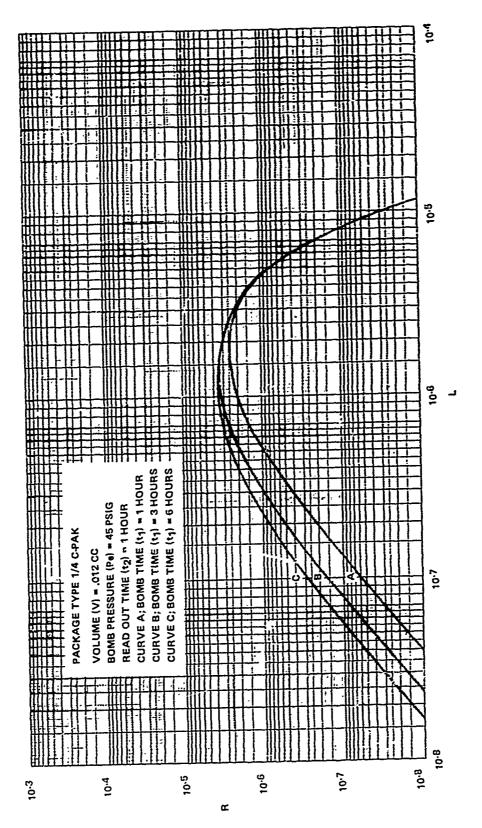


Figure 9. C-PAK Time/Pressure Sequence-Bomb Pressure = 45 psig

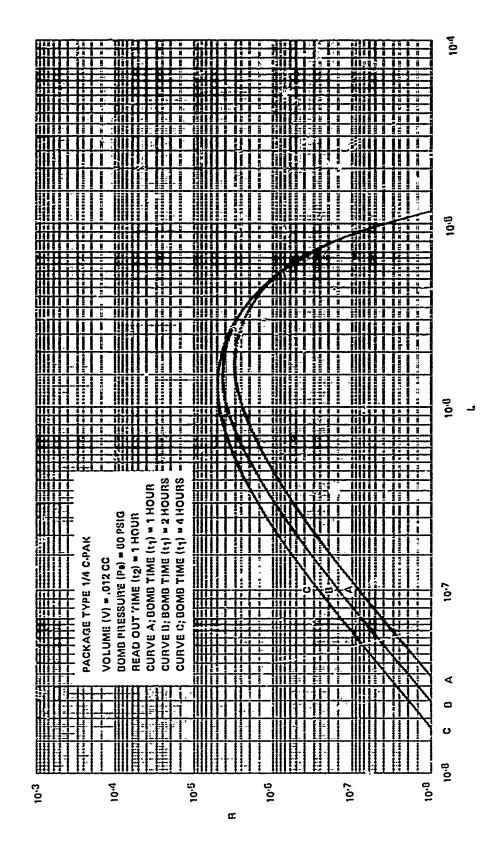


Figure 10. C-PAK Time/Pressure Sequence-Bomb Pressure # 60 pslg

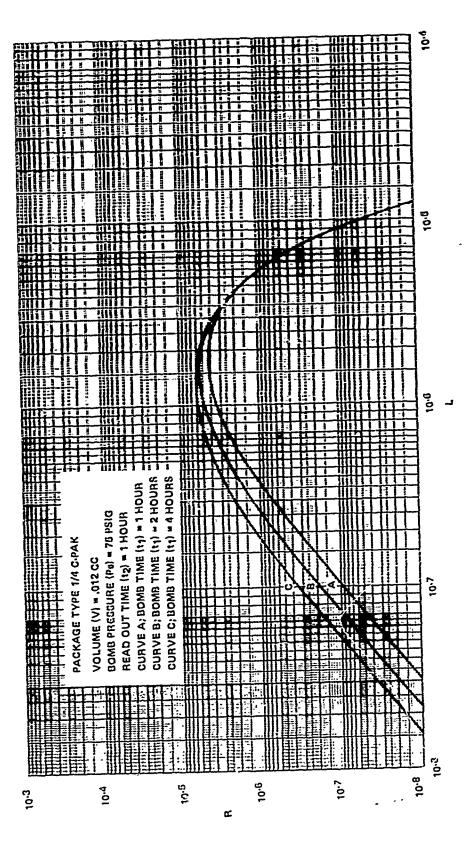


Figure 11. C-PAK Time/Pressure Sequence-Bomb Pressure = 75 psig

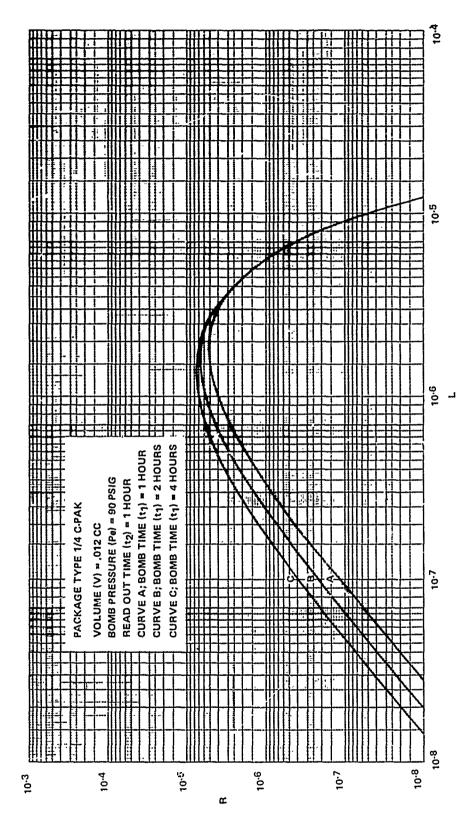


Figure 12. C-PAK Time/Pressure Sequence-Bomb Pressure = 90 psig

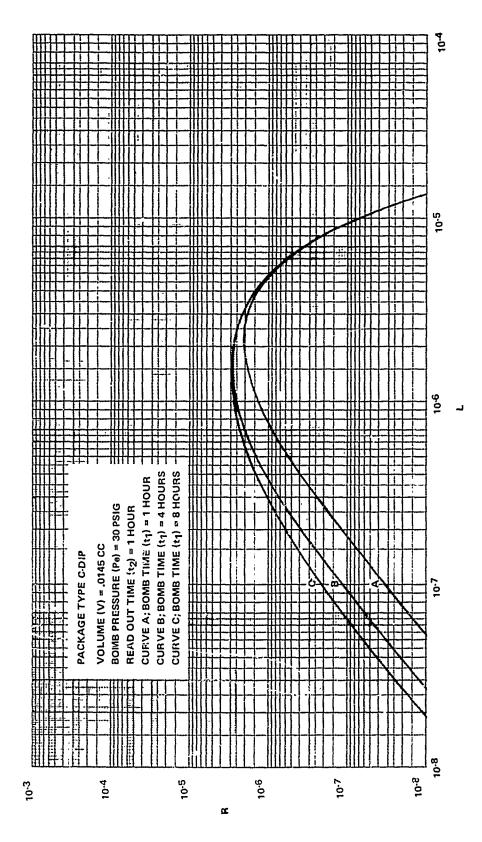


Figure 13. C-CIP Time/Pressure Sequence-Bomb Pressure = 30 psig

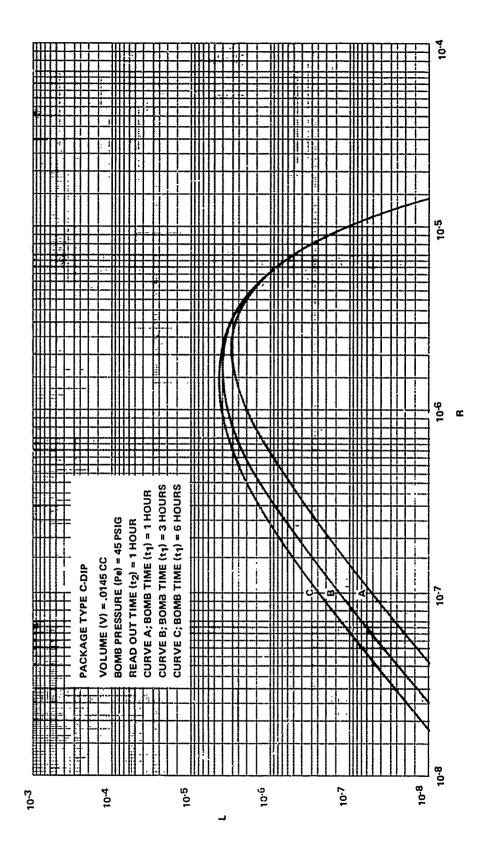


Figure 14. C-DIP Time/Pressure Sequence-Bomb Pressure = 45 psig

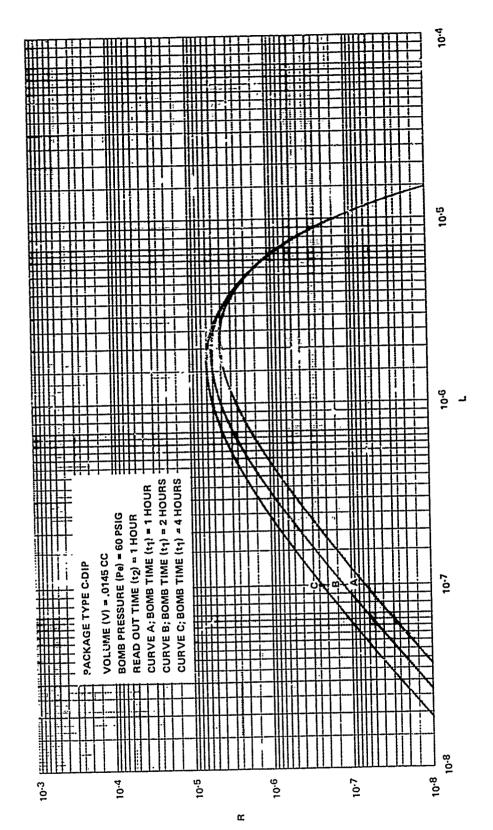


Figure 15. C-DIP Time/Pressure Sequence-Bomb Pressure = 60 psig

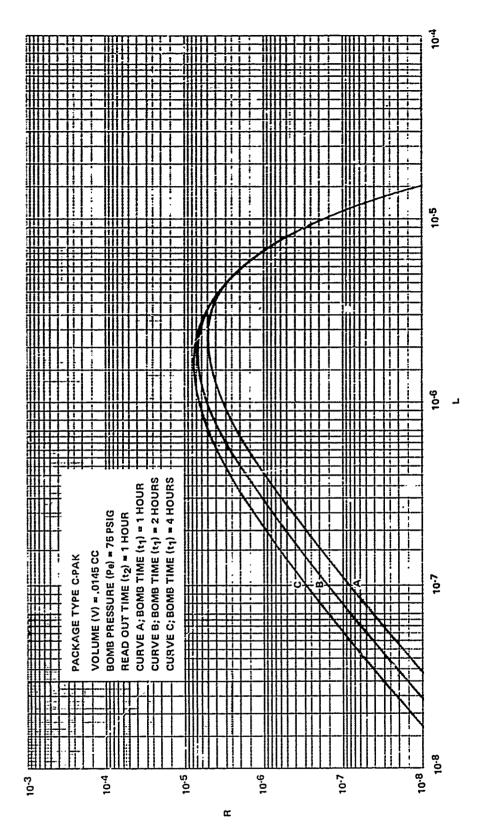


Figure 16. C-DIP Time/Pressure Sequence-Bomb Pressure = 75 psig

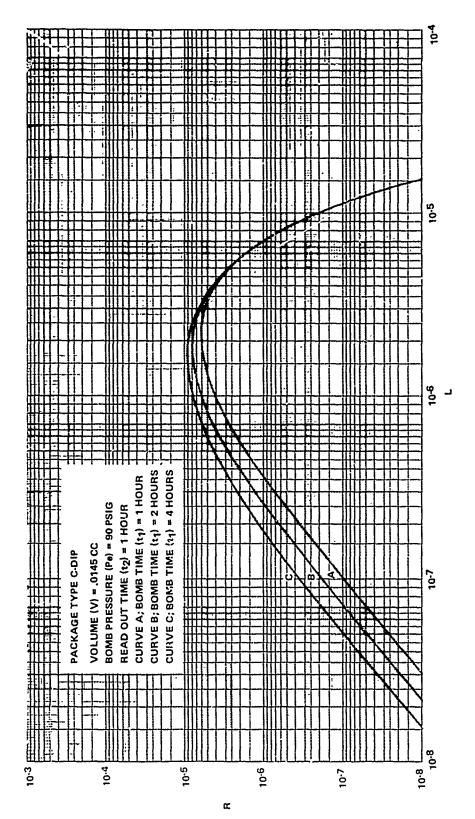


Figure 17. C-DIP Time/Pressure Sequence-Bomb Pressure = 90 psig

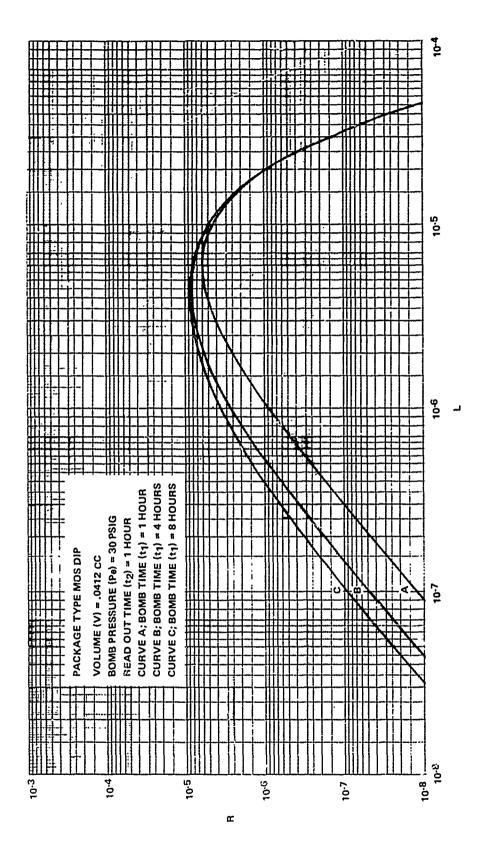


Figure 18. MOS DIP Time/Pressure Sequence-Bomb Pressure = 30 psig

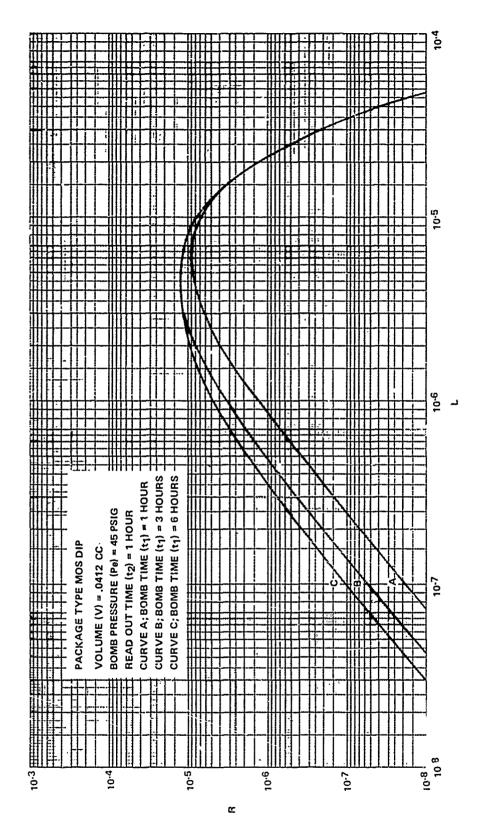
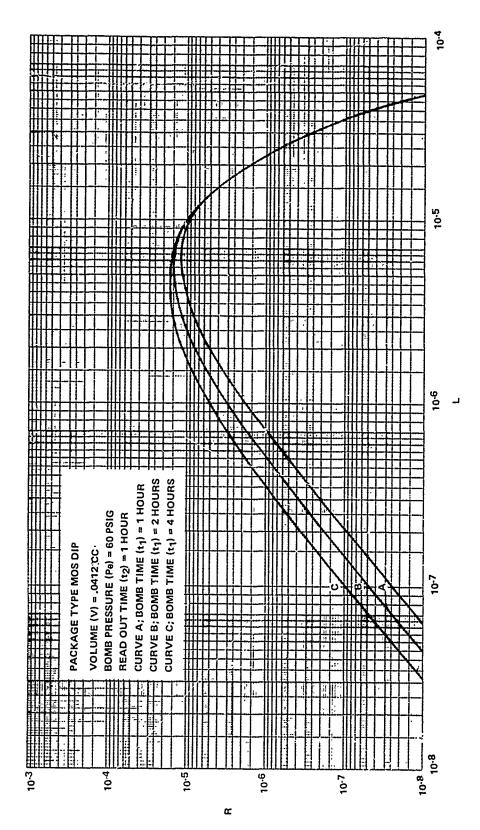


Figure 19. MOS DIP Tinne/Pressure Sequence-Bomb Pressure = 45 psig



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Figure 20. MOS DIP Time/Pressure Sequence-Bomb Pressure = 60 psig

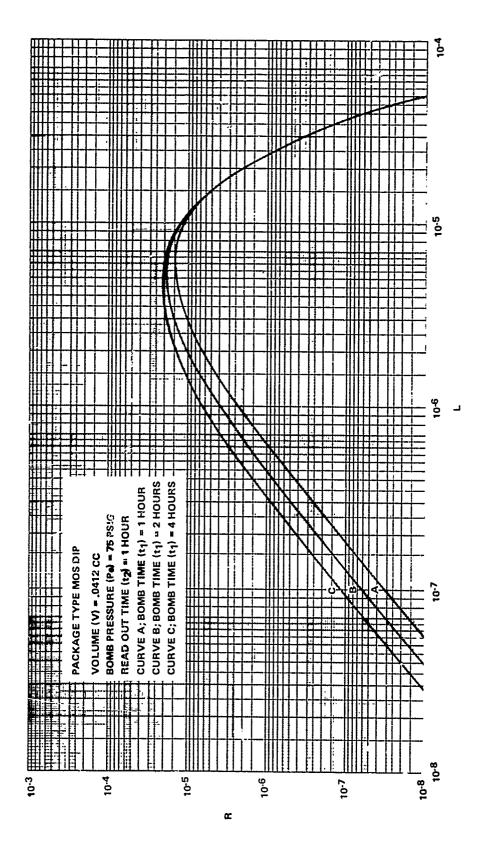


Figure 21. MOS DIP Time/Pressure Sequence-Bomb Fressure = 75 psig

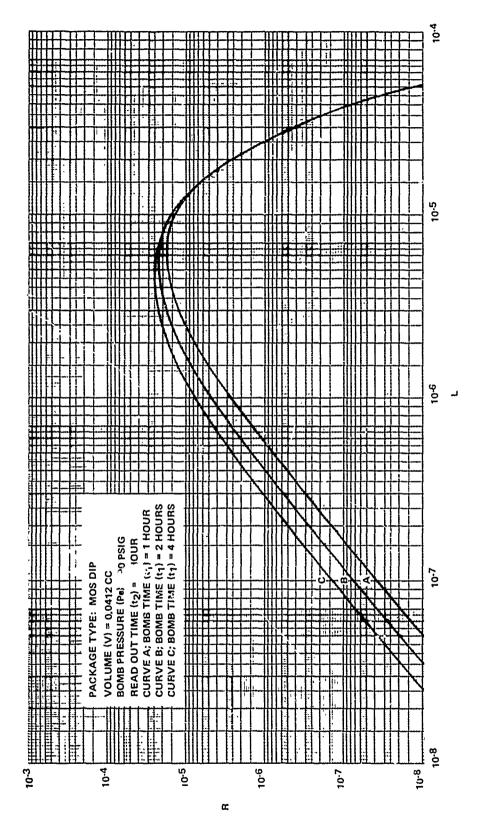


Figure 22. MOS DIP Time/Pressure Sequence-Bomb Pressure = 90 psig

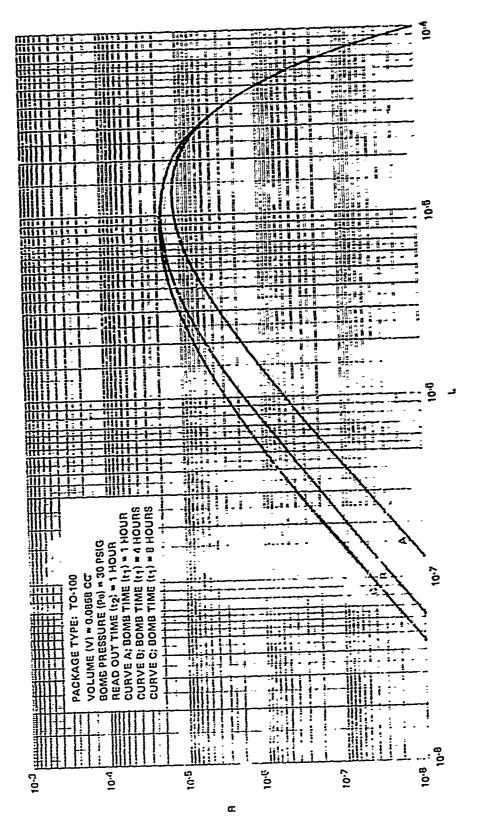
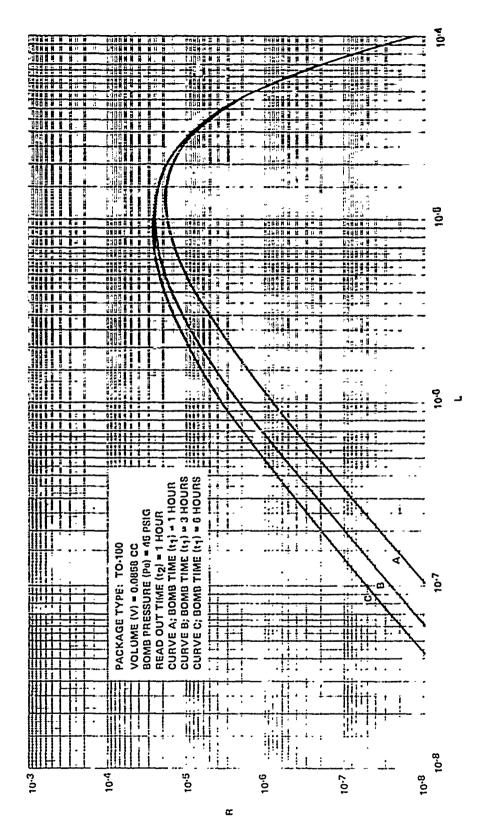


Figure 23. TO-100 Time/Pressure Sequence-Bomb Pressure # 30 pslg



der.

Figure 24. TO-100 Time/Pressure Sequence-Bomb Pressure # 45 pslg

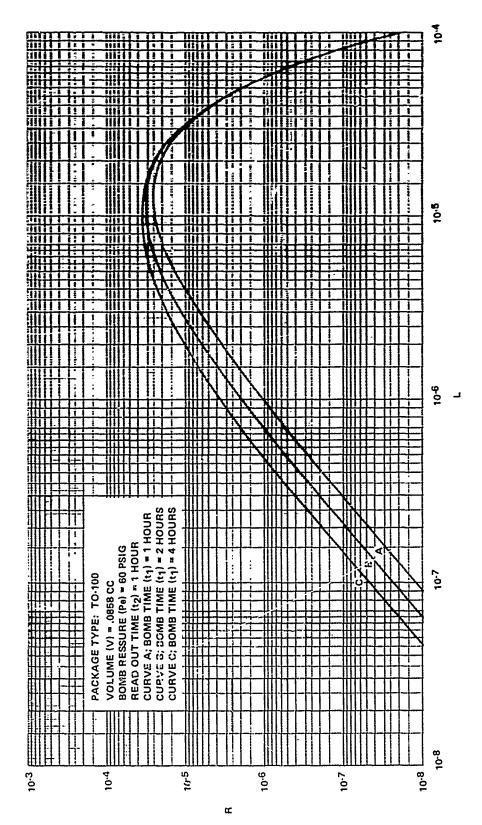


Figure 25. TO-100 Time/Pressure Sequence-Bomb Pressure = 60 psig

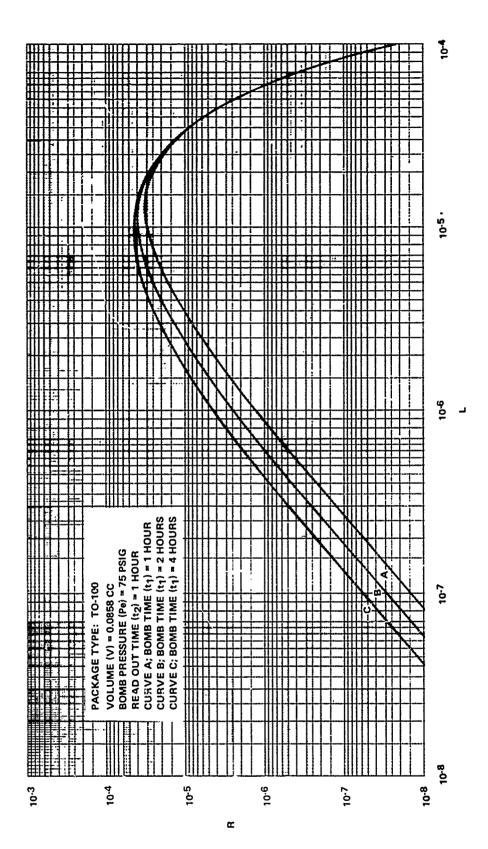
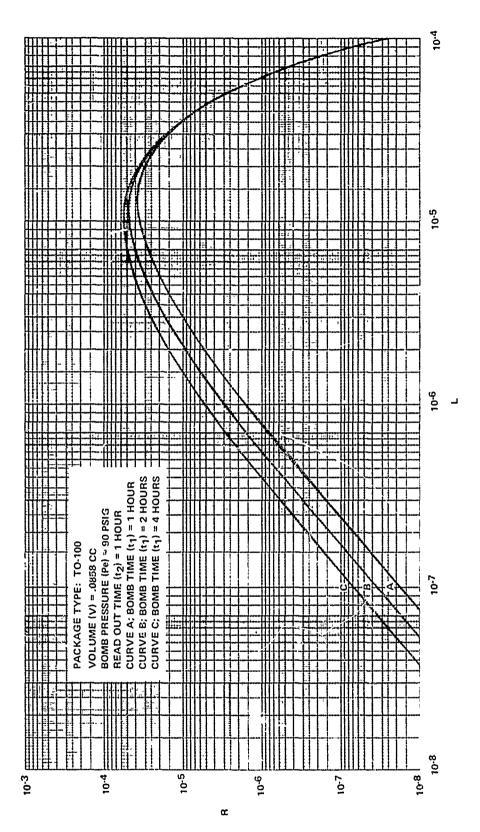


Figure 26. TO-100 Time/Pressure Sequence-Bomb Pressure = 75 psig



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Figure 27. TO-100 Time/Pressure Sequence-Bomb Pressure = 90 psig

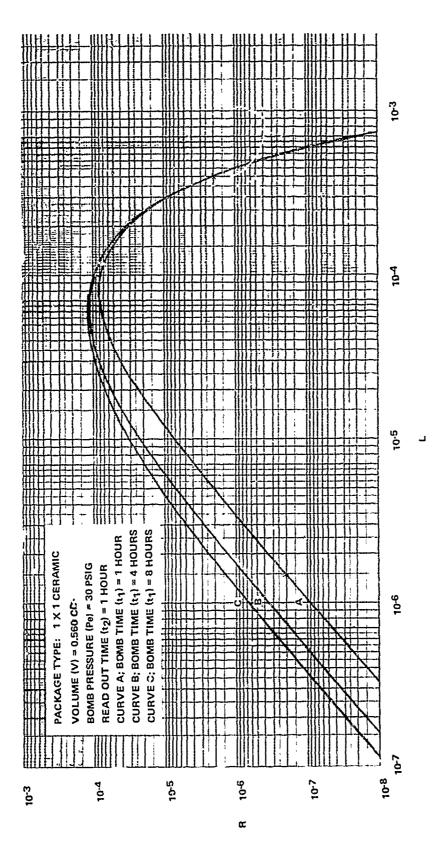


Figure 28. 1 X 1 Ceramic Time/Pressure Sequence-Bomb Pressure = 30 psig

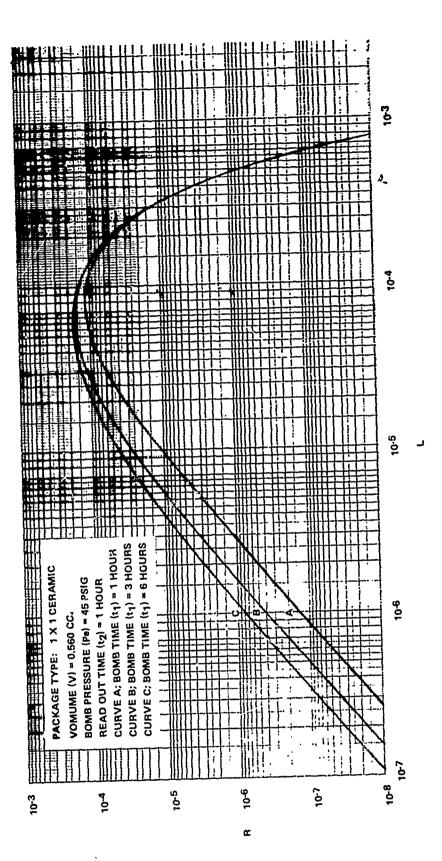


Figure 29. 1 X 1 Ceramic Time/Pressure Sequence-Bomb Pressure = 45 psig

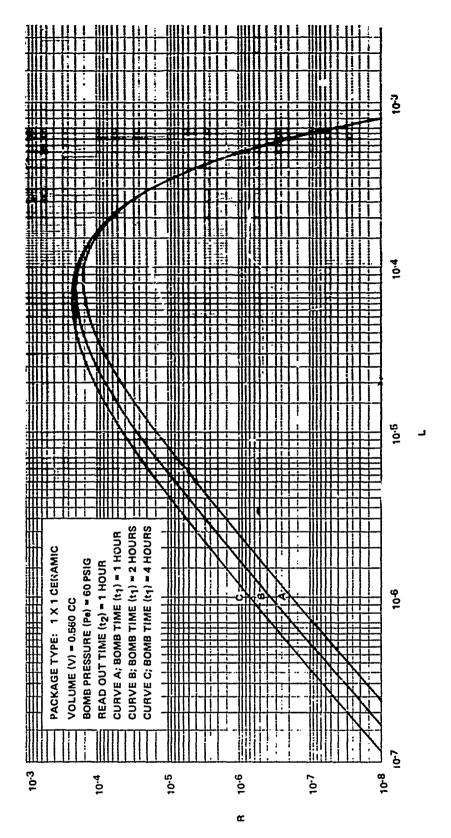
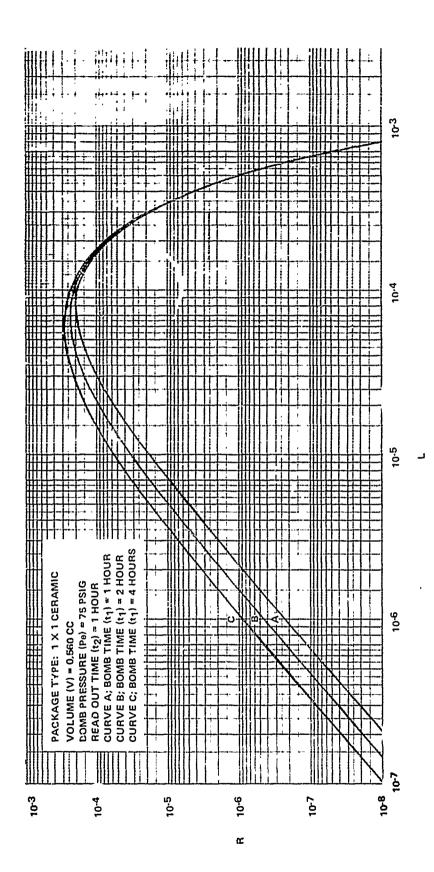


Figure 30. 1 X 1 Ceramic Time/Pressure Sequence-Bomb Pressure = 60 psig



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Figure 31. 1 X 1 Ceramic Time/Pressure Sequence-Bomb Pressure = 75 psig

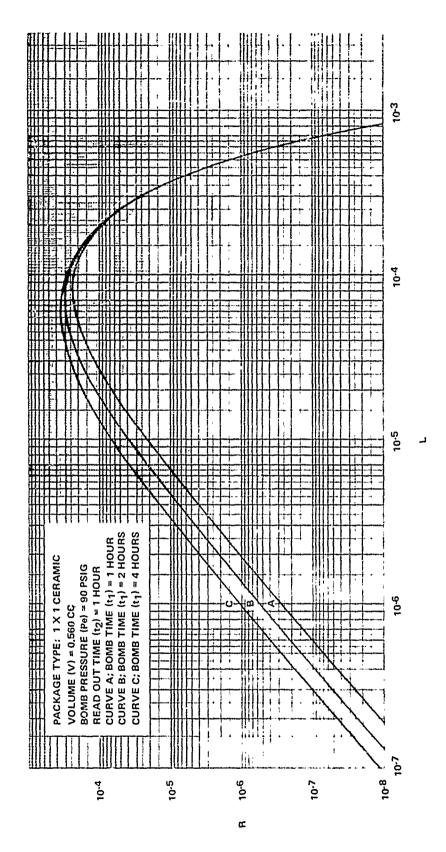


Figure 32. 1 X 1 Ceramic Time/Pressure Sequence-Bomb Pressure = 90 psig

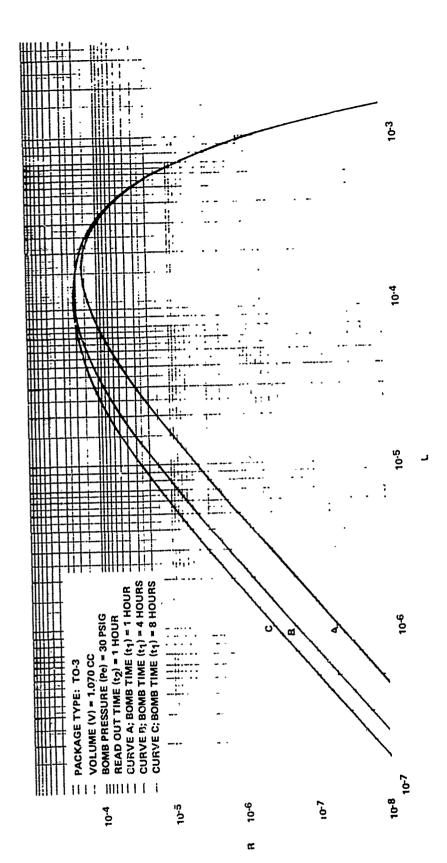


Figure 33. TO-3 Time/Pressure Sequence-Bomb Pressure = 30 psig

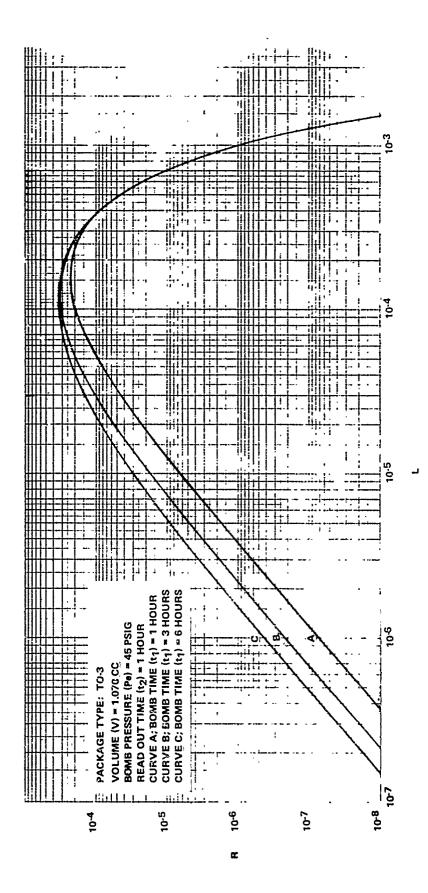


Figure 34. TO-3 Time/Pressure Sequence-Bomb Pressure = 45 psig

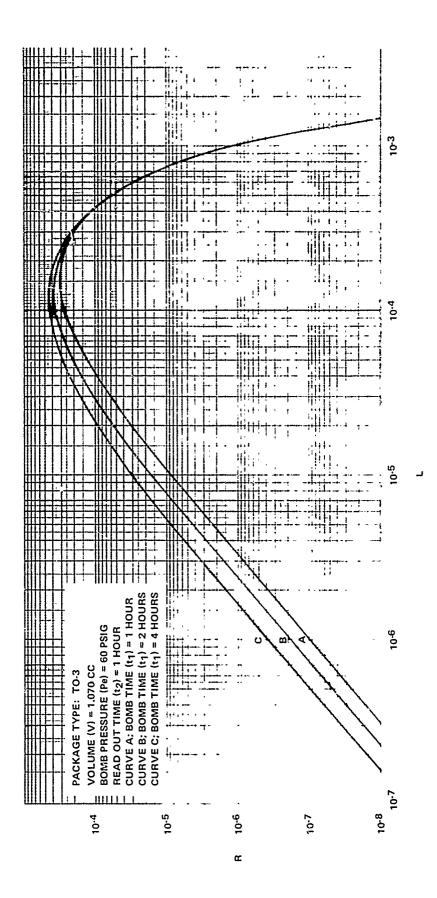


Figure 35. TO-3 Time/Pressure Sequence-Bomb Pressure = 60 psig

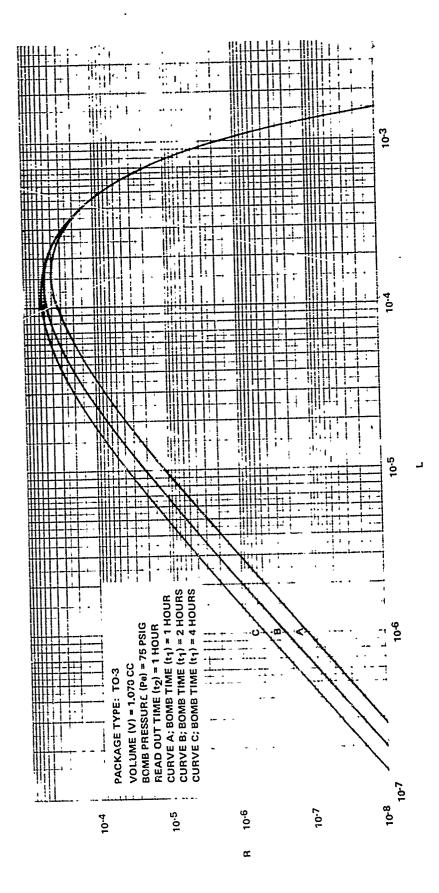


Figure 36. TO-3 Time/Pressure Sequence-Bomb Pressure = 75 psig

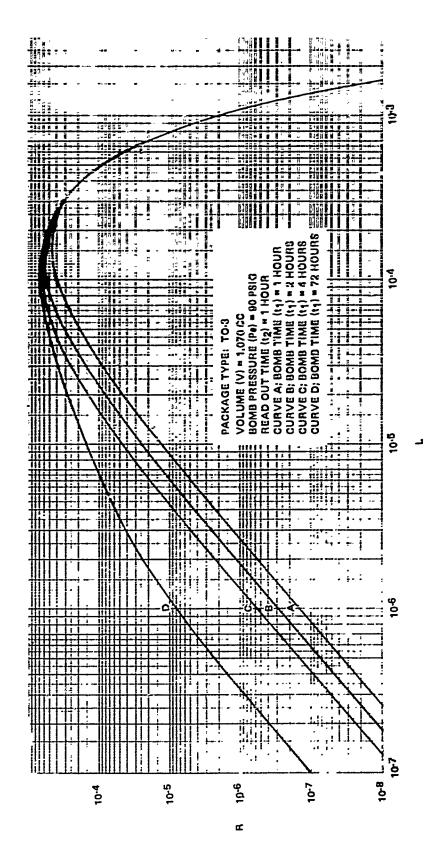


Figure 37. TO-3 Time/Pressure Sequence-Bomb Pressure # 90 psig

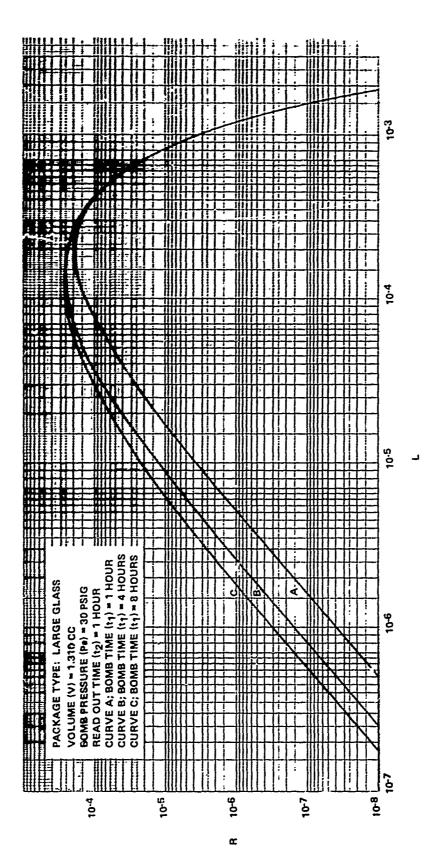


Figure 38. Large Glass Time/Pressure Sequence-Bomb Pressure = 30 psig

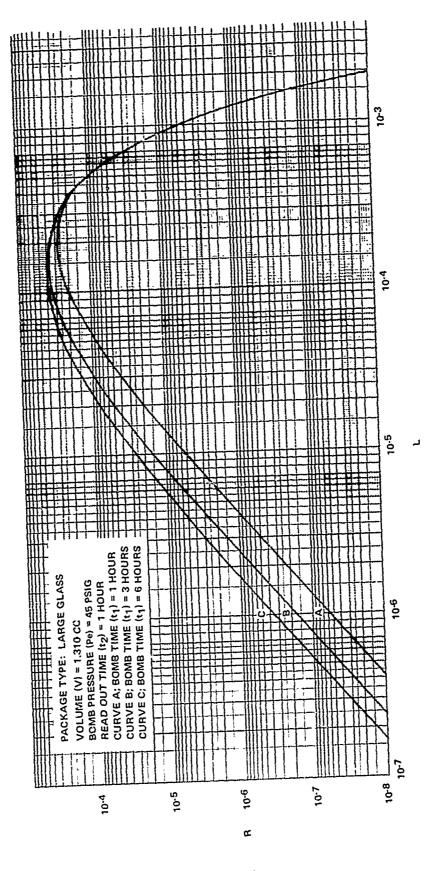


Figure 39. Large Glass Time/Pressure Sequence-Bomb Pressure = 45 psig

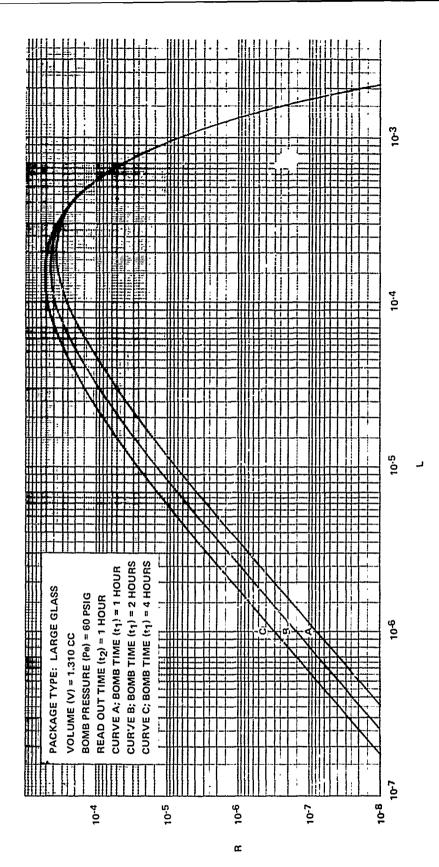


Figure 40. Large Glass Time/Pressure Sequence-Bomb Pressure = 60 psig

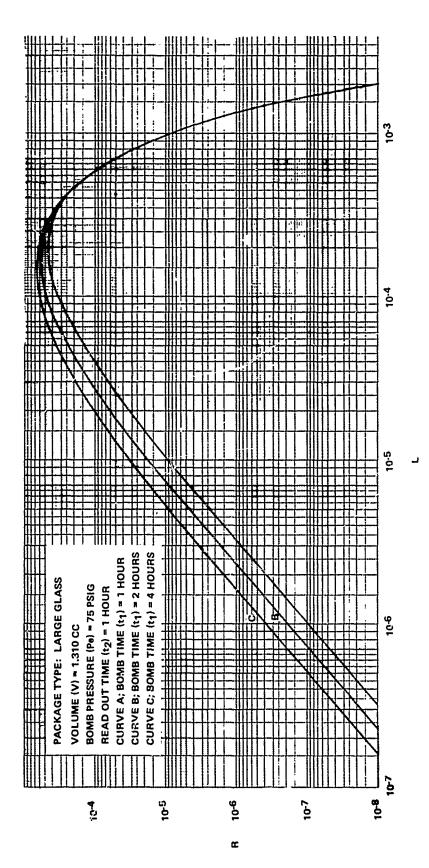


Figure 41. Large Glass Time/Pressure Sequence-Bomb Pressure = 75 psig

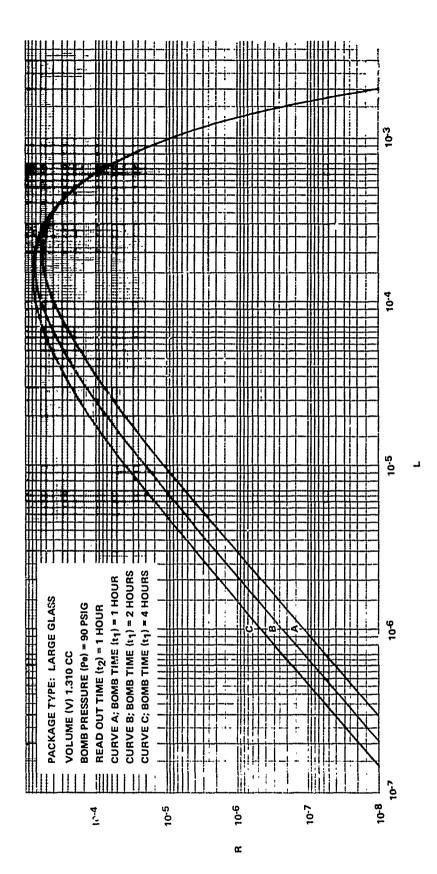


Figure 42. Large Glass Time/Pressure Sequence-Bomb Pressure = 90 psig

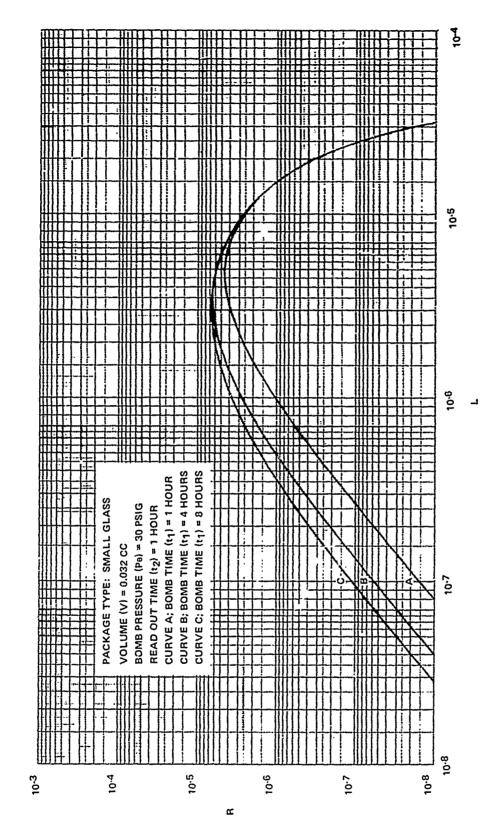
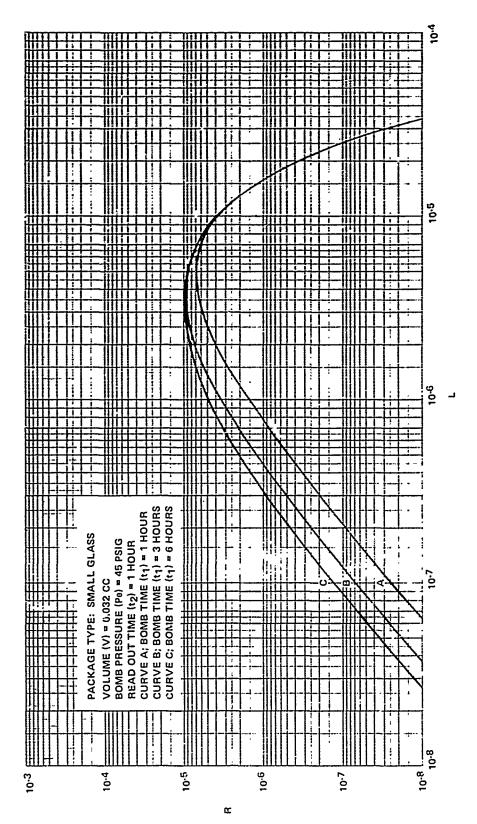


Figure 43. Small Glass Time/Pressure Sequence-Bomb Pressure = 30 psig



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Figure 44. Small Glass Time/Pressure Sequence-Bomb Pressure = 45 psig

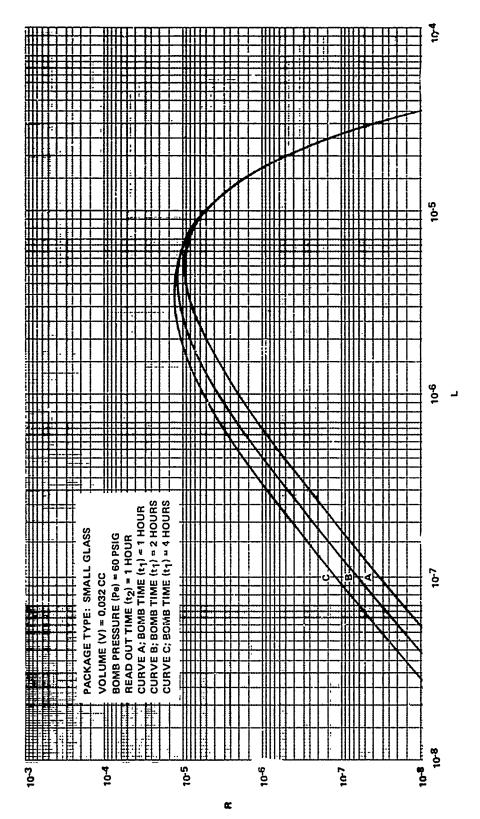


Figure 45. Small Glass Time/Pressure Sequence-Bomb Pressure = 60 psig

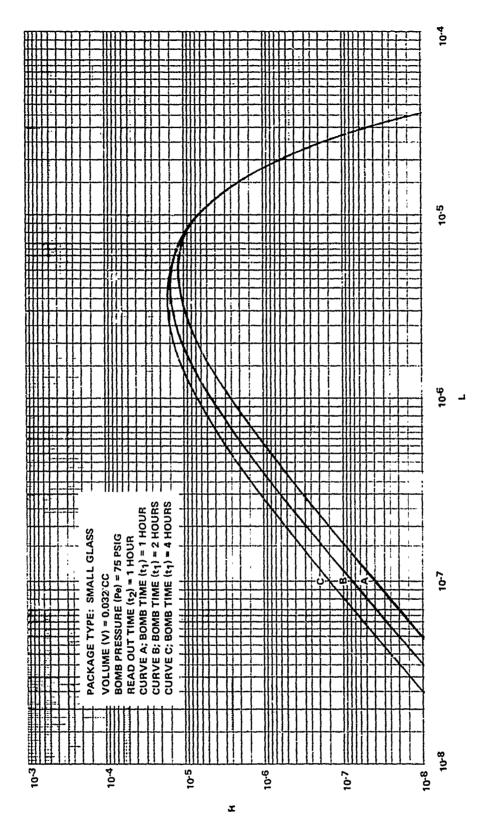


Figure 46. Small Glass Time/Pressure Sequence-Bomb Pressure = 75 psig

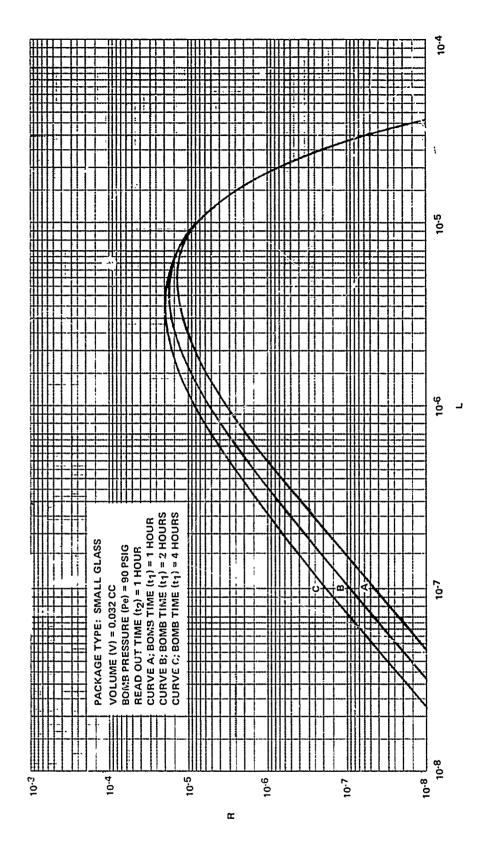


Figure 47. Small Glass Time/Pressure Sequence-Bomb Pressure = 90 psig

SECTION III

EVALUATION OF HELIUM METHOD

Phase II of the project was devoted to the evaluation of Test Condition A, Method 1014 of MIL-STD-883, the equipment used for this method, and the effect of test parameter variables on the sensitivity of the method.

This phase consisted of subjecting each test device and each glass standard to each of the pressurization conditions shown in Table III. The following format was used as a guideline for this phase:

Table III. Helium Time Pressure Matrix

Time	Pressure (psig)				
(Hours)	30	45	60	75	90
1	×	×	×	×	x
2	! 		×	×	x
3		×			
4	×		×	×	x
6		×			
8	×				

Graphs were plotted using Equation (1) for all units for each time and pressure sequences (Figures 3-47). The units were subjected to each of the test conditions and leak values recorded. Using the graphs for each type of unit, the calculated leak rate values were determined and tabulated. The units were subjected to a minimum of 16 hours vacuum bake between each test condition to ensure no residual gas. The evaluation was performed using MS-12 and MS-90 UFT Veeco mass spectrometers. The calibration of the spectrometers was checked each hour to ensure no drift in calibration.

It appears from a rearrangement of Equation (1), that the graph could be plotted for 30 psia and the calculated leak rate determined for any pressure by dividing the indicated value by the bomb pressure in atmospheres to reduce the indicated reading to 1 atmosphere. This is shown by the following:

$$R_1 = P_E \frac{L}{P_o} \left(\frac{M_A}{M} \right)^{1/2} \left\{ 1 - e^{-\epsilon} \left[\frac{Lt_1}{VP_o} \left(\frac{M_A}{M} \right)^{1/2} \right] \right\} e^{-\epsilon} \left[\frac{Lt_2}{VP_o} \left(\frac{M_A}{M} \right)^{1/2} \right]$$
(4)

When P_E increases to 2, 3—N the value of R increases by a factor of 2, 3—N. Therefore, by using a graph plotted at one atmosphere and bombing at four atmospheres, for example, the R value would be four times larger than the value on the graph. The true L value could be determined by dividing the R value by four to reduce it to the one atmosphere graph value. It was verified from the test results that the above statement is true. However, to eliminate any possibility of error, graphs were plotted for all test pressures. The values on the down side of the curve, 10^{-6} , 10^{-5} , and 10^{-4} , were determined by using the initial weight gain data, which indicated the leak range. If the evaluation had been performed as a production test, a horizontal line would have been drawn on the curve to screen for the smallest value specified and all readings above the line would have been rejected (Figures 48-51). The graphs were plotted assuming that all units would be read-out one hour after removal from the bomb. The units were, in fact, read within one hour, which resulted in the gross leakers reading different values for different conditions due to the readout time (Figure 52).

The test results on the packages with internal volumes ≤ 0.086 cc verified that the equation defines the gas behavior from 1 X 10⁻⁸ L to approximately 5 X 10⁻⁵ L as shown in Figure 53. The results also show that the devices with L values greater than the value under the curve read less than 1 X 10⁻⁸ in a very short time span. It can be concluded that the equation is true for devices with internal volumes ≤ 0.086 cc. The data verified that the equation defines the gas behavior from 1 X 10⁻⁸ L to approximately 5 X 10⁻⁵ L for devices with internal volumes ≥ 0.45 cc. The data shows that for the large volume packages (≥ 0.45 cc), the escape rate which is defined by the expression

$$e^{-\left[\frac{Lt_2}{VP_O}\left(\frac{M_A}{M}\right)^{1/2}\right]}$$
 (A)

is not valid beyond approximately 5×10^{-5} L. Based upon the results of the 1×1 ceramic and the TO-3, the magnitude of the escape rate is greater than that defined by the equation. The data show that for the large package, as with the smaller package, the devices with leak rates greater than the values under the curve read R values significantly less than the reject limit in a very short time span. The escape rate of devices with leak rates in the 10^{-5} range was verified by monitoring the decay rate over a 2-hour period on the glass standard leaks (Figure 54). It can be concluded that the equation is true for all evaluated packages over the range of 1×10^{-8} L to 5×10^{-5} L. The equation was found to be invalid for L values greater than 5×10^{-5} L. It should be noted that the

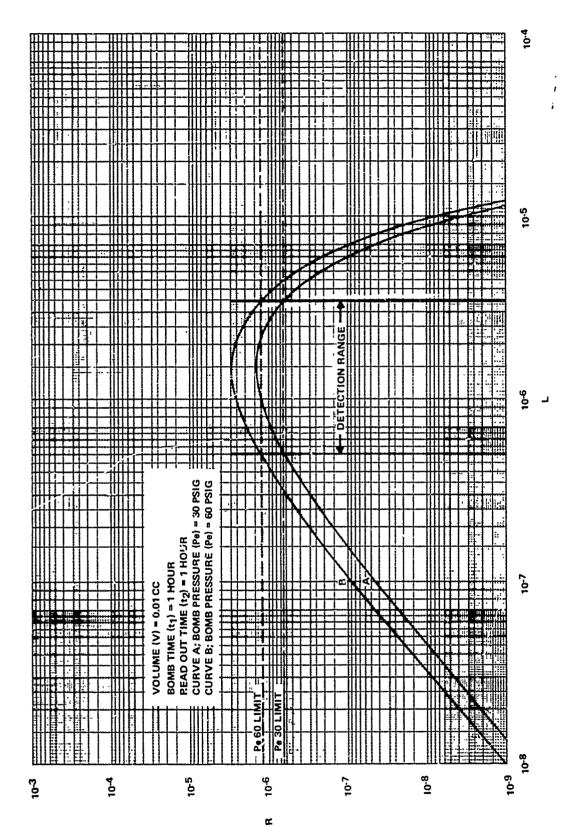


Figure 48. Effects of Pressure Increase for 0.01 cc Volume

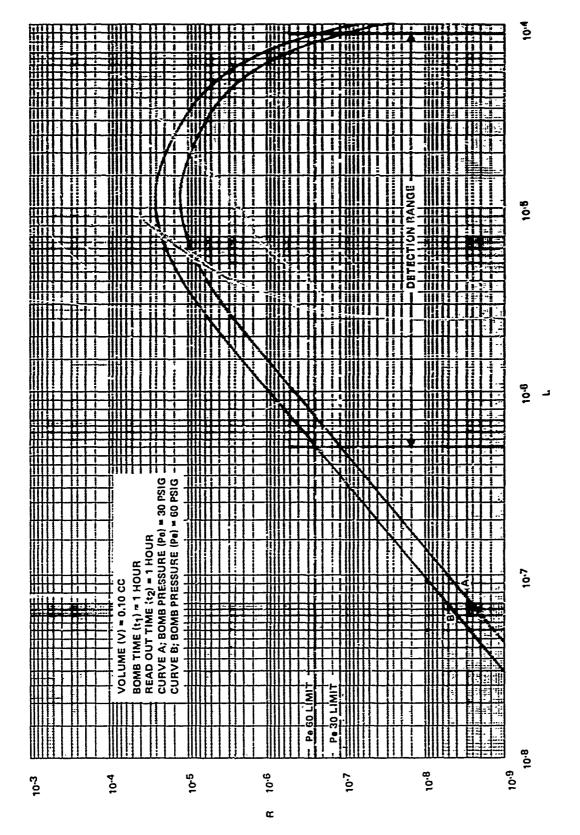


Figure 49. Effects of Pressure Increuse for 0.10 ce Volume

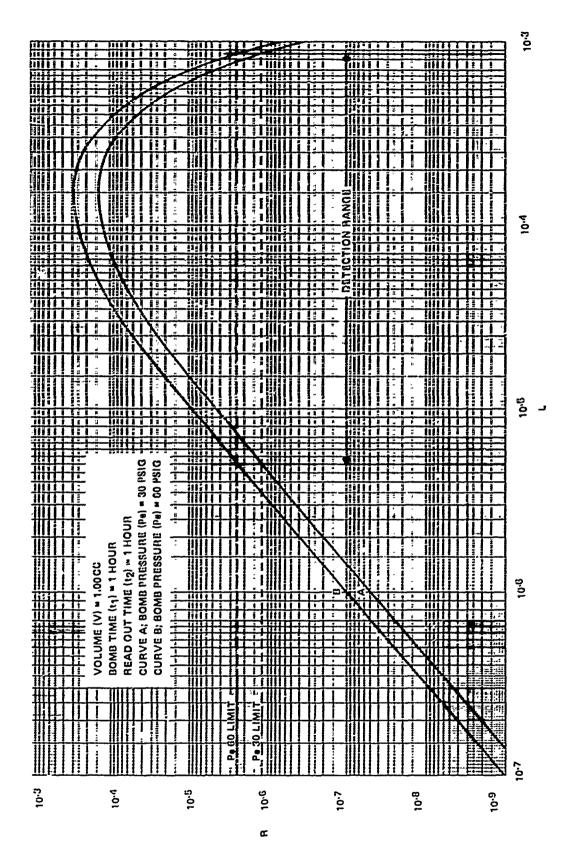


Figure 50. Effects of Pressure Incrense for 1.00 ce Volume

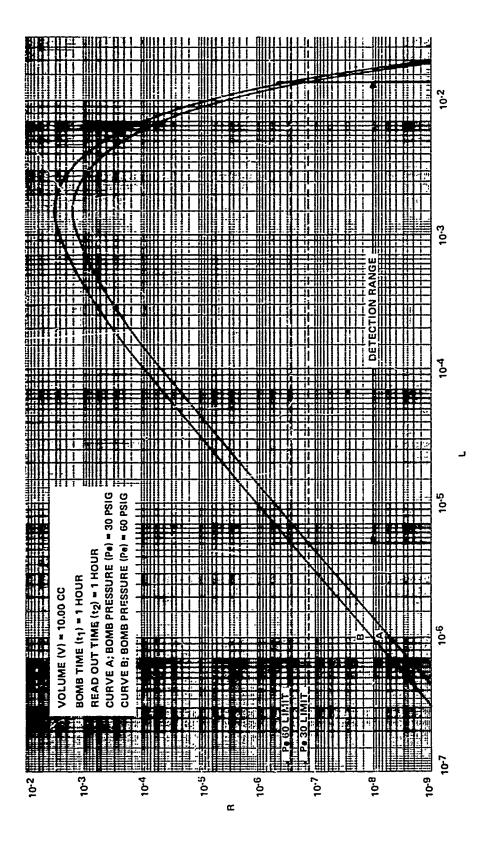


Figure 51. Effects of Pressure Increase for 10.00 cc Volume

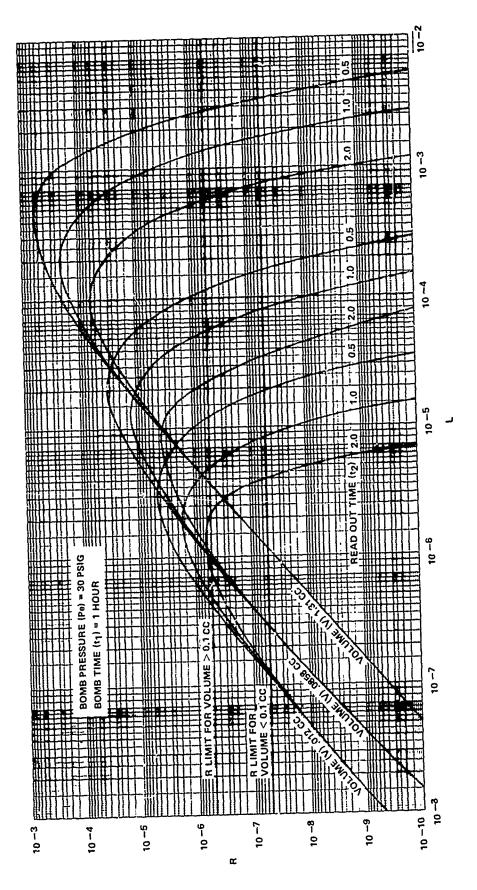


Figure 52. Effects of Time Out of Bomb on Indicated Leak

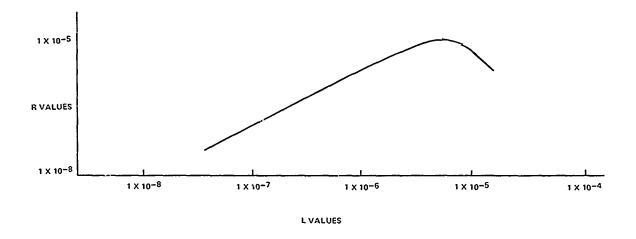


Figure 53. R Values versus Calculated L Values

test condition will detect leakers greater than 5×10^{-5} L, however, the escape rate is high under normal production test procedures and will be discussed under test results.

When testing some of the units, the mass spectrometer amplifier was reduced by a factor of 10 to enable readings to be made in the 10^{-5} range. The machine was calibrated using a diffusion-type calibrator with a helium output rate of 5.2×10^{-8} . All scales from 10^{-8} to 10^{-6} could be checked for one point linearly; however, the 10^{-9} and 10^{-10} could be questionable but the reject criteria in all cases required the unit to have an indicated value of 10^{-8} or greater. All units were tested a total of four times using the same pressure and exposure time to verify the repeatability of the method.

Several significant points resulted from this evaluation.

1) The sensitivity of this technique proved to be more dependent on pressurization time, time out of bomb, and package volume, than on the pressure used for exposure to the tracer gas (Figure 55). Examination of Equation (1) shows that as t₁ in the expression

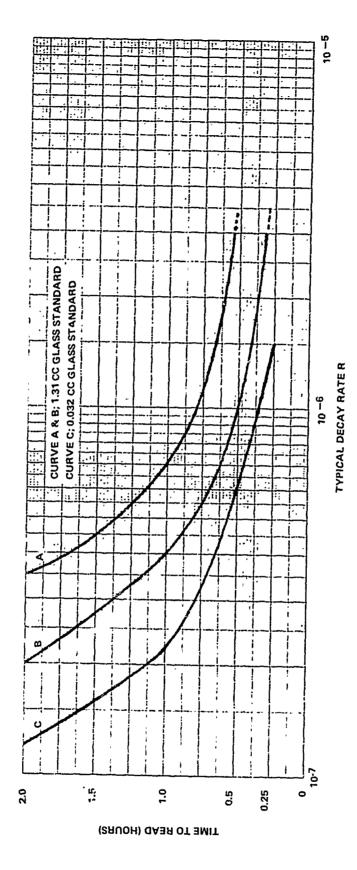
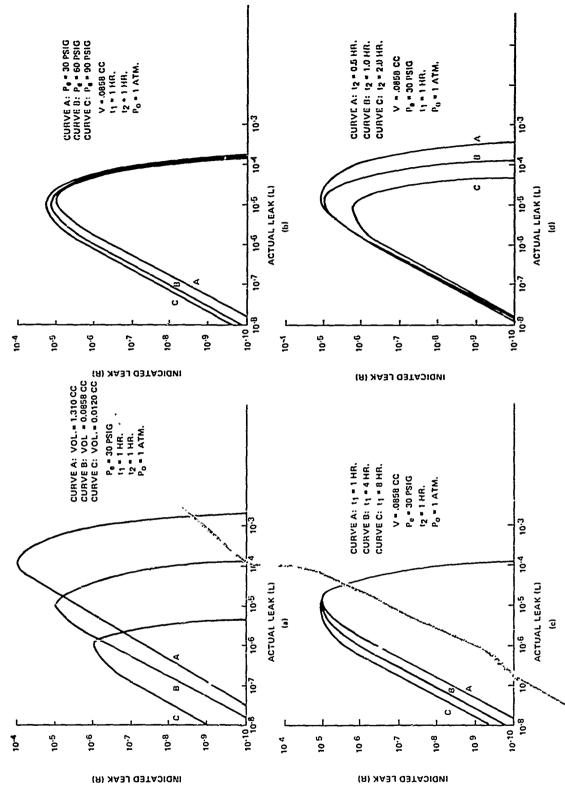


Figure 54. Typical Decay Rates



Figur, 55. Graphical Comparisons of (a) Volume Changes, (b) Pressure Changes, (c) Bomb Time Changes, and (d) Readout Time Changes of the Helium Leak Rate Formula

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$$1 - e^{-\left[\frac{Lt_1}{VP_0} \left(\frac{M_A}{M}\right)^{1/2}\right]}$$
 (B)

approaches ∞ the value of e^{-x} approaches 0, resulting in this term approaching 1 and thus producing a larger R reading. From the expression

$$e = \left[\frac{\text{Lt}_2}{\text{VP}_0} \left(\frac{\text{M}_A}{\text{M}} \right)^{1/2} \right] \tag{A}$$

When t_2 is 0 this expression becomes equal to 1. As t_2 approaches ∞ the value of e^{-x} approaches 0, resulting in the value of R approaching 0. Examining expressions (B) and (A) with respect to V as V gets larger, and if t_1 and t_2 are constant, then the value of L must get larger to make expression (B) equal to expression (A), as this is the point where the curve starts down. As L gets larger the expression

$$\frac{LP_E}{P_O} \left(\frac{M_A}{M}\right)^{1/2} \tag{C}$$

gets larger, resulting in a larger R reading. The exposure pressure appears in expression (C) only, and since the term is in atmospheres the effect on R is not as great as the terms in the exponential function. Therefore, the sensitivity of the method is affected very little by increasing the pressure above 60 psig.

Table IV depicts the data resulting from the matrix (Table III) in terms of the number of leakers, assuming reject values of $R > 5 \times 10^{-8}$ and $L > 5 \times 10^{-7}$ for volumes ≤ 0.1 cc, and $R > 5 \times 10^{-7}$ and $L > 5 \times 10^{-6}$ for volumes > 0.1 cc, detected at each pressure. The table shows that in most cases, if an R value is used as a reject criteria, the number of rejects increases as the bomb time increases at each pressure. As R increases, the actual leak rate L decreases. As an example, the L value for the TO-100 is equal to 3×10^{-7} when bombed at 30 psig for 1 hour, with R equal to 5×10^{-8} but the L value is equal to 8×10^{-8} when bombed at 90 psig for four hours using the same 5×10^{-8} R value (Figures 23 and 27). If the units are to be submitted to a helium test and rejected when R is equal to or greater than 5×10^{-8} , the bomb pressure and dwell time must be specified and observed; otherwise the actual leak rate L will vary greatly [Figure 55(b) and (d)].

Table IV. Helium Evaluation - Number of Rejects at Test Conditions

R>5 X 10^{-8} , L>5 X 10^{-7} for volume <0.1 cc R>5 X 10^{-7} , L>5 X 10^{-6} for volume >0.1 cc

Bomb C	onditions					Pac	kage				
Press	Time	то	-84	C-F	PAK	C-I	DIP	М	os	то	100
psig	Hours	R	L	R	L	R	L	R	L	R	L
30	1	18	16	75	61	39	33	23	20	68	64
30	4	15	13	69	64	50	36	27	24	69	62
30	8	19	15	75	52	58	38	25	20	67	61
45	1	16	12	67	63	48	40	19	19	67	62
45	3	18	12	71	60	54	36	27	20	68	63
45	6	16	13	59	44	57	38	23	19	71	61
60	1	16	14	62	51	54	40	21	19	67	60
60	2	17	14	71	57	56	40	27	20	67	56
60	4	24	21	78	52	56	35	52	39	79	69
75	1	17	15	68	54	53	33	25	19	54	46
75	2	17	12	60	36	48	31	28	22	55	40
75	4	18	14	70	46	52	31	25	19	61	50
90	1	18	13	68	62	49	35	49	30	52	44
90	2	19	15	66	40	53	35	41	26	53	45
90	4	20	16	67	54	53	36	46	31	55	44

Bomb C	onditions		Package							
Press	Time	1 X 1 C	Ceramic	T	TO-3		Glass	Sinall	Glass	
psig	Hours	R	L	R	L	R	L	R	L	
30	1	14	4	58	43	19	17	17	7	
30	4	18	6	52	40	27	18	17	6	
30	8	28	6	64	33	30	19	17	4	
45	1	22	7	45	33	32	22	17	9	
45	3	21	7	49	29	33	20	17	4	
45	6	44	6	51	30	20	19	16	4	
60	1	26	7	41	32	31	21	17	9	
60	2	35	4	51	33	34	21	17	7	
60	4	37	. 5	55	34	- Sie	19 19 16	17	6	
75	1	42	11	43,	35	26	المراجع والمراجع	17	3	
75	2	50	13	46	32	28	16	17	3	
75	4	53	11	44	32	33	16	استرخاني	3	
90	1	47	12	52	40	28	14	17	7	
90	2	57	6	53	44	34	13	17	6	
90	4	60	13	55	43	32	12	17	3	

- Table IV shows that if an L value was used as the reject criteria, the number of rejects was essentially the same for all bomb pressures and times up to 60 psi. One advantage of specifying the L value as the reject criteria is that if the bomb pressure or dwell time is inadvertently different than what is specified, all units will still be tested at the proper value since L is a calculated value. Also, all units will be tested to the same actual leak rate. In this case the R value will vary but will not affect the results of the test.
- 4) The repeatability of the procedure is very dependent on the leak rates and time to read of the devices being tested. Repeatability as discussed here is the machine's ability to read within the same decade on four data runs, not necessarily the ability to detect the same rejects four times. In the so-called fine-leak range, repeatable readings occurred on from 70 to 87 percent of the devices on each of four test runs at the same conditions. Lack of repeatability was caused primarily by devices with leak rates in the 10⁻⁶ range and higher rates on small volume ceramic packages than on metal can packages. Table V shows the percentage of fine leakers of each case type which exhibited repeatable readings throughout the four test runs and also the percentage of the total sample, fine and gross leakers, which had repeatable readings.

Table V. Test Condition A Repeatability

	Percent Including Gross Leakers		
83	94		
70	26		
71	64		
87	89		
77	93		
80	56		
	85		
	86		

The object of the MS-90 UFT evaluation was to determine the capability of this mass spectrometer in detecting gross leakers and number of units that can be tested per hour. This machine is designed to have a very rapid pump-down time, thus testing the devices before the helium has a chance to escape. This rapid pump-down time frame occurs in the first 1-1/2 seconds after the unit has been placed in the test chamber and pumping has begun. During the next one second, a Pirani gauge is exposed to the pressure in the test chamber and if the pressure is low enough, the test valve is allowed to open. If the pressure is too high, the "gross leak" lamp will light

and the test portion of the cycle will be bypassed. In order for this machine to be consistent in detecting gross leakers, the magnitude of expression

$$e = \left[\frac{Lt_2}{VP_O} \left(\frac{M_A}{M} \right)^{1/2} \right]$$
 (A)

must be small enough to make the value of R larger than the reject point.

Test conditions were chosen to relate to a specific condition utilized in the MS-12 AB variable data runs (Table VI). The devices were subjected to a minimum of 16 hours vacuum bake and tested for residual helium prior to this test sequence.

Time (t₁ - hours) **Package** Bomb Pressure (psig) TO-84 30 C-PAK 30 C-DIP 30 MOS 60 TO-100 60 1 X 1 Ceramic 60 TO-3 60 Glass Standards

Table VI. MS-90 UFT - Device Preconditioning

The MS-90 UFT was calibrated as follows prior to the start of this sequence:

1) Checked and set the filament current.

- 2) "Peaked out" the machine to read the leakage of helium, which was marked on the side of the calibrator.
- 3) Verified the zero and calibrator reading to ensure no residual helium in the system.

A sensitivity check was made at the beginning and at the conclusion of the test sequence on each package type. The leak indicator gauge was adjusted to indicate the leak rate limit and the devices were categorized as good or reject.

An attempt was made to read variable data with the mass spectrometer operating in the automatic mode. Unless the approximate leak rate is known, it is impossible to obtain reliable variable readings because the 1-second sample time inherent in the equipment is inadequate to seek out the proper indicator range. Therefore only fail/pass data was recorded. The data results indicate

no significant differences in the number of gross rejects detected by this machine. A few were detected due to the faster read time and therefore gas still being in the units. This is a function of read time and therefore a percentage cannot be placed on the number. The number of rejects detected at each condition is shown in Table VII.

Table VII. MS-90 UFT Helium Evaluation – Number of Rejects $R > 5 \times 10^{-8}$ and 5×10^{-7}

	Pressure/Time (t ₁)							
Package	30/1	45/1	60/1	60/2				
TO-84	18							
C-PAK	56	1						
C-DIP	38	1						
MOS				23				
TO-100		[69				
1 X 1 Ceramic			40					
TO-3		1		61				
Glass Standards		47						

The time required to classify as good or reject on an MS-90 UFT was approximately three times as fast as the MS-12 AB system. The test sequence time on this particular machine varied from 8 to 9 seconds depending upon the volume of the empty fixture used. The spectrometer is more efficient when the internal cavity of the fixture and the overall volume of the package is approximately the same. There was no evidence of rapid pump-down being significantly more effective in detecting gross leakers. The residual helium was a problem when testing devices which had large leaks.

The results of this study indicate that the mass spectrometer, when set up as described above, can be used to detect microcircuit seal leaks with a high degree of accuracy in the leak range defined by the equation for each package type. The leak range limits of each package are discussed under test results.

SECTION IV

EVALUATION OF RADIO: SOTOPE

Phase III of the project was devoted to evaluation of radioactive tracer gas methods described in Condition B, Method 1014 of MIL-STD-883.

Equation (2) in Section III was solved for each package type for $Q_s = 1 \times 10^{-8}$. The equation indicates that the gas does not escape from the units, this did not prove to be true. All the gross leakers detected by weight gain were not detected. The equation appears to be valid for the fine leakers as both Test Conditions A and B produced the same results for the fine leakers. In order for the equation to be completely valid, there should be a function to describe the escape rate of the gas. The equation was solved using different (600 and 1200) internal count reject parameters, and three (277, 600, and 1397) specific activity values. The results are discussed below.

The units were subjected to a varying number of wash cycles (Table VIII) to determine the effect on each package type (Table IX). The units were vacuum baked for a minimum of 16 hours between each test sequence to ensure no residual gas. The testing was performed on two different systems, a CEC 24-510 and an IsoVac Mark IV to verify correlation between systems. The test results indicate that the number of wash cycles, up to three, made no significant difference in the readings. The repeatability testing was performed a total of four times on each unit, using one wash cycle.

Two of the repeatability runs were made with a specific activity of 600 and two with a specific activity of 1397. The specific activity, when testing with the Mark IV, was 277. The data showed that there was no significant difference in the results as long as the other parameters are chosen to satisfy the equation. The units were tested using an internal count of 1200 and 600 counts per minute as the R parameter of the equation. Varying the specific activity and the R parameters allowed a varying bomb time with no significant difference in the results. The tracer gas was stored

Table VIII. Krypton-85 Matrix

Wash	Microcuries per cm ³						
Cycles	277	600	1397				
0	×		×				
1	×	×	x				
3	x		X				

Table IX. Radioisotope Test Results – Number of Units Detected as Rejects

Devices		CEC 24-510		IsoVac MARK IV				
	ow	1W	3W	ow	1W	3W		
TO-84	19	20	22	22	23	23		
C-PAK	56	51	52	49	50	47		
C-DIP	29	32	29	22	37	33		
MOS	22	21	20	17	31	19		
TO-100	42	44	48	44	47	42		
1 X 1 Ceramic	1	5	4	6	6	8		
TO-3	29	26	31	36	52	51		
Glass Standard	12	17	16	13	15	15		

ACTIVATION PRESSURE AND TIME FOR $Q_S = 1 \times 10^{-8}$ VOLUME OF 0.1 cc AND LESS REJECT Q = 5 X 10⁻⁷ VOLUME GREATER THAN 0.1 cc REJECT Q = 5 X 10⁻⁶

at 0.3, 0.4, and 0.5 torr with no effect on the results. The data is shown in Table VIII and will be discussed for each package type under test results.

The following describes the procedure used for Phase III. The equation

$$Q_{S} = \frac{R}{SKT\overline{P}t}$$
 (2)

was solved for each package type assuming Q_s equal to 1×10^{-8} and R equal to 1200 and 600 counts per minute. The time T was selected in tenths of an hour as this is controlled by the design of the equipment. \overline{P} was calculated so that the pressure applied to the units would not exceed 100 psia. The specific activity S of the gas was determined by comparing a sealed sample gas source supplied by the Atomic Energy Commission with an activity of 24.5 μ curies/cc and corrected for its decay rate by using the following formula.

$$A = A_0 e^{-\frac{0.693 t}{T^{1/2}}}$$
 (5)

where

A = activity now

A₀ = the original activity on the given date

e = the natural log of 2

t = the elapsed time between the original measurement and now

 $T^{1/2}$ = the half-life of the isotope

This value was calculated to be $10.54\,\mu$ curies/oc and read 22,000 cts/min. A sample of gas was then taken from the system. This sample volume was 0.05 cc and measured with a pipette mercury assembly. The specific activity was then calculated by the equation

$$S \mu \text{curies/atm cc} = \frac{\frac{R_1 \text{ cts/min System Sample}}{V_{\text{cc}} P \text{ atm}}}{\frac{R_2 \text{ cts/min Std}}{A \mu \text{ curies}}}$$
(6)

This equation will give a ratio of the cts/min to µcuries/cc of the system sample compared to the standard as shown.

$$\frac{R_1 \text{ cts/min}}{S \mu \text{curies/cc}} = \frac{R_2 \text{ cts/min}}{A \mu \text{curies/cc}}$$
(7)

Knowing R₂, A and measuring R₁, S can be calculated for a true value although the counting efficiency of the system is much less than one. The specific activity of the system was calculated as 10 µcuries/cc with a 6.2 X 10⁴ cts/min for a 0.05 cc volume. Calculating the cts/min for this volume with a concentration of 600 µcuries/cc, the reading should be 6.5 X 10⁷ cts/min. This reading is off by a factor of 1.06 X 10³ due to the counting efficiency of the system. This is compensated for by determining a K factor for each package type as the material and geometrical configuration will affect the counting efficiency. The K factor was determined by drilling a small hole in six devices of each package type and attaching a small copper tube so that a known amount of gas could be placed inside the device. The device was connected to the pipette mercury assembly and 0.02 cc of gas placed inside the device. The copper tube was then pinched closed at the device and the cts/min read. Six devices of each package type were read and an average reading calculated. The K factor for the device was then calculated by the equation

K cts/min
$$\mu$$
 curies =
$$\frac{\text{R ets/min}}{\text{S }\mu\text{ curies/atm cc P atm V}_{\text{cc}}}$$
 (8)

This can be reduced to the following

$$K \operatorname{cts/min} \mu \operatorname{curies} = \frac{R \operatorname{cts/min}}{c \mu \operatorname{curies}}$$
 (9)

where C pearies is equal to the activity of the gas inside the unit. This is a product of the volume of gas times the specific activity of the grs. Now if the cts/min for a given volume of gas contained inside a given package type was calculated, it would produce

$$R = Y_{cc} s k \tag{10}$$

with $V_{\rm cc}$ equal to the volume of gas. This approach allows for a system-type calibration on each package type being tested. Based upon the test results of this study, the radioactive-tracer-gas test method will detect leakers within the leak range limits of each package with a high degree of accuracy. The leak range limits of each package will be discussed in the test section of this report.

As with Condition A, the repeatability of the procedure is dependent on the leak rates being within the sensitivity range for the devices being tested volume. Table X shows the percentage of fine leakers of each case type which exhibited repeatable readings throughout the four test runs and also the percentage of the total sample, fine and gross, which had repeatable readings.

Table X. Test Condition B Repeatability

Packagē	Percent Fine-Leak Range Only	Percent Including Gross Leakers
TO-84	98	97
C-PAK	30	ස
C-DIP	92	92
MOS	95	დვ
TO-100	97	97
1 X i Ceramic	97	93
то-з	97	93

SECTION V

TEST RESULTS OF CONDITIONS A AND B

Phases III and IV test results show that each package size must be handled individually, as any general statement would not hold true for all packages. Results are based on the reject limits of 5 X 10⁻⁷ for volumes greater than 0.1 cc. For both methods to have a common baseline, the results are based upon L, a calculated leak rate for Condition A and upon Q, a calculated value for Condition B. The R value was determined by drawing a horizontal line on the graph starting at L = 5 X 10⁻⁷ or 5 X 10⁻⁶ as applicable and rejecting all values above the line (Figures 48-51). The results show that for the units with a volume less than 0.04 cc there was not an overlap between Test Conditions A and B and Test Condition C. The gap between the test conditions could be closed in most cases by lowering the reject value for the device. Test Condition A has a slightly broader detection range than Condition B. The total test time for Condition B is much less than Condition A due to the bomb times required. The accuracy of both Condition A and Condition B depend upon the strict adherence to exact bomb pressures, dwell time, and time to readout. The sensitivity of the test conditions and the number of rejects detected using current MIL-STD-883 conditions are based upon single test runs with the results displayed in Table XI. The result of performing the tests using the three reject criteria of MIL-STD-883 is displayed in Table XII.

Table XI shows that the results of the test are dependent apon the test condition used and the reject criteria of that condition. If the same Condition A, L value and Condition B, Q value are

Table XI. Comparison of Rejects Detected by Test Condition A and Test Condition B, using a Common Baseline Q and $L > 5 \times 10^{-7}$ for volume ≤ 0.1 cc Q and $L > 5 \times 10^{-6}$ for volume > 0.1 cc

	Rejects D	etected
Device Type	Condition A 60/1 Table III	Condition B
TO-64	14	20
C-PAK	51	53
C-DIF	40	30
MOS	19	21
TO-100	60	44
1 X 1 Ceremic	7	6
70-3	32	29
Large Giass	21	15
Small Glass	9	5

Table XII. Rejects per Failure Criteria of MIL-STD-883, Condition A and Condition B

Darice Type	R	L	Q
TO-84	16	14	34
СРАК	62	51	75
C-DIP	54	40	45
MOS	21	19	33
TO-100	67	42	64
1 X 1 Ceramic	26	7	s
TO-3	41	32	75
Large Glass	31	21	32
Small Glass	17	9	14

used, the results will be similar on those devices within the detection range as shown in Table XI. Test Condition A has a slightly broader detection range for some package types than does Condition B. This is pointed out by the escape rate percentage for each package (Table XIII).

The overkill and escape percentages are based on four test runs performed on each device. The overkill percentage is based on the number of times the test condition called a device in the 10^{-7} or smaller range a gross leaker, with a gross leaker being defined as a device having a leak rate of 1×10^{-6} or greater. The escape percentage is based upon the condition not detecting a leaker in a specific range. The leak rate of the escaping devices was known from the gross leak data. This data is displayed in Table XIII.

SENSITIVITY OF TEST CONDITIONS A AND B

A. TO-84 Package (0.006 cc Internal Volume)

The TO-84 was the smallest volume package tested. It can be seen from the graphs (Figures 3-7) that if the 5×10^{-7} L value is used as a reject point, the sensitive range of the test is from 5×10^{-7} to 2×10^{-6} . If the R value of 5×10^{-8} is used with 1-hour bomb time at 60 psig, the sensitive range is extended to include from 6×10^{-8} to approximately 3×10^{-6} . These ranges are verified by the fact that 92% of the devices known to have leak rates larger than 1×10^{-5} were not detected by Condition A. Test Condition B data indicate that it has slightly less range than Condition A towards the gross end. Eight-nine percent of the devices known to have leak rates larger than 1×10^{-5} were not detected, which is not significantly different from Condition A. However, 33% of the devices having leak rates of 10^{-6} escaped; whereas 4% of this group escaped on the Condition A test. The 10^{-6} group escape rate is reduced to 17% if a reject point of 5×10^{-8} (current limit) is used and to zero if a 1×10^{-8} limit is used.

Table XIII. Test Co. tions A and B, Overkill and Escape Rates When L and $Q = 5 \times 10^{-7}$ on Volumes of <0.1 cc and 5×10^{-6} on Volumes >0.1 cc

	_	_	_						_		_
10:3	1.07	8		11		63	33	យ	0	58	
ğ	-	4		Ξ		43	32	ប	0	77	
1 X 1 Ceramic	0.46	8		i		98	001	100	93	83	
C Can	ö	۷		ı		98	20	25	45	37	
TO-100	0.086	В		2,3		24	22	3.5	0	1	
τŌ	0.0	۷		4.		2.2	2.8	1.7	0	i	
MOS DIP	0.041	8		0		43	20	56	ı	1	
MOS	0.0	٨		-		0	46	55	ı	1	
C-DIP	0.014	8		2.4		46	1	80	į	1	
Ö	0.0	A		3.3		15	1	89	1	ı	
СРАК	0.012	В		7,5		61	53	43	i	ı	
ဝ်	0.	٨		ഗ		4	42	55	1	ı	
TO:84	0.006	83		2.5		33	83	1	1	1	
70	0.0	۷		-		4	35	i	!	1	
Package	Volume (cc)	Test Condition	Overkill %/Bange	<10-6	Escape %/Range	10-6	10-5	10-4	10-3	10-2	

The overkill on Condition A was 1% and on Condition B 2.5% with an overkill being defined as a fine leaker which is classified as a gross leaker by the test condition.

There is not an effective overlap of either Condition A or Condition B with gross leak test conditions for packages of this volume.

B. C-PAK (0.012 cc Internal Volume)

The graphs (Figures 8-12) which result from the solution of the Test Condition A formula indicate that if a 5×10^{-7} L value is used, the sensitive range extends to 5×10^{-6} . If the 5×10^{-8} R value is used with a 1-hour bomb at 60 psig, the range is 9×10^{-8} to 9×10^{-6} . The data tend to support these ranges with the 42% escape rate of devices known to be in the 10^{-6} range. However, the escape rates in the 10^{-5} (42%) and 10^{-4} (55%) points out that Condition A does have some sensitivity beyond the point indicated by the graphs on packages of this volume. Time from release of pressure to read this sensitivity into the gross range is a function of (t_2) and in a practical sense cannot be utilized to replace a gross leak test. The Test Condition B data indicate that the sensitivity range is essentially the same as that of Condition A. The escape rates in the 10^{-6} and 10^{-5} ranges were slightly higher, 61 and 53% respectively, but the escape rate in the 10^{-4} group was lower, 43%. The escape rate in the 10^{-6} group is reduced to 37%, comparable with Condition A, if a 5 \times 10⁻⁸ limit is used.

The overkill rates were higher (5% on Condition A and 7.5% on Condition B) than on the metal can TO-84 devices. Because of the makeup of the population being tested, that is the majority of the devices being leakers of some magnitude, these overkill rates may be higher than would be encountered in a population having a normal distribution.

As indicated by the escape rates in the gross ranges $(10^{-5} \text{ and } 10^{-4})$, there is an overlap but it must be defined as helpful but not dependable in terms of removing these gross leakers.

C. C-DIP (0.014 cc Internal Volume)

Figures 13-17 show that at an L value of 5 X 10^{-7} , the sensitivity range extends to 6 X 10^{-6} and at an R value of 5 X 10^{-8} using standard bomb conditions, the range is from 9 X 10^{-8} to 1 X 10^{-5} . An analysis of the data indicates that the range is slightly less than indicated since 15% of the devices having leak rates in the 10^{-6} range escaped using the 5 X 10^{-7} L value and 6% of this group escaped using the 5 X 10^{-8} R value. However, some of the leakers in the 10^{-4} group were detected by the method which, as with the C-PAK, indicates that t_2 is a critical factor in detecting gross leakers by Condition A. The sensitivity range of Condition B is apparently slightly less than that of Condition A since 46% of the devices in the 10^{-6} group escaped detection using

the 5 \times 10⁻⁷ limit. However, if the current 5 \times 10⁻⁸ Q limit is used, the escape rate in the 10⁻⁶ group is reduced to 3%.

The overkill rates were 3.3 and 2.4% respectively for Conditions A and B using the 5 \times 10⁻⁷ limit in both cases. Some slight increase is noted if the limits are lowered, but as pointed out earlier, these are not normal distributions.

Based on the fact that some escapes do occur in the 10^{-6} range with the conditions, an overlap with the bubble gross methods does not exist but the fine and gross methods do meet if the proper limits are chosen for the fine leak tests.

D. MOS DIP (0.041 cc Internal Volume)

Figures 18-22 show that at an L value of 5×10^{-7} , the sensitivity range extends to 2.5×10^{-5} and that if an R value of 5×10^{-8} is used at standard bomb conditions (1 hour at 60 psig), this range is extended from 1.7×10^{-7} to 3.7×10^{-5} . The data verifies this because all of the devices in the 10^{-6} group were detected as leakers and the escape rate in the 10^{-5} group was 46%. If the 5×10^{-7} limit is used for Condition B, the sensitivity is reduced significantly because with this limit the 10^{-6} group had an escape rate of 43%, although the escape rate in the 10^{-5} was 50%, about the same as Condition A. If the current Condition B limit of 5×10^{-8} is used, the escape rate in the 10^{-6} group is 11%, again indicating that Condition B is slightly less sensitive than Condition A on a package of this volume.

The overkill rates on this package were 1% on Condition A and zero on Condition B.

There is an overlap with gross leak methods with this volume as indicated by approximately 50% of the devices in the 10^{-5} range being detected on both of the test conditions.

E. TO-100 (0.086 cc Internal Volume)

Figures 23-27 show that with the 5 X 10^{-7} L limit, the sensitivity extends to 7 X 10^{-5} and with the 5 X 10^{-8} limit at standard conditions the range is from 2 X 10^{-7} to 9 X 10^{-5} . The data indicates that this range is covered since the escape rates were 2% in the 10^{-6} group and 3% in the 10^{-5} group when the 5 X 10^{-7} L limit was used. Only 2% of the devices in the 10^{-4} group escaped which indicates that with a short t_2 time many gross leakers will be detected when Condition A is used. With the 5 X 10^{-7} baseline limit, the sensitivity of Co. dition B was significantly less than that of Condition A since 24% of the 10^{-6} group and 22% of the 10^{-5} group escaped. However if the 5 X 10^{-8} MIL-STD-883 limit is used these escape rates are reduced to zero

and 3% respectively. The escape rate in the 10^{-4} group was 3.5% with either of the limits which indicates good extension into this range.

The overkill factors were 1.4% for Condition A and 2.3% for Condition B which are about the same as experienced with other packages.

There is a good overlap with the gross leak conditions provided the proper fine leak reject limits are used. This is pointed out by the low escape rates in the 10^{-5} and 10^{-4} groups.

F. Ceramic Package (0.45 cc Internal Volume)

Figures 28-32 show that if the 5 X 10^{-6} L value is used, the sensitivity extends to 4 X 10^{-4} , and that if the 5 X 10^{-7} R value is used, the sensitivity range is from 2 X 10^{-6} to 5 X 10^{-4} at standard bomb conditions. The data failed to verify these sensitivity ranges. Escape rates ranged from 86% in the 10^{-6} group to 25% in the 10^{-4} group with 10^{-5} , 10^{-3} , and 10^{-2} groups falling between these extremes when the 5 X 10^{-6} L reject value was used. However if an L value of 1×10^{-6} is used, the escape rate drops to 1.4% in the 10^{-6} group to zero in all other groups including 10^{-2} . If the L value is further reduced to 7 X 10^{-7} , no escapes occur.

The sensitivity of Condition B was poor on this package because of the high surface count rate. Table XIV shows that the surface absorption causes indications of leaks in the 10^{-7} range through the first hour after removal from the bomb. This sorption on the actual devices varied over a wide range and by the time desorption occurred, the internal tracer gas level was reduced to a point

Table XIV. Surface Absorption on 1 X 1 Ceramic
Lids with Epoxy Sealant
(All Data X 10⁻⁸ atm cc/sec)

	Time to Read After Conditioning (Minutes)									
Ероху	1.5	30-35	60-65	90-95	120-125					
Α	40.0	20.0	10.0	4.0	2.0					
Α	40.0	19.0	9.0	3.0	1.0					
Α	39.0	19.0	9.0	3.0	1.0					
D	38.0	18.0	9.0	3.0	1.4					
D	40.0	20.0	9.0	2.5	1.0					
D	41.0	20.0	9.0	3.0	1.2					

A = Ablestick

D = Duraseal

which allowed the escapes. The situation is further complicated by some percentage of the beta particles apparently having sufficient energy to penetrate the ceramic. This part of the count cannot be differentiated from surface count.

There were no devices in this group in the fine-leak range so an overkill factor could not be established.

Test Condition A overlaps through the 10^{-2} range but the escape rates on Condition B require that the gross range be fully tested by other methods if Condition B is used.

G. TO-3 (1.07 cc Internal Volume)

Figures 33-37 show that if the L value of 5×10^{-6} is used, the sensitivity extends to 9×10^{-4} and that if the 5×10^{-7} R value is used, the range is from 2×10^{-6} to 1×10^{-3} . As with the large ceramic package, the data did not verify this range. The escape rate was 32% in the 10^{-5} group using the limits stated above. Escape rates in the 10^{-4} , 10^{-3} , and 10^{-2} groups were 5, 0, and 14% respectively. The escape rate is reduced to zero in the 10^{-5} group and 10% in the 10^{-4} group if the L limit is reduced to 5×10^{-7} .

The sensitivity range of Condition B was essentially the same as that of Condition A if the same baseline limit of 5 X 10^{-6} was used. The escape rate was 33% in the 10^{-6} group, 5% at 10^{-4} , zero at 10^{-3} and 28% in the 10^{-2} group. These escape rates are reduced to 11% in the 10^{-5} group and to zero in the 10^{-4} and 10^{-3} groups if the current specification limit of 5 X 10^{-8} is used.

Overkill rates were unacceptably high on this package, 11% on Condition A and 17% on Condition B. Further analysis of this test group indicated that the problem was caused by voiding in the weld flange area on the devices and not by the test conditions themselves.

The overlap with gross leak test conditions is good extending through the 10^{-3} range and well into the 10^{-2} range provided the proper fine-leak limits are used.

Maximum sensitivity in terms of extending Corditions A and B into the gross leak ranges is shown in Table XV. It requires that all Condition A limits be lowered and that Condition B limits for packages having internal volumes of less than 0.01 cc be lowered.

Table XV. Test Condition Limits Required to Achieve Minimum Escape Rates

	_	_	,						
10-3	1.07	8	ហ		7	=	C	0	11
}	-	4	100		18	25	ល	0	0
1 X 1 Geramic	15	В	ន		54	0	20	53	44
1 X 1 Geramic	0.45	4	100		-	0	0	0	0
TO-100	0.086	В	យ		0	ო	4	1	1
10	Ö	٨	5		•	٥	•	ı	ı
MOS DIP	0.041	8	S		-	20	55	1	ı
Š	ő	٩	; 0;		0	53	=	ı	ı
C-DIP	0.014	В	ហ		ო	i	65	I	1
<u>ن</u> 	0.0	7	10		9	1	20	1	ı
C-PAK	0.012	В	ιΩ		37	20	88	ı	j
-ਹੋ	0.0	٧	10		35	41	51	1	l
TO-84	900.0	8	••	_	0	81	1	ı	1
7.	ö	₫.			4	16	1	ı]
Package	Volume (cc)	Test Condition	L.mit (L or Q) X 10-8 atm cc/s	Escape %/Range	10-6	10-5	10-4	10-3	10-2

2. CONDITION A REPEATABILITY (TABLE V)

A. TO-84

Ninety-four percent of these devices read in the same leak rate decade on all four of the data runs. One of these failing to repeat was in the 10^{-5} range, four were in the 10^{-6} range, and only one in the $<10^{-6}$ range. Even though these readings failed to repeat, the device in the 10^{-5} range and three of those in the 10^{-6} range would have been rejected on all four of the test runs.

B. C-PAK

Overall repeatability on this ceramic package was very poor, only 26% of the devices had consistent readings on all four data runs. On the devices which had leak rates of $<10^{-6}$, however, the readings did repeat on 70% of the devices. The devices in this $<10^{-6}$ group which failed to repeat were called gross leakers on one of the tests and in the case of one device, two of the tests.

C. C-DIP

Overall repeatability on this package was 64% with a 71% repeatability on those devices having leak rates of $<10^{-6}$. As with the C-PAK, the cause of nonrepeatability in the fine-leak range was due to the devices being called gross leakers on one or more of the test runs.

D. MOS DIP

Eighty-nine percent of the devices in this group had readings which repeated on all four of the test runs. Eighty-seven percent of the devices in the $<10^{-6}$ range had readings which would have consistently rejected or accepted them to a 5 X 10^{-8} R criteria.

E. TO-100

Ninety-three percent of these devices had repeating readings in each of the test runs. All of the devices which failed to repeat were called rejects on one or more of the test runs.

F. 1 X 1 Ceramic

Fifty-six percent of the devices in this group had readings which could be termed repeatable. This seems low, but it must be pointed out that all the devices in this group had leak rates of 10^{-6} or greater. If one considers only those devices with leak rates of $<10^{-3}$, then 70% of the readings were repeatable and if the population is further reduced to include only those devices with leak

rates of $<10^{-4}$, 72% of the readings are repeatable. Eighty percent of devices in the 10^{-6} range had consistent readings in all four of the test runs.

G. TO-3

Eighty-five percent of this group had repeatable readings on all four of the test runs. Twenty-seven percent of those failing to repeat had leaks of 10^{-4} or larger and the rest were in the 10^{-6} range.

3. CONDITION B REPEATABILITY (TABLE X)

A. TO-84

Ninety-seven percent of the devices had readings which repeated on all four of the test runs. Those which failed to repeat with one exception were in the 10^{-5} range. More than 98% of the devices with leak rates of $\leq 10^{-6}$ had repeatable readings on all runs.

B. C-PAK

Sixty-five percent of these devices had readings which repeated in all four test runs. Sixty percent of the devices having leak rates $\leq 10^{-6}$ repeated each time; however, only 10% of those not repeating were in the $< 10^{-6}$ range.

C. C-DIP

Ninety-two percent had repeated readings in the four test runs. Those which failed to repeat were in the 10^{-5} and 10^{-6} ranges with some of the test runs classifying them as rejects and others as good devices to the present 5 X 10^{-8} specification limit.

D. MOS DIP

Ninety-six percent of the devices in this group had repeatable readings through the four test runs. Those which were nonrepeating were devices which shifted between the 10^{-8} and 10^{-7} ranges. If only the devices in the $\leq 10^{-6}$ range are considered, 95% had repeatable readings

E. TO-100

Ninety-seven percent of these devices had readings which repeated on all four test runs. Those not repeating were in the 10^{-6} range and were not detected as leakers on one or more of the test runs. The 97% is also true if only the devices in the $\leq 10^{-6}$ range are considered.

F. 1 X 1 Ceramic

Ninety-three percent of these devices had repeatable readings and with the exception of one device, the nonrepeaters were in the 10^{-2} , 10^{-3} , and 10^{-4} ranges. If only the 10^{-6} range is considered, 97% of the devices had repeatable readings.

G. TO-3

Ninety-eight percent of the devices had readings which repeated on all four test runs. Both of those not repeating were in the 10^{-6} range and were read in the 10^{-8} range on two of the four test runs. In the $\leq 10^{-6}$ range, the readings were 97% repeatable.

SECTION VI

SURFACE ABSORPTION

This phase of the study was conducted with 25 C-DIP lids, 30 1 X 1 ceramic lids, CV98 sealing glass, and Ableseal and Duraseal sealing compounds. The C-DIP and 1 X 1 packages will be discussed separately.

The 25 C-DIP lids were subjected to a 60 psig, 4-hour bomb in helium. Five each of the lids were read at intervals of 1, 30, 60, 90, and 120 minutes. Readings in each case were completed within 5 minutes. This procedure was used to negate the effect of previous vacuum cycles on the lids. The readings progressed downward from a maximum of 2.8 \times 10⁻⁸ at 1 minute to 3 \times 10⁻⁹ at 30 minutes to 3 \times 10⁻⁹ at 60 minutes to 5 \times 10⁻¹⁰ at 90 minutes to zero at 120 minutes. This indicates that surface sorption would be a problem only on marginal devices read immediately after removal from bomb if a limit of <5 \times 10⁻⁸ was being used.

This procedure was repeated with krypton-85 using a bomb time and pressure equivalent to a test with a 1×10^{-8} limit on a package of this volume. All 25 of the lids read zero at >1 minute so no further readings were taken. The vacuum cycle inherent in the Radiflo systems for storage of the krypton-85 evidently removes all gas which has been absorbed by the ceramic.

The C-DIP lids were then cured with the sealing glass by processing through a furnace at normal sealing temperatures. The lids were then rebombed at the same conditions used previously. There was not a significant change in the values. The maximum readings were: 3×10^{-8} at 1 minute, 4×10^{-9} at 30 minutes, 2×10^{-9} at 60 minutes, 5×10^{-10} at 90 minutes, and zero at 120 minutes.

The lids were then resubjected to the radioisotope test with significantly different results. The maximum readings were: 7.8×10^{-8} at 1 minute, 7.10^{-8} at 30 minutes, 5.8×10^{-8} at 60 minutes, 5.5×10^{-8} at 90 minutes, and 5.1×10^{-8} at 120 minutes. There were also lids that read zero and 1×10^{-8} at one minute, this led to an examination of the lids which showed seal glass voiding to be more pronounced in some than in others.

For the C-DIP package, it can be concluded that surface sorption is not a problem during helium testing if the test limit being used is in the 10^{-7} range but that it could result in overkill if the limit were less than 5 X 10^{-8} . The sorption resulting from voids in the sealing glass can result in overkill of this package at the normal 5 X 10^{-8} radioisotope limit.

Twenty-five of the 1 X I ceramic lids were subjected to the same initial procedures as were the C-DIP lids. The maximum readings after belium bomb were: 8×10^{-8} at 1 minute, 2.7×10^{-8} at 30 minutes, 2.2×10^{-8} at 60 minutes, 1.5×10^{-8} at 90 minutes, and 8×10^{-9} at 120 minutes. This indicates that the surface sorption would be a factor at limits of 1 $\times 10^{-7}$ or less. The lids all read zero after subjection to the radioisotope test. As with the C-DIP, this can be attributed to the vacuum portion of the Radiflo store cycle.

The lids were then divided into two groups with Ableseal strips being cured onto one group and Duraseal onto the other group. After subjection to the same helium bomb conditions, the maximum readings in the Ableseal group were: 2.1×10^{-6} at 1 minute, 1.2×10^{-6} at 30 minutes, 6.2×10^{-7} at 60 minutes, 4.5×10^{-7} at 90 minutes, and 2.5×10^{-7} at 120 minutes. In the Duraseal group the maximums were: 3.5×10^{-7} at 1 minute, 6.2×10^{-8} at 30 minutes, 3.5×10^{-7} at 60 minutes, 2.5×10^{-8} at 90 minutes, and 1.5×10^{-8} at 120 minutes. Similar results were obtained on the radioisotope test. The maximum readings in the Ableseal group were: 4×10^{-7} at 1 minute, 2×10^{-7} at 30 minutes, 1×10^{-7} at 60 minutes, 4×10^{-8} at 90 minutes, and 2×10^{-8} at 120 minutes. In the Duraseal group the maximums were: 4.1×10^{-7} at 1 minute, 2×10^{-8} at 60 minutes, 3×10^{-8} at 90 minutes, and 1.4×10^{-8} at 120 minutes. Voids in the scalant contributed to these values.

These results point out that each ceramic and sealing system must be evaluated to determine what the absorption problems are. Appropriate wait times must be established from out-of-bomb to read but must be kept within limits which will allow detection of the actual hermetic scal failures. It is apparent from this data that high overkill and/or escape rates can occur with large ceramic packages unless these absorption factors are considered.

The total data, C-DIP and large ceramic, also point out that no general rule can be applied and that each package having a different type of ceramic and/or different sealing material must be evaluated prior to starting a test program on the package.

SECTION VII

TEMPERATURE PRECONDITIONING

This phase of the study was conducted using the TO-100 and C-DIP units. The test was conducted by installing a heater inside a helium pressure bomb and maintaining temperatures of 50°C, 75°C, 100°C, and 125°C while bombing the units at 60 psig for 1 hour. Upon completion of the hour bombing, the units were tested while maintaining the specified temperature until time of reading. The units were then placed into a large brass fixture and heated to 75°C, 100°C, and 125°C. The units still in the fixture and at temperature were then subjected to a radioisotope test.

The test results are shown in Figure 56. The ceramic devices exhibited the same characteristics in both helium and krypton. That is, the devices characterized towards the gross end of the range at 25° C moved towards the finer end of the leak range at increased temperature. Devices which indicated leaks in the 10^{-6} and 10^{-7} atm cc/s range moved toward or into the 10^{-8} range. The metal can device leak rates tended to spread in helium as the temperature was increased, moving from the 10^{-6} and 10^{-7} range toward the 10^{-8} and 10^{-5} ranges. At 125° C the population showed a strong tendency to move back toward the fine end of the range. The same spreading occurred in krypton at 75° C as with the helium but further increases in temperature shifted the population toward the gross end of the range, resulting in significantly different distributions at 125° C.

The resulting conclusion is that temperature preconditioning does not improve the sensitivity of either of the fine leak test conditions. In fact, it adds a variable which would allow unacceptable ceramic devices to be accepted and causes some metal devices which are acceptable at room temperature to be rejected and others which should be rejected to be accepted. Because of these factors, temperature conditioning and/or testing is not recommended for microcircuit seal testing.

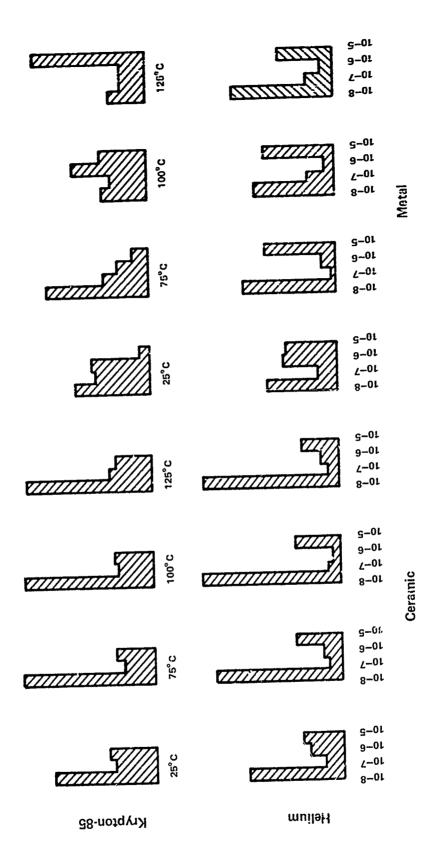


Figure 56. Temperature and Leak Rates

SECTION VIII

GETTERING EVALUATION

This phase of the study was conducted to determine the feasibility of using encapsulated in or bombed in gettering materials to detect gross leakers by either the helium or radioisotope fine-leak conditions. Polyimide, FC-48 fluorocarbon, PP-9 fluorocarbon, and vacuum pump oil were evaluated as gettering agents. The package types used were the TO-84, the C-PAK, and the MOS DIP. The evaluation of the fluorocarbons utilized 100 devices of each package type. The polyimide evaluation was conducted on 100 C-PAK devices and the vacuum oil evaluation was conducted with ten MOS DIP packages. Small volume packages were used because normal Condition A and B escape rates in the gross range are much higher than with relatively large volume packages.

The C-PAK devices containing polyimide were rejects from a special process line. They were screened and categorized by the procedures described in the discussion of Screening and Fabricating Leakers. The leak rate categories of the devices are shown in Table I. The devices were tested at the standard conditions of Conditions A (helium) and B (radioisotope).

The helium results are shown in Table XVI. There was a noted improvement in terms of escape rate in the 10^{-6} and 10^{-5} ranges over those devices which did not contain polyimide. The escape rate in the 10^{-6} group was 6% where it was 41% in the ungettered group. In the 10^{-5} group, the devices containing the polyimide had an escape rate of 33% and the ungettered group had an escape rate of 42%. There was also a marked change in overhill rates however. The nongettered group had a 5% overkill rate, this increased to 18% with the use of the polyimide.

Table XVI. Overkill and Escape Rates with Getters Using Helium

	Polyimide	FC-48	PP-9
Overkill %/Range <10-6	18	0	0
Escape %/Range 10 ⁻⁶	-	-	
10~5	6	91	100
10 - 0	33	88	100
10 ⁻⁴ 10 ⁻³	100	100	85
10~3	100		-

The radioisotope results are shown in Table XVII. The improvement in escape rate in the 10^{-6} range was very significant. The escape rate in the 10^{-6} range was zero as compared to 37% in the ungettered devices. In the 10^{-5} group, the escape rates were 17% for the gettered devices and 20% for the ungettered ones. The overkill rate in the gettered group was 2%.

Table XVII. Overkill and Escape Rates with Getters Using Krypton-85

Polyimide	FC-48	PP-9
2	10	2
į		
0	48	36
17	54	67
100	22	30
96		_
	2 0 17 100	2 10 0 48 17 54 100 22

The TO-84, C-PAK and MOS DIP devices which were used to evaluate the fluorocarbons are the same ones used in other phases of the investigation. Their leak rate values are shown in Table I. They were processed in the following manner.

The devices were placed in a pressure vessel and the pressure reduced to 1 torr, this condition was maintained for 1 hour. The fluorocarbon which had been preconditioned by bubbling helium through it was then introduced into the vessel without breaking the vacuum. It was pressured to 60 psig with helium and this condition was maintained for a period of 2 hours. Each unit was allowed to air dry for a period of 2 minutes prior to testing to allow the fluorocarbon on the external surfaces to evaporate.

Results were negative in that the escape rates were much higher in the gross ranges than when no gettering was used. In the 10^{-6} range, the escape rates were 91% with FC-48, 100% with PP-9, and 41% with no getter. This was caused by fluorocarbon vaporization during the initial pump-down of the mass spectrometer which resulted in excessively long pump-down times being required for the machine to reach test vacuum levels. With the MS-90 UFT system, this results in all devices being classified as gross leakers.

After a 16-hour vacuum bake which was also used between each FC-48 and PP-9 test run, the devices were subjected to the radioisotope test. The devices were baked at 100°C for 1 hour and immediately immersed in the fluorocarbon when removed. After 30 minutes in the fluorocarbon, they were removed, allowed to air dry for 2 minutes, then bombed in krypton-85 at the 1 X 10⁻⁸

conditions for each package. The escape rates were not improved over the no gettering process; in the 10^{-6} group, the escape rate was 48% with FC-48, 36% with PP-9, and 37% with no gettering.

The MOS DIP devices, which had been specially prepared by drilling a hole in each lid, were used to evaluate the vacuum pump oil. This was done to prevent the test samples used for the other phases from possibly being contaminated rendering them unusable for further testing. The devices were baked at 100°C for a period of 1 hour and immersed in the vacuum pump oil. After 30 minutes they were removed and the external oil removed with freon. The devices were then bombed with krypton-85 at conditions equivalent to 1 X 10⁻⁸ Condition B test. All of the devices were detected as leakers when they were read after removal from the bomb.

It was noted that oil had leaked out of some of the devices contaminating the surface of other devices. In a normal distribution of devices this might result in overkill but could be prevented by proper holding fixtures for use in the pressure vessel.

None of the gettering agents proved to be feasible from a production standpoint. The fluorocarbons were ineffective, the polyimide allowed all or most leakers in the 10^{-4} and 10^{-3} ranges to escape, and the vacuum pump oil process is not cost-effective because of the clean-up procedures required to assure that all oil is removed from the external surfaces prior to exposure to the tracer gas.

The data indicate however that an agent which could be encapsulated into the device and which had better gettering characteristics than the polyimide would work. The polyimide significantly reduced the escape rates in the 10^{-6} range; therefore it is reasonable to assume that a material which would absorb better would improve the escape rates in larger leak rate ranges. The data also indicate that a material which had the gettering characteristics of the vacuum pump oil and which could be removed from the external surfaces by an inexpensive process could be successfully used to detect gross leakers with the fine leak test conditions.

SECTION IX

CONTROLLED ORIFICE EVALUATION

This phase of the study was devoted to an evaluation of using a mass spectrometer to detect gross leaks by using an orifice at the input to limit the flow of tracer gas into the machine. It was assumed that if a constant pressure, having a magnitude that would allow the spectrometer to remain in the "Test" mode, could be maintained, that gross leakers could be detected. This would be accomplished by constantly monitoring the gas flowing out of the device through the orifice from the time the device was inserted in the fixture rather than having to wait until the fixture cavity was pumped down after insertion. This delay to pump down the fixture is believed to contribute to gross leaker escapes by allowing the helium concentration in the device to reach a nondetectable level before the machine reaches test pressures.

A special test fixture having two ports was fabricated for this evaluation. One of the ports was connected to the intake manifold of the mass spectrometer through a Veeco type VV-5') adjustable leak valve which was used as the orifice The other port was connected to the manifold of the mass spectrometer through a Hoke valve. This arrangement is shown in block form in Figure 57.

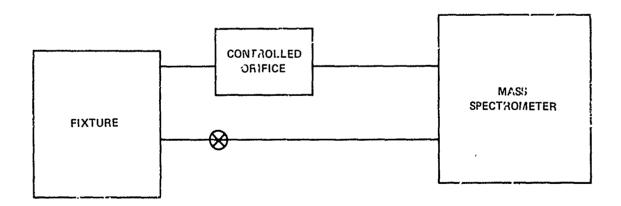


Figure 57. Block Diagram of Controlled Orifice Test Setup

The test sequence used was to bomb the device in helium, insert it in the fixture immediately upon removal from the bomb, read the device through the orifice (Hoke valve closed), and if no indication of a gross leak occurred, then read through the no-orifice line. The devices were left connected through the orifice for a period of 1 minute and were classified as gross leakers if the reading increased one major scale division within the period. For example, if the reading was 5×10^{-8} at time zero, the device was rejected if the reading increased to 6×10^{-8} during the 1-minute period.

Three metal can package types were used for this evaluation, the TO-84, the TO-100, and the TO-3, in order to cover a large internal volume range. The TO-84s were subjected to three test runs and the other packages to one test each, making a total of 500 test samples. All devices were bombed at 60 psig in helium, the TO-84s for 2 hours, and the larger packages for 1 hour.

The results are shown in Table XVIII. The method did detect some of the TO-84 gross leakers which had been missed when the orifice was not used, however the escape rate was still 38%. The test was less effective on the other packages yielding larger escape rates than had occurred without the orifice being used. The overkill rates were very high, 9% on the TO-84, 51% on the TO-100 and 35% on the TO-3.

Table XVIII. Overkill and Escape Rates Using Controlled Orifice Helium Testing

	TO-84	TO-100	TO-3	
Overkill %/Range <10 ⁻⁶	9	51	35	
Escape %/Range ≥10−6	38	26	67	

These facts, high escape rates, and high overkill rates coupled with the longer time required to test each unit led to the conclusion that controlled orifice testing would not provide any effectivity improvement for microcircuit seal testing.

SECTION X

INTRODUCTION TO GROSS LEAK TEST CONDITIONS C AND E

The object of this part of the study was to evaluate Test Condition C of MIL-STD-883, Method 1014, and the proposed weight gain test, Condition E. The units which were used in the valuation of Test Conditions A and B were used for this study also. Prior to starting the study, all leak rate values were verified to ensure that the units had not plugged or opened-up in such a way as to give erroneous indications. The units were grouped and retained the original SN, although the L value may not have remained the same. The number of devices in each leak rate decade is shown in Table XIX. This study was conducted using the following fluorocarbons:

3M	Flutec
FC-40	PP-9
FC-78	PP-1
FC-77	PP-2

The purpose of using six fluorocaroons was to determine if there was an optimum fluid or combination of fluids for Condition C or Condition E. In order to perform the testing with a minimum probability of damage to the units, the following test sequence was followed:

- 1. C₁ bubble
- 2. Weight gain
- 3. C₂ bubble

Table XIX. RADC Microcircuit Leak Fate Values (Condition C and E)

TO-84	% by % TO-84 All Ceramic (C-PAK)		Ceramic Dual In-Line (C-DIP)		MOS Dual-In-Line (MOS DIP)		
	No.		No.		No.		No.
Leak Rate	Units	Leak Rate	Units	Leak Rate	Units	Leak Rate	Units
<10-6	57	<10-6	10	<10-6	45	<10-6	60
10-6	6	10-6	47	10-6	18	10-6	14
≥10 ⁻⁵	36	10-5	16	10-5	0	10-5	6
		>10−4	27	≥10 ⁻⁴	14	≥10-4	20
Total	96	Total	100	Total	77	Total	100
7O-10	Ceramic TO-100 1 Inch by 1 Inch		TO-3.		Glass Standards		
<u> </u>	No.		No.		No.		No.
Leak Rate	Units	Leak Rate	Units	Leak Rate	Units	Lea!: Rate	Units
<10-6	56	106	35	<10-6	45	<10-6	5
10-6	16	10-5	1	10-6	25	10-6	9
10-5	6	10-4	4	10-5	9	10-5	16
≥10-4	1	10-3	15	10-4	10	≥10−3	20
		10-2	16	19-3 10-2	3 8		
Total	79	Total	71	Total	100	Total	50

SECTION XI

EVALUATION OF TEST CONDITION C

This phase was performed in two parts, part one was the evaluation of Condition C_1 and part two the evaluation of Condition C_2 . This phase was conducted using four different fluorocarbons.

3M	Flutec
FC-40	PP-9
FC-78	PP-1

C₁ evaluation was performed by subjecting each package to two test sequences using FC-40 and two test sequences using Flutec PP-9. The test was performed by immersing the uppermost portion of the unit to a minimum of two inches below the surface of the fluid. The fluid was maintained at a temperature of 125 ± 5°C during this test. The units were observed at a magnification of 3X and any unit which produced a stream of bubbles or a growing bubble was considered a reject. Surface bubbles or trapped nongrowing bubbles were not considered cause for rejection The devices were observed against a dull, nonreflective black background for a period of 30 seconds in the center of a collimated light beam. Each unit was recorded as good or reject by serial number.

Each group of devices was tested two times in the FC-40 fluid and two times in the PP-9 fluid at the conditions described above. The results by package type are shown in Table XX. The C_1 test has been assumed to be sensitive from 10^{-3} through 10^{-1} leak sizes. Only two of the sample groups contained devices known to be in the 10^{-3} and 10^{-2} ranges. One other group, the glass standards, contained devices in the 10^{-3} range but none in the 10^{-2} decade. The data indicate that under ideal conditions (i.e., the glass standards with no weld flanges or seal interfaces) the method is sensitive in the 10^{-3} decade. No escapes occurred in this range on these devices. However, escapes did occur in both the 10^{-3} and 10^{-2} groups on the TO-3 and 1 X 1 ceramic packages. In the TO-3 package group, 33% of the devices in each decade escaped in either of the test fluids. The ceramic escape rates were significantly less, 3.3% and 6.5% with FC-40 and 6.6% and 0% with the PP-9.

The data also indicate that the test condition sensitivity extends into the 10^{-4} and 10^{-5} decades. For example, on the TO-84 package, the escape rates were 8.4% with FC-40 and 9.7% with PP-9 in the 10^{-5} decade. Similar observations can be made on each of the other package types (Table XX). The overkill rates (devices in the less than 1×10^{-5} leak size group which were rejected for bubbles) varied with the package type. These rates are higher on ceramic packages than

Table XX. C₁ Escape and Overkill Rates in FC-40 and PP-9

Package	10-84	84	C-PAK	¥	C-DIP	4	MOS DIP	DIP	TO-100	8	1 X 1 Ceramic	1 nic	10-3	8	Glassa	s
Fluid	FC-40	6- d d	FC-40 PP-9	6-dd	FC-40 PP-9	6-4d	FC-40 85-3	5:40	5C.40	6.99	FC-40	PP-9	FC-40	6-dd	FC-40	PP-9
Overkill %/Range <10 ^{–5}	-1	4.8	18	25	11	41	13	20	2	2	4	67	45	8	ري دي	o
Escape %/Range 10-5	8.4	9.7	88	34	1	J	33	25	20	42	0	0	20	55	6.3	6.3
4	ı	ł	జ	6	14	4	12	S	0	8	25	25	စ္က	45	ı	1
ဗု	ı	l	ı	ı	1	1	1	ı	ı	1	3.3	9.9	33	33	0	0
-5	l	ı	ı	i	1	ì	ı	í	i	ı	6.5	0	33	33	ı	1
	-	_	_	•	-	_	-		-	•	-	-	_	-	•	-

on metal packages with the exception of the TO-3 which had a large weld flange area from which bubbles emanated. For example, the overkill rates on the C-DIP were 11% in FC-40 and 14% in PP-9 versus 2% in FC-40 and 10% in PP-9 on the TO-100 package.

To determine whether or not there was a significant difference in the two fluids used, the data on all of the devices were compiled to determine overall escape and overkili rates. This is shown in Table XXI.

Table XXI. Comparison of FC-40 and PP-9 on Total Sample Population

	3M FC-40	Flotec PP-9
Overkill %/Range		
<10 ⁻⁵	18	22
Escape %/Range		
10-5	21	21
10-4	16	16
10-3	8.4	11
10 ⁻⁵ 10 ⁻⁴ 10 ⁻³ 19 ⁻²	32	24

The overkill rate was 18% in the FC-40 and 22% in the PP-9. The escape rates are 21% in each fluid in the 10^{-5} range and 16% in each fluid in the 10^{-4} range. In the 10^{-3} group the escape rates were 8.4% in FC-40 and 11% in PP-9. In the 10^{-2} group the rates were 32% in FC-40 and 24% in PP-9 but the data base in this decade (24 devices) is too limited to draw a firm conclusion as to whether one fluid is better than the other in this range.

Repeatability, the ability to detect or accept specific devices in a leak range, was very poor. This is pointed out by the large overkill and escape percentage shown in Table XX. The ability of the test condition to detect a "bubble" or "no bubble" condition consistently when subjected to four test runs was poor. Table XXII shows the repeatability of the condition for the devices with leak rates $\geq 10^{-5}$ and the overall results even though the effectivity is very poor in the 10^{-4} and 10^{-3} ranges. The table shows that for the TO-84 and the C-DIP package the ability to produce consistent bubble or no bubble results is much better than the ability to detect all the units in a range. For example the overkill and escapes on the TO-84 in FC-40 was 11% and 8.4%, but the bubble, no bubble results were 96%. The C-DIP results showed 11% and 14% overkill and escape with a bubble no bubble result of 100% and 94%.

Table XXII. C1 Gross Leak Repeatability

Package	>13 ⁻⁵ (%)	(%) Dressig
TC-8:	95	92
JPA%	54	49
CDIS	100	29
MOS DIP	න	69
TO-109	94	72
1 X I Ceramic	e 5	52
то-з	35	40
Gim	Şa	9 .

The data resulting from these tests indicate there is not a significant difference in the test fluids. Either 3M FC-40 or Flutec PP-9 can be used to conduct the test. It also shows that although the sensitivity extends into the 19⁻⁵ range, the test cannot be termed reliable because of the escape rates which occur in the larger leak rate decades and because of the overkill rates which occur with some package types.

The overkill problem discussed above was also reported by Raytheon in the paper "Raytheon Weight Test Method for Detecting Gross Leaks in Small Internal Volume Semiconductor Packages." The overkill rates reported in the paper were higher than those experienced during this investigation. The overkill rate could be reduced by using only a "steady stream of bubbles" as the reject criteria but there is an associated risk of increasing the escape rate.

it must be concluded that Test Condition C_1 will have some escape rate and some overkill rate even under carefully controlled conditions.

C₂ evaluation was performed by subjecting each unit to two test sequences using 3M FC-78/FC-40 combination and two sequences using Flutec PP-1/PP-9 combination. The procedure was as follows: The units were placed inside a vacuum/pressure bomb and the pressure reduced to 1 terr and maintained for 1 hour. Without breaking the vacuum, the fluid (FC-78 or PP-1) was admitted to the bomb. Devices with internal cavity volume equal to or less than 0.1 cc were then pressurized to 90 psig with dry nitrogen. Devices with an internal cavity volume greater than 0.1 cc were pressurized to 50 psig. The pressure was maintained for a period of 3 hours. The units were then removed from the bomb and retained in a bath containing the bomb fluid (FC-78 or PP-1). The units were removed from the bath and allowed to dry 3 ± 1 minute in the air prior to immersion in the indicator fluid. The units were immersed a depth of 2 inches below the surface of

the indicator fluid (FC-40 or PP-9). The indicator fluid was maintained at a temperature of $125 \pm 5^{\circ}$ C during the testing. The units were observed at a magnification of 3X and any unit which produced a stream of bubbles or a growing bubble was considered a reject. During this test procedure, as with the C_1 procedure, a surface or trapped bubble was not considered a reject. The devices were observed against a dull, nonreflective black background for a period of 30 seconds in the center of a collimated light beam. Each unit was recorded as good or reject by serial number.

The results show that Condition C_2 detects most of the leaking devices in the 10^{-5} and larger ranges (Table XXIII). The exceptions are the TO-84, 1 X I ceramic, and TO-3 packages. The escapes on the TO-84 package are probably due to the small volume of liquid inside the package vaporizing and blowing out of the package before the device is completely submerged in the fluid. Failure to monitor the device from the time of entry into the fluid allows a greater number of devices to escape. The results show that approximately 40% of the devices in the 10^{-6} range were detected as rejects, which indicates the method does extend into the 10^{-6} range. However, it cannot be termed a reliable method in this range because of the 60% which escaped. The overkill was much higher on the TO-3 than any of the other packages. This is probably due to a wide seal flange area containing weld voids. The results also show a high escape rate in the 10^{-3} and 10^{-2} ranges on the 1 X 1 ceramic and TO-3 devices. It could not be determined if these same escape rates would apply to the smaller volume packages as none of the small volume devices leaked in the 10^{-3} or 10^{-2} range.

Repeatability, the ability to detect specific devices in a leak range, was good for leak rates $\ge 10^{-5}$. The devices in the $\le 10^{-6}$ did not produce results as good as the results of the gross leakers (Table XXIII). The ability of the condition to produce consistent "bubble," "no bubble" results over four test runs was good. Table XXIV shows that the condition has a high percentage of repeatability with respect to consistently detecting bubble, no bubble conditions for units with leak rates $\ge 10^{-5}$ with the exception of the TO-3 package. The overall results are not as good, which indicate that the condition produces most of the erroneous results in the $\le 10^{-6}$ leak ranges. This is also shown in Table XXIII.

The overall test results indicate there is no significant difference in the fluids (Table XXV). Either combination can be used for Condition C_2 testing.

One test run in each of the fluid combinations was conducted without the vacuum cycle but with the bomb pressure increased one atmosphere above specification values. The results indicate that escape rates are higher on packages having an internal volume of <0.10 cc if the vacuum cycle is omitted. There is no significant difference on packages having volumes larger than 0.10 cc.

It can be concluded that Condition C_2 is more effective and repeatable than Condition C_1 . If Test Condition C_2 is used, it is not necessary to run Condition C_1 .

Table XXIII. C_2 Escapes and Overkill Rates in FC-78/FC-40 and PP-1/PP-9

	**	ırds	PP-1/		6:44			ç	3	1	ຊ	ı	•	>	Ç	?	,	
	Glass	Standards	FC-78/ PP-1/		70.45 64			ç	2	1	26	1	ç	2.5	Ť.	?	,	
		3	/1.dd		6.dd				35		14	88	Ş	2	_	,	28	
		10.3	FC-78/ PP-1/	;	FC-40			;	44		19	22	,	2	c	>	22	
	1	nic	7b-4d	- :	PP-9				ı		45	0	ļ	22	U		0	
	1 × 1	Ceramic	FC-78/	;	FC-40				ì		99	0	-	22	ç	2	က	
		8	71.00		PP-9				53		??	رع		0		ı	1	
		TO-100	CC.79/ DD.1/	2	FC-40				12		27	α	ì	0		1	1	
		010	11.00		6-dd				8.4		32	25	?	0		1	ı	
		MOS DIP	100 100 11/	ر د د	FC-40				52		42	α	;	വ		1	1	
		<u>a</u>	1	-	PP-9				10		28	ļ		7		1	1	
		C-DIP	102	75.78/	FC-40				14		64	!	1	0		ı	i	
l		¥			6-dd				90		38	0	9	0	,	1	1	
		C.PAK		18/01	FC-40				20		37	, (2	c	,	1	ı	
		78		FC-78/ PP-1/	6-dd	- 1			23		25	}	>	1		ı	1	
		TO.84	2	FC-78/	FC-40			_	23	 	42	!!	2	ı		1	1	
		O Constant	rackaye	Fluid			_	Overkill %/Range	<10-6	Escape %/Range	9-01	2 !	5_01	10-4		10-3	10-2	?

Table XXIV. C₂ Gross Leak Repeatability

Packag e	>10 ⁻⁵ (%)	Overall (%)
TO-84	88	70
C-PAK	93	73
C-DIP	93	79
MOS DIP	85	69
TO-100	94	78
1 X 1 Ceramic	92	70
то-3	78	65
Glass	96	94

Table XXV. Comparison of Test Fluids FC-78/FC-40 and PP-1/PP-9

Fluid	FC-78/FC-40	PP-1/PP-9
Overkill %/Range <10 ⁻⁶	26	21
Escape %/Range		
10-6	41	30
10-5	5	3.4
10-4	2.3	2
10-3	4.2	2.8
10-3 10-2	10	20

SECTION XII

EVALUATION OF CONDITION E

In preparation for evaluating the weight gain test, the fluid flow rate through leak sizes in the gross range versus pressure was determined. The leak size at which fluid flow ceases was also determined. A control valve (Veeco type VV-50) was used to provide verifiable leak sizes which were measured with the MS-12 mass spectrometer. The equation

$$R = \frac{LP_E}{P_O} \left(\frac{M_A}{M} \right)^{1/2} \left\{ \left[1 - e^{-\frac{Lt_1}{VP_O} \left(\frac{M_A}{M} \right)} \right]^{1/2} \right\}$$
 (11)

is obtained from Equation (1) and defines the indicated leak rate of the device at the end of the bomb period. The system used allowed the volume of gas inside the control valve to become ∞ . This makes e^{-x} approach zero and makes the portion of the equation inside the braces equal to one. A pressure bottle with a regulator was used to supply the helium to the inlet side of the orifice with the outlet side under vacuum. A vacuum had been pulled on the inlet side of the orifice to remove the normal air prior to introduction of the helium. Therefore, the atmosphere was approximately 100% helium at 1 atmosphere. The expression

$$e^{-\left[\frac{LP_{E}}{P_{O}}\left(\frac{M_{A}}{M}\right)^{1/2}\right]}$$
 (A)

defines the escape rate of the gas through the orifice. The regulator and pressure bottle kept the amount of helium to the orifice constant. Therefore, time t_2 was always effectively 0, making the expression equal to 1. Now the equation can be written as:

$$R = \frac{LP_E}{P_O} \left(\frac{M_A}{M}\right)^{1/2} [1] [1]$$

This allowed the valve to be set to exact L values by adjusting the valve to produce the proper R value at each test pressure (30, 60, 90 psig).

The valve was plumbed in such a way as to allow helium, liquid, vacuum or a drain to be applied at the inlet of the valve. The outlet of the valve fed directly to a glass vial which was fitted tightly to the valve. By removing the glass vial, the outlet could be connected to the Veeco machine. The valve was mounted in such a way that it could be rotated to drain the fluid at the end of each test point.

The procedure for setting and checking an R value was as follows:

- 1. With the control valve outlet connected to the mass spectrometer, the inlet was subjected to a vacuum.
- 2. With the inlet under the vacuum, helium was supplied to the inlet at a pressure set to approximately 1/4 psig. This ensured a 100% helium atmosphere supplied to the orifice.
- 3. The orifice was adjusted to L values ranging from 3 X 10^{-4} to 1 X 10^{-6} .
- 4. The pressure was removed and the inlet side of the valve pressure was reduced to the vacuum condition.
- 5. The line from the valve outlet to the mass spectrometer was removed and a glass vial was attached.
- 6. With the inlet still under vacuum, the fluid FC-78 was admitted to the inlet side and pressurized to the value of interest (30, 60, or 90 psig). The maintenance of vacuum until the fluid was introduced ensured that trapped air did not produce erroneous readings.
- 7. The time of pressurization was measured with a stopwatch and varied from 40 minutes to 6 hours. The times were varied to provide several data points for each leak size at each pressure. Accuracy of the data was assured if the flow rate in mg/min did not vary with total time.
- 8. Upon completion of the dwell time, the vial was removed and the amount of fluid the vial had gained was determined by using balance scales which would measure to 0.1 milligram. From this data the gain in milligrams per minute was determined.
- 9. To ensure that the leak rate had remained constant, the pressure was removed from the inlet and the fluid drained from the valve. Then the inlet was subjected to a vacuum in order to evaporate all of the FC-78.

10. The valve was then connected to the mass spectrometer and while under a vacuum, helium was supplied to the inlet at approximately 1/4 psig. If the reading did not repeat, the data point was considered to be in error. The valve setting was not adjusted in any way after the initial setting until completion of verifying the L value after the flow rate was determined.

The above procedure was performed for each data point at each pressure and plotted on the curves (Figure 1).

The testing was performed in the following manner: Each device was weighed and this initial weight recorded. The units were then placed inside a vacuum/pressure bomb and the pressure reduced to 1 torr. This pressure was maintained for 1 hour. The indicator fluid (FC-78, FC 77, PP-1, or PP-2) was then admitted to the pressure bomb without breaking the vacuum and the pressure increased to the desired value (30, 60 or 90), which was maintained for 2 hours. Upon completion of the 2-hour period, the devices were removed from the bomb and maintained in a bath of the indicator fluid. They were then removed from the bath and allowed to air dry for 3 ± 1 minute prior to being reweighed. The delta weight was determined for each device and recorded along with the weight gained per minute value for devices that did not fill. The fluid flow rate for a 2×10^{-6} leaker was then taken from the graphs (Figure 1) and the weight calculated that a device would gain in 2 hours with this leak rate. All devices that gained at least this amount were classified as leakers. The devices that gained less than the calculated amount were considered to be acceptable. It was assumed that any weight less than the calculated value was a combination of scale repeatability, surface retention of fluid, and fluid inside the seal area.

The weight gain test was performed to provide answers to the following questions:

- 1. What is the best fluid?
- 2. What is the best test pressure?
- 3. What is the sensitivity of this test?

To determine the best fluid, all devices were subjected to a test sequence using FC-78, FC-77, PP-1, and PP-2. The bomb pressure in all cases was 60 psig, with a bomb time of 2 hours. The data showed that FC-78 provided lower overkill and escape rates than did any of the other fluids (Table XXVI). The remaining tests were performed using FC-78 because of better escape and overkill rates shown in Table XXVI.

The devices were then subjected to a test sequence at pressures of 30, 60, and 90 psig. The test result. snow that the weight gain test is effective for all package types in the 10⁻⁻⁵ and larger range. Tables XXVII through XXXIV list the results for individual package types. The preceding statement

Table XXVI. Comparison of Fluids at 60 psig with a Reject Limit Equal to L of 2 X 10^{-6} which is 4.8 Mg Gain

Fluid	FC-78	FC-77	PP-1	PP•2
Overkill %/Range			,	
<10-6	5	10	8.4	5.8
Escape %/Range				
10-6	69	70	62	70
10 ⁻⁵	1.1	5	1.1	1.7
10-4	1	3.5	1	1.5
10-3	0	2.7	2.7	2.7
10 ⁻⁵ 10 ⁻⁴ 10 ⁻³ 10 ⁻²	0	0	4	8

Table XXVII. Escape and Overkill Rates at Varying Pressures and Limits, TO-84

Pressure	30	60	90	60	90
Reject Limit Milligrams	0.78	4.8	8.3	0.7	0.9
Overkill %/Range <10 ⁻⁶	3.5	0	1.8	7.0	12
Escape %/Range 10-6 10-5	83 0	67 2.8	£3 8.5	33 0	33 0

Table XXVIII. Escape and Overkill Rates at Varying Pressures and Limits, C-PAK

Pressure	30	60	90	60	90
Reject Limit Milligrams	0.78	4.8	8.3	1.0	1.0
Overkill %/Range					
<10 ⁶	40	0	30	20	50
Escape %/Range					
10-6	55	62	47	50	36
10-5	32	0	12	0	12
10-4	7.5	0	0	0	0

Table XXIX. Escape and Overkill Rates at Varying Pressures and Limits, C-DIP

Pressure	30	60	90	60	90
Reject Limit Milligrams	0.78	4.8	8.3	1	1
Overkill %/Range <10 ⁻⁶	11	2.2	2.2	13	18
Escape %/Range					
10-6	70	89	84	39	33
10-5	_	-	-		-
10-4	7	7	7	0	0

Table XXX. Escape and Overkill Rates at Varying Pressures and Limits, MOS DIP

Pressure	30	60	90	60	90
Reject Limit Milligrams	0.78	4.8	8.3	0.9	2
Overkill %/Range <10 ⁻⁶	21	1.5	1.5	8.4	11
Escape %/Pange					
10-6	20	63	50	35	14
10-5	17.	0	0	0	0
10-4	0	5	0	0	0

Table XXXI. Escape and Overkill Rates at Varying Pressures and Limits, TO-100

Pressure	30	60	90	60	90
Reject Limit Milligrams	0.78	4.8	8.3	1	1
Overkill %/Range <10 ⁻⁶	8	3.6	0	12	7
Escape %/Range					
10~6	50	76	76	37	50
10-5	0	0	0	0	0
10-4	0	0	0	0	0

Table XXXII. Escape Rates at Varying Pressures and Limits, 1 X 1 Ceramic

Pressure	30	60	90	60	90
Reject Limit Milligrams	0.78	4.8	8.3	1	1
Overkill %/Range					
<10-6	_	-	-		-
Escape %/Range					
10-6	95	92	80	92	56
10-5	0	0	0	0	0
10-4	25	0	25	0	25
10-3	6.6	0	13	0	13
10-2	12	0	12	0	12

Table XXXIII. Escape and Overkill Rates at Varying Pressures and Limits, TO-3

Pressure	30	60	90	60	90
Reject Limit Milligrams	0.78	4.8	8.3	1	1
Overkill %/Range					
<10-6	16	2.2	4.8	20	28
Escape %/Range					
10-6	15	23	30	3.8	3.8
10-5	0	10	0	0	0
10-4	0	0	0	0	0
₁₀ –3 10–2	0	0	0	0	0
10-2	0	0	0	0	0

Table XXXIV. Escape and Overkill Rates at Varying Pressures and Limits, Glass

Pressure	30	60	90	60	90
Reject Limit Milligrams	0.78	4.8	8.3	1	1
Overkils %/Range					
<10 ⁻⁶	0	0	0	20	0
Escape %/:tange					
10-6	100	100	100	67	100
10-5	63	0	0	0	0
10-4			-	_	_
10-3	0	0	0	0	0

is based on the 60 psig data using the so-called optimum limits. It should be noted that no escapes (Table XXXV) occurred in the 10^{-5} or larger ranges under these conditions. Overkill rates were slightly higher at these conditions but it must be remembered that these are not normal distributions of devices and therefore many of the "fine leakers" had values larger than fine-leak test limits. Under normal conditions, the overkill rates should be lower because these devices would have been rejected at the fine-leak test.

Table XXXV. Weight Gain, Escape and Overkill Rates at Fill Rate and Optimum Limits

Pressure	30	60	90	60	90
Reject Limit Milligrams	0.78	4.8	8.3	1.0	1.0
Overkill %/Range					
<10-6	13	5	2.9	12	16
Escape %/Range					
10-6	58	69	62	48	48
10-5	3.8	1.1	1.1	0	1.1
104	2	1	1	0	0.5
10-3	2.8	0	5.5	0	5,5
10-2	8	0	8	0	8

This method is not effective for the entire 10^{-6} range, as escape rates are 69% and 62% at 60 and 90 psig respectively. The results can be greatly improved by lowering the reject limits to the optimum conditions as shown in Table XXXV. If these limits are used, the escape rates will be lowered to 48% and 38% at the 60 and 90 psig test pressures. This points out that 90 psig is more effective in the 10^{-6} range, however the 90 psig condition allows escapes in the 10^{-5} and larger range which are detected when 60 psig is used. The additional devices detected in the 10^{-6} range are believed to be those with leak rates near the fluid flow cut-off point. These devices would normally be detected by fine-leak conditions since the flow rate data indicates that their leak rates are 2×10^{-6} or smaller. Based on the above, 60 psig appears to be the optimum pressure for the weight gain test.

The results of the no-vacuum cycle indicated that for the TO-84 package with a volume of 0.006 cc, the number of escapes increased by 20. The C-PAK overall results were essentially the same as five additional units that were detected and six units that were detected before escaped. The C-DIP results allowed six additional escapes with no additional detections. The MOS DIP resulted in six additional escapes and one additional detected. The TO-100, 1 X 1 ceramic, TO-3, and glass packages had no significant difference in the results. It can be concluded that the vacuum cycle is necessary for packages with a volume smaller than 0.10 cc (Table XXXVI).

^{*1.0} Milligram

Table XXXVI. Comparison of Results at 90 psig With Vacuum and 105 psig Without Vacuum

Device Type	No. of Rejects Detected at 90 psig	No. of Escapes at 105 psig Which Were Detected at 90 psig	No. of Rejects at 105 psig Which Were Accepted at 90 psig
TO-84	34	20	1
C-PAK	64	6	5
C-DIP	20	6	0
MOS DIP	33	6	1
TO-100	12	1	0
1 X 1 Ceramic	37	2	2
TO-3	49	0	3
Glass Standard	36	2	0

It can be concluded that the weight gain test (Condition E) is the most effective of the Gross Leak Methods when conducted at the specified limits. Figure 1 shows that five times more fluid is forced into the device when bombed at 60 psig than when bombed at 30 psig. This indicates that if 30 psig is used as the bomb pressure, the bomb time must be five times greater than the 60 psig time in order to obtain the same amount of fluid in the device. There were some escapes at 30 psig and 90 psig that did not occur at the 60 psig level, therefore, if possible, the test should be conducted at 60 psig. FC-78 was the most effective fluid used. The higher evaporation rate results in less error from surface retention than resulted from the other fluids.

The vacuum cycle is required for packages having internal volumes of less than 0.1 cc but provides no improvement on packages with larger internal volumes.

SECTION XIII

SUMMARY

The investigation was not successful in isolating a single test condition which would be effective over the entire fine- and gross-leak rate ranges for all packages. Isolation of such a condition for all package sizes would have provided the most cost-effective testing solution for determining whether or not microcircuit packages were hermetic.

The investigation was successful in determining that a maximum of two test conditions are required to cover the entire leak rate range. It also pointed out that if the 1×10^{-6} L limit being proposed for packages having an internal volume of greater than 0.4 cc, is an acceptable limit, then the weight gain test (proposed Condition E) can be used as a single test for hermetic seal on microcircuit packages of that size.

It was also determined that no particular piece of equipment provides more valid results than the others used if conditions are properly chosen and the equipment properly set up and operated in accordance with the manufacturers instructions.

The MS-90 UFT machine is more efficient than the MS-12 in terms of time per unit tested but the results are not improved because of this faster speed.

It is important that nonabsorptive filler blocks be used with large radioisotope systems to occupy the space in the pressure vessel which is not taken up by the parts being tested. If this is not done, the longer pump-down times required will result in more escapes in the mid-range than will occur with the small system or Condition A.

The helium data (Condition A) was analyzed to determine the validity of the formula in MIL-STD-883. It was determined that for all pressurization conditions, the devices did fit the curve. This confirms that the molecular flow assumed in the formula is correct in the fine-leak range. It should be pointed out that in actual practice, however, many of the gross leakers would have been accepted as good product instead of being categorized as rejects. Their values could be located on the down slope of the curve (see Figures 3-47) only by reference to the initial data. All other data analyses were conducted under the assumption that the leak-rate value of each device was unknown. The fact that the formula could be verified, however, made it possible to establish the sensitivity of the helium test under any given set of conditions. The sensitivity of the helium test as presently specified in Test Condition A does not provide adequate range. This is shown by the escape rates shown in Table XIII for the 10^{-6} and 10^{-5} ranges. This can be corrected by changing the limits to

and have been desirable and the state of the

those suggested in Table XV which minimize escape rates in the mid-ranges. The use of the controlled orifice technique will also provide increased range on volumes of less than 0.01 cm³, but it was too time consuming for production-type operations. The controlled orifice provided no improvement in sensitivity or range on packages having volumes greater than 0.01 cm³.

Evaluation of the radioisotope data indicated that the number of wash cycles (<3) was not significant; therefore, all additional testing was performed with one wash cycle. It was also determined that specific activity within the range (277 to 1397 microcuries per cm³) used did not affect the results as long as bomb times and pressures satisfied the equation in Condition B of Method 1014. Although curves were not constructed for this condition, the data indicate that the fine-leak range covered is essentially the same as that of Condition A. In most cases, however, the escape rate: were higher in the gross-leak range (Table XV). This is believed to be the result of the vacuum cycle required to store the krypton-85 and does not make Condition B less effective than Condition A for fine-leak testing of microcircuits.

Evaluation of package materials indicated that the major sorption area is the seal-package interface or the seal material, and in most cases, not the ceramic itself. Each material/package configuration must be tested and appropriate delay times installed if necessary.

Temperature preconditioning of the devices provided interesting results which negated the idea of improving the method by this means. Leak rates on metal can devices increased; whereas, leak rates on ceramic devices decreased. The degree of shift in the leak-rate range was dependent on the temperature and was inconsistent. Temperature preconditioning proved to be deleterious to securing valid results.

The evaluation of gettering materials established that fluorocarbons provided no increase in test sensitivity for Test Condition A or B. The polyimide improved the escape rates in the 10^{-6} and 10^{-5} ranges on both Conditions A and B but did not entirely eliminate escapes (Tables XVI and XVII). It also caused an unacceptably high (18%) overkill rate on Condition A. The vacuum pump oil does work using Condition B but tends to be drawn out of gross leakers during pump-down, contaminating good devices. It is concluded that gettering is a possible means of testing the entire leak-rate range with a single test; but extensive work is still required to determine the proper material(s) to be used.

Condition C₁ bubble testing evaluation data indicated that either 3M FC-40 or Flutec PP-9 fluid could be used to conduct the test. It could be assumed from this that fluids cited by each manufacturer as being equivalent could also be used. These would include 3M FC-43 and FC-48 and the Flutec PP-7.

The test results indicated that overkill (good devices rejected) and escape (nonhermetic devices accepted) rates will occur even under carefully controlled conditions. These rates are package dependent, being higher on ceramic and large seal area metal devices than on small all metal/glass ones.

The results also indicate that some gross leakers in the 10^{-4} and 10^{-5} range are detected by Condition C_1 but the escape rates are so large that the condition could not be used as a single test for these ranges.

Condition C_2 bubble test results show it to be a more reliable technique for detecting gross leaks than Condition C_1 . This is true even in the 10^{-3} and 10^{-2} ranges which C_1 is intended to cover.

As with the C_1 test, similar results were obtained with 3M and Flutec fluids. The 3M FC-78/FC-40 combination was not significantly different from the Flutec PP-1/PP-9 combination. Both yielded good repeatability, and relative to C_1 , low escape rates.

The vacuum cycle presently specified is necessary on packages having internal volumes of less than 0.10 cc tc minimize escape rates. It could be omitted on larger packages with no significant difference in escape or overkill rates.

Condition C_2 is recommended as a more effective and repeatable procedure than C_1 over the entire gross-leak range.

The weight gain test (proposed Condition E) proved to be the most effective of the gross-leak methods. Sixty psig was determined to be the pressure at which the escape rate could be reduced to zero for all devices having leak rates of 10^{-5} or larger.

The fluids evaluated did not prove to be equivalent as had occurred with the bubble tests. The 3M FC-78 provided better results in terms of overkill and escape rates than did the FC-77, PP-1, or PP-2.

The vacuum cycle is required on the weight gain test for devices having internal volumes of <0.10 cc but does not improve results on larger packages.

The data was also analyzed to determine the effectiveness of subjecting the units to a series of fine-leak and gross-leak testing. The results of the fine-leak repeatability and the result of the gross-leak testing was considered to be a combination test. The sequences were matched by pairing the fine-leak runs 1, 2, 3, and 4 with the corresponding gross-leak runs. The results show that with

Conditions A or B followed by Condition E there will be no escapes in any range which are greater than 1×10^{-5} . The greatest escape rate occurred on the C-PAK, a ceramic package. One problem with the ceramic packages is that occasionally the seal area will form voids in the sealing glass and trap the tracer gas when fine-leak testing is performed, and the device will be rejected. When these units are then subjected to gross-leak Conditions C or E, they will hold enough fluid in the void to bubble but not enough to weigh 1.0 milligram. This is indicated by the test results shown in Table XXXVII. This anomaly would also result in Condition A detecting more leakers than Condition B as more of the tracer gas would be removed by the store cycle of Condition B than the natural diffusion which occurs with Condition A. Table XXXVII shows that fine-leak testing followed by Condition C_2 allows some escapes in the 10^{-5} range that do not occur when Condition E is used. It can be concluded that Condition E is more sensitive than Condition C_2 , and even under ideal conditions, there will be some escape in the 10^{-6} range for some package types as the present fine and gross methods do not detect all leakers.

Recommendations for application of these results are discussed in Section XIV.

Table XXXVII. Fine-Leak Testing Followed by Gross-Leak Testing

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Device		TO-84		,	C-PAK			C-DIP		¥	MOS DIP		7	TO-100		٠ ×	1 X 1 Ceramic	ાં		10:3	
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							ပိ	ndition	Condition A followed by Condition E	wed by	, Cont	dition	ш								
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							ပိ	ndition	Condition B followed by Condition E	wed by	/ Conc	dition	ш								
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							Condi	tion A	Condition A or B followed by Condition C2	pewo	by Co	nditio	n C2								
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SECTION XIV

RECOMMENDATIONS

The following recommendations are made to provide the highest levels of confidence that nonhermetic microcircuits will be detected by the test or sequence of tests conducted. That in the case of sequential tests maximum overlap of the conditions will be provided and that overkill rates be minimized to the extent possible commensurate with detection of the nonhermetic devices.

For helium testing, Condition A, three limits must be established to cover the broad range of microcircuit package volumes. The limits recommended are L (actual leak rate) ralues.

Internal	
Volume	L Limit
cc	atm cc/s
<0.01	5 X 10 ⁻⁸
$> 0.01 \le V < 0.4$	1 X 10 ⁻⁷
≥0.4	1 X 10 ⁻⁶

These limits are lower in value, one decade, one-half decade, and one-half decade, respectively, than presently specified but are necessary to minimize escape rates in the 10^{-6} and upper end of the gross leak range.

Helium tests may be performed at bomb pressures from 30 to 60 psig but the limit value and time chosen must provide an R (indicated leak rate) value which can be accurately read on the mass spectrometer being used. A maximum t_2 (time from removal of bomb pressure to read) of one hour is recommended with a 30-minute maximum being preferred.

For radioisotope testing, Condition B, two limits must be used to minimize escape rates in the 10^{-6} and upper gross leak ranges. The limits recommended are Q values.

Internal	
Volume	Q Linıit
cc	atm cc/s
<0.01	1 X 10 ⁻⁸
≥0.01	5 X 10 ⁻⁸

Radioisotope tests may be conducted at any pressure of at least 30 psig. It is recommended that a minimum bomb time of 0.2 hour be used. Conditions chosen must satisfy the equation $Q_S=R/SKTP$ stated in MIL-STD-883 with the above time and pressure limitations. Microcircuits must be read within 1 hour after removal of bomb pressure with a 50-minute maximum being preferred.

It is recommended that the present Method 1014 Condition C₁ followed by Condition C₂ be deleted and that C₂ only be used as the bubble test condition. Based on the fluid fill rate data, a bomb condition of 2 hours at 60 psig is recommended. Also for packages having an internal volume greater than 0.1cc a bomb condition of 10 hours at 30 psig may be permitted. These conditions insure that fluid in a sufficient quantity, to cause observable bubbling, will be forced into the package.

The failure criteria should be changed to read: Devices are considered rejects if during the 30-second test period, a definite stream of bubbles or two or more large bubbles originating from the same point are observed.

The weight gain test is recommended for inclusion in MIL-STD-883. Sixty psig for a period of 2 hours is recommended for bombing. If the package will not withstand 60 psig the pressure may be lowered to 30 psig and the bomb time increased to 10 hours. The pressurization should be preceded by a 1-hour vacuum cycle on devices having internal volumes of less than 0.1 cc.

The limits to be specified are 1.0 milligram for packages of <0.01 cc and 2 milligrams for packages larger than 0.01 cc. Batch categorization may be used if the devices are separated into cells of 0.5 or 1 milligram depending on volume. They may then be accepted if they shift no more than one cell in value after bombing. Weight loss should not be considered as cause for rejection.

It is recommended that the following tests be performed for detection of nonhermetic devices.

Test Condition follo	owed by Test Condition
A or B	C, D or E
A or B	C or D
E	None
	A or B

^{*}If reliability requirements can be satisfied by a leak rate of $\leq 1 \times 10^{-6}$ atm cc/s.

It is recommended that the changes made to Method 1014 of MIL-STD-883 as a result of this study be incorporated into Method 1071 of MIL-STD-750. This will provide consistent test procedures for microelectronic and discrete devices used in military systems.

APPENDIX

MICROCIRCUIT SEAL TESTING DATA

APPENDIX DATA CONTENTS

Data		
Ref. No	o. Title	Pages
1.	TO-84 Helium L Values Variable Condition	26-127
2.	C-PAK Helium L Values Variable Condition	28-129
3.	C-DIP Helium L Values Variable Condition	30-131
4.	MOS DIP Helium L Values Variable Condition	32-133
5.	TO-100 Helium L Values Variable Condition	34-135
6.	Ceramic Helium L Values Variable Condition	36-137
7.	TO-3 Helium L Values Variable Condition	38-139
8.	Glass Standards Helium L Values Variable Condition	140
9.	TO-84 Helium R Values Variable Condition	42-143
10.	C-PAK Helium R Values Variable Condition	44-145
11.	C-DIP Helium R Values Variable Condition	46-147
12.	MOS DIP Helium R Values Variable Condition	48-149
13.	TO-100 Helium R Values Variable Condition	50-151
14.	Ceramic Helium R Values Variable Condition	52-153
15.	TO-3 Helium R Values Variable Condition	54-155
16.	Glass Standards Helium R Values Variable Condition	156
17.	TO-84 Helium Repeatability R Values	58-159
18.	C-PAK Helium Repeatability R Values	60-161
19.	C-DIP Helium Repeatability R Values	62-163
20.	MOS DIP Helium Repeatability R Values	64-165
21.	TO-100 Helium Repeatability R Values	66-167
22.	Ceramic Helium Repeatability R Values	68-169
23.	TO-3 Helium Repeatability R Values	70-171
24.	Glass Standards Helium Repeatability R Values	172
25.	TO-84 Radiflo Q Values Variable Conditions	74-175
26.	C-PAK Radifio Q Values Variable Conditions	76-177
27.	C-DIP Radiflo Q Values Variable Conditions	78-179
28.	MOS DIP Radiflo Q Values Variable Conditions	30-181
29.	TO-100 Radiflo Q Values Variable Conditions	32-183
30.	Ceramic Radiflo Q Values Variable Conditions	34-185
31.	TO-3 Radiflo Q Values Variable Conditions	36-187
32	Glass Standard Radiflo O Values Variable Conditions	188

APPENDIX DATA CONTENTS (Continued)

Duta		
Ref. No	o, Title	Pages
33.	TO-84 Radiflo Repeatability Q Values	190-191
34.	C-PAK Radiflo Repeatability Q Values	192-193
35.	C-DIP Radiflo Repeatability Q Values	194-195
36.	MOS DIP Radiflo Repeatability Q Values	196-197
37.	TO-100 Radiflo Repeatability Q Values	198-199
38.	Ceramic Radiflo Repeatability Q Values	200-201
39.	TO-3 Radiflo Repeatability Q Values	202-203
40.	Glass Standards Radiflo Repeatability Q Values	204
41.	C-DIP Helium R Values Temperature Conditions	206-207
42.	TO-100 Helium R Values Temperature Conditions	208-209
43.	C-DIP Radiflo Q Values Temperature Conditions	210-211
44.	TO-100 Radiflo Q Values Temperature Conditions	212-213
45.	Helium Getter Evaluation	214-215
46.	Radiflo Getter Evaluation	216-217
47.	Surface Absorbtion Helium	218
48.	Surface Absorbtion Radiflo	219
49.	Helium Controlled Orifice	220-221
50.	TO-84 Weight Gain Data	222-223
51.	C-PAK Weight Gain Data	224-225
52.	C-DIP Weight Gain Data	226-227
53.	MOS DIP Weight Gain Data	228-229
54.	TO-100 Weight Gain Data	230-231
55.	Ceramic Weight Gain Data	232-233
56.	TO-3 Weight Gain Data	234-235
57.	Glass Standard Weight Gain Data	236-237

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1. TO-84 Helium L Values Variable Condition (Sheet 1 of 2)

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75 PS16 2 HOUPS	0.05%	0000	0.00		0.009	2000.0	0.009	2:300.0	000	0.00	450.0	500.0	500.0	500.0	0.009	0.000	500°	500.0	200.0	0.004	0.000		2005	500.0	0.0	0.000	200.0	400.0	0.000	200	000	0000	500.0	403 0	609.0	500.0	400.0	400.0	400.0	498.0	د	ر.دي.	•
1 HOUS	0.00%	65.0	5.00	2000	0.004	600.0	500.0	0.0000	600.0	0.000	0.00	A00.	0.000	400.0	9000	500.0	0.00,	,00°	600	2000	2000		400	6.000	200.0	500.0	2007.0	6,004	600	0.00		0000	603.0	500.0	400.0	60.09	\$00°	400.0	400.0	400.0	0.000	ر. د	
4 HOURS	0.0	0,0	•		Ċ		0.0	800.0	3000.0	3000		2000.0	900.0	0.0	450.0	700.0	530.0	c.0	8.00.0	100.0	800.0	0.00		800	900.0	900.0	800.0	٥.٠	700.0	200		700.0	700.0	700.0	700.0	900.0	700.0	700.0	170.0	100.0	700.0	700.0	> > > >
PS16 2 HOURS	0.000	6.00.0	0.000	0000	0.004	100	6000	650.0	0.000	0.000	0.000	0.004	499.0	500.0	650.0	503.9	200.0	500.0	500.0	500.0	500.0	200.0	500.0	2005	500.0	500.0	500.0	5,00.0	600.0	200.0	0.00	0.005	500.0	500.0	500.0	500.0	500.0	0.004	400.0	500.0	200.0	200.0	>
60 1 MOUR	0.000	0.00%	0.00	000	0.00	550.0	600.0	2000.0	0.000	20002	0.00%	600.0	0.009	557.0	550.0	550.0	550.0	550.0	0000	550.0	550.0	550.0	0.004	0.00	500.0	600	550.0	550.0	550.0	0.000		2005	550.0	6006	2000.0	0.000	6.004	0.009	60000	0.003	6000	400.0	
4 HOURS	0.009	550.0	6.00	0.000	550.0	602.0	550.0	2000.0	600.0	3000	2000	200.0	500.0	450.0	0.064	450.0	500.0	450.0	452.0	450.0	450.0	550.0	0.000	2005	450.0	523.0	450.0	450.0	452.0	250	2000	45.0	303.0	557.0	55).0	450.0	500.0	453.0	0.65.	650.0	55.0	0.6.95	7
PS16 3 HOURS	659.0	550.0	6.054	0.000	6.00.0	650.0	650.0	2300.0	2000.0	2000-0	0.000	560.0	0.009	550.0	550.0	530,0	650.0	540.0	567.0	560.0	560.0	560.0	0.045	567.0	260.0	560.0	600.0	560.0	560.0	560.0	2000	2,045	6000	56.0.0	550.0	560.0	560.0	560.0	6.004	550.0	560.0	6,045	
45 1 HOUP	650.0	650.0	500.0	0.000	000	0.009	9000	0.0	150.0	2000-0	6000	500.0	0.0	500.0	500.0	500.0	0.0	500.0	400.0	0.004	603.0	0.006	2000	0.009	0.009	9000	400.0	500.0	0.009	600.0	000	000	600	500.0	0.000	400.0	401.0	597.0	400.0	0.000	5.00.0	400	
A HOURS	650.0	650.0	0.009	000	009	6.00	0.004	650.0	6.00.0	2000.0	0.007	500.0	600.0	\$00.0	4000	500.C	650.0	500.0	500.0	500.0	500°C	630.0	0.004	0.004	6.00-0	0.004	600.0	500.0	500.0	500.0	2000		500.0	0.004	0.00%	6.00	500.0	5.00.5	500.0	600.0	6,00.6	0.000	2
P \$16 4 HQURS	600.0	6000	9009	0000	2004	0.009	520.0	2.00.5	200.0	2000.0	0.000	500.00	400.0	420.0	300.0	6.005	503.2	3.02	200.0	450.0	0.057	5.00.0	0.00	000	200.0	0.00	200.0	5.00.0	4.30.0	500.0	0.000		0.00	500.0	5005	5.00.0	500.0	500.0	500.0	5.00.0	453.0	0.00	
30 1 HOUR	550.0	650.0	450.0	0.076	0.054	650.0	650.0	2000.0	0.0000	2000.0	0.000	6.00	6.50.0	550.0	580.0	500.0	6.50.0	650.0	500.0	0.50.0	2000	450.0	220	0.000	580.0	580.0	(50.0	5,045	650.0	5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.00	0.00	537.0	450.0	450.0	580.0	A 50. G	540.0	3.08.C	5000	550.0	2000	,
2613HT 641%	-	~	~ .	0.0001			~	_			0.0004	٤.	_	-				100001	1000001	0.00000 10.00	0.000 0010.001	1,00001	700.010000.0	0.0000010.000	0.000010.008	400.010000.0	900.010.000.0	9.0070019.0	0.0000310.007	300°010°00°0	7.00,01,00,00,00,00,00,00,00	200 0100000 0	200.010.000.0	2000011.002	700.010000.0	800.0170970.0	0.0000010.007	0.0000010.00	7,0,010,007	703,010,000,0	0.0000010.007	0 000010 002	
14111A1 14111A1	0.0	c c	٠ د د					0.00.	3770.0	3,77,0		2003	0.000	C.	450.0	703.7	50.03	٠,٠	400	C	100.00	70.01	0.007	0.000	850.0	900°	0.000	, ° °	2000	200°	0.007	2002	700.0	700.	700.0	900.0	700.	130.0	7.0.0	709.0	700.0	100	
۲.	5	£.	Ç.		2 3		α	3	ç	<u>,</u> (. 3	3	1		α	S	٤	=	2	۲.	2 :	: :	2 5	8	2	٤	=	۵	a . :	2 5	; ;	7	ď	ç	2	=	ò	5	8	3	1	š

ALL I VALUES GFEATER THAN 1-17- IRE ESTINATED VALUES FRINING THAT THESE OFVICES 49 GROSS LEAKEPS.

1. TO-84 Helium L Values Variable Condition (Sheet 2 of 2)

PACKYGF CPAK - HELIUM I VALUES ELIUM VARTARLF CONDITION FVALUATION ALI OATA X10-9 ATM-EC/SFG

4 HOURS	3000.0	- 6	85.0	۲.۲	`:	==	7.2	-:	0.0001	3000.0	a .	0 0	2.1	46.0	1000.0	`: :	2 6	30.0	1.3	=:	e • •	3000	96.0	3000.0	1200.0	0000	1200.0	3000	0000	360.0	3000.0	2000.	0.000	1200.0	3000.0	3000.0	1200.0	1400.0	360.0
ሳስ ሶ ኗየና 2 ዘኅሀዩ	80.0	c c	-	2.6	- 60	1.2		0.0	0000	13.0	C:		0.0	3000.0	38.0	٠-6	•	18.0	1:1		m •	26.0	25.0	3000.0	1300.0	480.0	2000	420.0	120.0	550.0	3000.0	240.0		1300.0	3000.0	3000.0	1300.0	1300.0	900.0
9 1 H7418	3000.0		34.0	¥ .	x .	::	2. R	۲.,۲	0.0001	3000	3000	\$		3000.0	3000.0	2.5	,	0.00	۲.	4.			1.3	1000.0	1400.0	3000	3000.0	3000.0	0.000	1200.0	3000.0	3000.0		1200.0	30000	3000.0	1300.0	1409.0	0.000r
4 HORIRS	3000.0	0 4	26.0	3000.0	~ .		1.5		0.0005	1.5	٠.	4,000	6.0	33.0	0.09	~;	2000	20.05		٥,٠	-:	0.000	3000.0	3000	1300.0	30000	1000	3000	0000	370.0	30000	000	3000	150.0	3000.0	200	1200.0	1500.0	390.0
75 P\$16 2 HRBPS	3,000.0	<u> </u>		96.0	÷.	::	1.0	°:	3000	67.0	~:	~ .	9.1	42.0	3000.0	~.	•	0.34	0.0	W. B.	* .		1.2	3000.0	1200.0	3000.0	1400.0	0.000	0000	520.0	480.0	470.0	100.0	1300.0	0.0000	0.000€	1300.0	1300.0	3000.0
7. 1 ++C(JP	3000.0	A. C. C.	74.0	7.7	::	; - ',	7.4	٠,	0000	32.0	28.0	2000	0.6	3000.0	3000.0	53.0	•	24.0	c	6	er c	3000.	2.1	3000.0	1400.0	320.0	1300.0	7,000	0.000	460.0	3000.0	3000.0	1000	9.00	3000.0	250.0	1300.0	0	3000.0
4 HOURS	3000.0	9.0	1.0	7.0	200	50.0	9.0	7. A	0.000	0.0	3000.0	3000.0	3000	0.4	1000-0	.000	0000	3000.0	3.000 €	3000.0	3000	120.0	70.0	3000.0	920.0	3000.0	3000	3000	0.000	120.0	3000.0	3000	3000	3000	30000	3000.0	1300.0	3000.0	200,0
PSIG 2 HOURS	1.1	۳. ۳. 	1.4	3.6	* ·	.0.	3.0	٠. د د	2000	2.5	~	1000	17.0	2000.0	0.000	m -	0000	0.09	21.0	34.0	0.000	0000	3000.0	3000.0	1200.0	3000.0	3000.0	0.0001	820.0	590.0	3000.0	3000	3000.	1400.0	3000.0	3000.0	1300.0	1200.0	3000.0
60 1 HOUR	3000.0	 		r . 2		3.2	1.8	0.4	0.000	57.0	· ·	1.000	1.3	8.0	3000.0	0.9	0 000	45.0	2.5	2.9	2.5	0.000	1.9	3000.0	1000.0	3000.0	3000.0	0.0001	960.0	1100.0	3000.0	3000-0	0.000	1400.0	3000.0	3000.0	1300.0	1300.0	3000.0
6 HOURS	3000.0	0 0	ç	0.1	~ .	. v		1.5	-	1.3	0.1	- 0	1.2	7.2	45.0	4.1		60.04	0.1	1.0	2000	0000	0.0	3000.0	1400.0	3000	3000.0	3000.0	1000	1200.0	3000.0	3000	200.0	1300.0	3000.0	370.0	1200.0	1400.0	320.0
PS 16 3 40025	3000.0	- °	w.	9.1	•		1.3	7.2	8.1	3000.0	2.1	3000.0	31.0	14.0	40000	3.6	0000	3000-0	9.0	1100.0	3000.0	0.000	4.	3000.0	1100.0	4000.0	3000.0	0000	260.0	1000.0	3000.0	0.000%	0.000	1400.0	3000.0	0.000	1200.0	1300.0	3700.0
45 1 HOUG	3000.0	4.6	7.5	9.2	5.2	2.0	0.4	4.0	30005	4.2	9.0	2000	2.0	3000.0	3000.0	3000.0		42.0	4.8	N,	0. v. 0	3000	3.0	3000.0	1400-0	360.0	3000.0	3000	3000	11.00.0	3000	0.000	3000	950.0	3000.0	3000.0	1000.0	1300.0	3000.0
A HOURS	0.0	0.4		0.7	× 0	12.0	1.1	1.7	0.0005	1.4	0.8	3000-0	2000	30.0	3000.0	7.8	0000	42.0	14.0	3.7	3000	120.0	69.0	3000	1400.0	1000.0	3000-0	3000-0	1300.0	1400.0	3000.0	3000-0	0.000	210.0	330.0	3000.0	340.0	0.0	300000
P\$16 4 HNURS	3000.0	6 6 6	0.0	1.0		÷0.09	0.3	2.7	3000	3000.0	0.0	3000	3000	30.00.0	1000.0	0.0	0.000	3000	3000.0	2,2	3030.0	0.000	3000.0	3000-0	1400.0	0.0001	0.0001	0.0001	000	300000	1000+0	3000.0	3000-0	3000	3000.0	3000.0	1300.0	1200.0	3000*0
37 1 HPJR	1.3																																						
WEIGHT	0.0	¢ ¢	0.0	0.0	6.0		0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	c c	,	0.0	0.0	0.0	c (0.0	0.0	0	0	0.0	0 0		0	0.0	6.0		0.0	0.0	0.0	1000.0	1 00000	10000.0
INITIAL VEFCO	3000.0	\$ 0. \$ 0. \$ 0.	1	0.7	20.0	50.0	9.0	7.9	3000	0.0	3000.0	1000	0.000	0.7	3000.0	7.0	0.000	3000.0	3000.0	\$400.0	3636.0	120.0	0.0	0.000	920.0	3000	3000.0	1000.0	0.000	120.0	4000.0	3000.0	0.000	1000	3000.0	3000.0	1300.0	3000.0	200.0
MUT.	- ^	m 4	ď	\$	- :	r v	2	=:	7 [7	<u>~</u>	2!	<u> </u>	2	20	25	7,5	0.4	52	26	22	÷ %	, ç,	۲	33	, ,	35	3,4	ć e	39	40	2 ;	; ;	4	4.5	4.	. v	4	2

ALL L VALUES GREATER THAN 1X10-6 ARE FSTIMATED VALUES KMOMING THAT THESE DEVICES ARE GROSS LEAKERS.

2. C-PAK Helium L Values Variable Condition (Sheet 1 of 2)

PACKAGE CPAK - HELTUM L VALUES ELTUM VARIABLE CONDITION FVALUATION ALL DATA XIO-8 ATM-CC/SFC

4 HOURS		0.000
90 PS16 2 HOURS	3000.0 3000.0 3000.0 550.0 550.0 550.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570.0 570	150.0
90 1 HPUR	00000000000000000000000000000000000000	0.000€
4 HOURS	25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25000 25	3000.0
75 PS16 2 HCURS	10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10	450.0
7 1 HCUR	30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30	3000-0
→ HOURS	2	200.0
PSIG 2 HOURS	2	3000.0
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ALL I VALUES GREATER THAN IXIO-6 ARF ESTIMATED VALUES KNOWING THAT THESE DEVICES ARE GROSS LFAKERS.

2. C-PAK Helium L Values Variable Condition (Sheet 2 of 2)

PACKAGE COLP - HELIUM L VALUES HELIUM VARIAGLE CONDITION EVALUATION ALL DATA XIO-8 ATM-CC/SEC

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	9 HOUR	3.0	2.5		4.0	2.3	r.		2.8	8.4	0.13	9	7.0	7.8	6°6	0.0	0.54	4	7.0	(3.2	3000	120.0	36.0	12.9	63-0	25.0	100.0	100.0	4.9	5.3	1000	240.0	3000.0	3000	7.	3000.0	4.0	3000.0	3000	8.2
	4 HOURS	5.		•	2.6	∹			2.1	7.0	12.0	2 6	8.2	6.1	8.4	7	12.0	6.4	2.1	2.1	1.9	0.0005	3000.0	35.0	120.0	0.06	56.0	0.89	2,62,0	4.5	13.0	0.000	150.0	150.0	23.0	7.7	3000.0	1400.0	3000.0	1000	450.0
	75 PSIG 2 HOURS	1.9	2.7	6:	3.0	3.4															,								96.0									7.5	1.00	0.000	68.0
	T HOUR	2.1	* 4	3.5	3.8	3.1																							34.0												62.0
	4 HOURS	. s	2.4	0	3.8	0	•	9.1	1.2	20.0	12.0		20.0	4.0	0.0	2.0	18.0	9.0	13.0	9.4	12.0	3000	3000	3000.0	3000.0	3000.0	3000.0	3000.0	3000.0	23.0	21.0	2000	3000.0	3000.0	2.7	20000	1000	1400.0	3000.0	3000	30000
C/SEC	PSIG 2 HOURS	7.4	1.7	2.1	4.2	1.	* *	3.5	5.4	9.6	2.0	3.6	15.0	7.9	\$ °	,	0.61	9.6	17.0	2.2	0.11	3000	3000.0	3000.0	3000	3000	3360.0	1000.0	770.0	7.9	16.0	72.0	3000.0	3000.0	15.0	2000	3000.0	1400.0	3000.0	1200	3000.0
DATA X10-8 ATM-CC/SE	60 1 HOUR	7.0	. ~. •	2.0	6.5	60	0 0	•••	5.5	13.0	13.0	9	16.0	6.5	φ.	,	19.0	9.5	14.0	0,0	0000	3000	120.0	3000.0	3000-0	3000.0	120.0	100.0	2000	6.5	19.0	0.00	3000	3000.0	3000-0	2000	3000.0	1400.0	3000.0	0.004	3000.0
C DATA XI	6 HOURS	1.5	9-1	9.0	2.6	7.5	0.0	2 -2	5.1	0,6	12.5	2.0	16.0	7.0	2.0	2.0	16.0	0.6	16.0	9.1	0.00	3000	3000.0	3000-0	0.000	3000	3000.0	3000.0	150.0	10.0	0-91	0.51	30000	3000.0	0.6	20000	3000-0	1.3	3000.0	250.0	3000.0
₹	PSIG 3 HOURS	2.3		1:0	2.8	*	7.7	2.3	1.7	8	9.6	2.5	12.0	3.7	4.	***	15.0	7.5	9.8	0°0	0.00	3000	3000.0	3000.0	3000-0	3000.0	140.0	140.0	140-0	16.0	12-0	95.0	3000.0	3000.0	37.0	2.4	3000.0	4.3	3000.0	1400.0	450.0
	45 1 HOUR	1.6	6.1	1.3	2°8	3.6		3.4	3.4	80	0.6	•	14.0	6.2	2.1		14.0	0.0	12.0	0 0 0	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	3000.0	95.0	3000.0	110.0	3000.0	3000.0	62.0	2.5	6.3	14.0	52.0	3000.0	3000.0	0.64	75.0	3000.0	1,400.0	3000		3000.0
	8 HOURS	6.0	1.1	0.0	1.9	٠. د			1.0	13.0	23.0	3.6	26.0	7.8	 	22.0	30.0	11.0	19.0		13.0	3000	3000.0	3000*0	3000-0	3000.0	3000.0	3000.0	3000	21.0	25.0	30000	3000	3000-0	2.000	1,2	3000.0	1300.0	3000	0.003	3000.0
	PSIG 4 HOURS	0,0		2.6	2.7	0 1		1.5	0.0	80 0	7 0	2.5	6.5	2.0	7,0		14.0	6.5	(0.0	7.2	2000	3000	3000.0	3000.0	3000-0	3000	3000.0	3000.0	22.0	18.0	14.0	3000	3000.0	3000.0	3000	3000	3000.0	1000	3000	1700-0	1560.0
	30 1 HOUR	3.4	9.0	8**	9.9	7.7	6.4	6.2	3.4	0.0	7.6	8	6.6	4.2	J. 1.		12.0	8.5	8.5	7.7	- 0	75.0	58.0	200.0	90.0	130.0	75.0	0.0	42.0	12.0	20.0	40.0	8.6	3000.0	0.440	3,0	3000.0	3.5	3000.0	3.5	5.0
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ALL L VALUES GREATER THAN 2X10-6 ARE CSTIMATED VALUES KNOWING THAT THESE DEVICES ARE GROSS LEAKERS.

3. C-DIP Helium L Values Variable Condition (Sheet 1 of 2)

PACKAGE COID - HELLUM L VALUES HELLUM VARIABLE CONDITION CVALUATION ALL DATA X10-6 ATM-CC/3EC

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ALL L VALUES GREATEK THAN 2X10-6 ARE ESTIMATED VALUES KNOWING THAY THESE DEVICES ARE UROSS LEAKEAS.

3. C-DIP stellum L Values Variable Condition (Sheet 2 of 2)

FACKAGE MOSUIP - MELLUM L VALUES
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AIL L VALUES GREATER HAN 5X13-6 PPE ESTIMATED VALUES KNIWING HAT THUSE NEVICES ARE GACSS LEARERS.

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6 HOURS	\$2000000000000000000000000000000000000	5300.0
PSIG 3 HOURS		4600.0
45 1 FCUR		4500.0
8 FCURS		5400.0
PSIG 4 HOURS		30005
30 1 FCUR	2	3900.0
REIGHT GAIN	700000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 2000000 200000 200000 200000 200000 200000 200000 200000 2000000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 200000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000	
INITIAL		5500.01
UNIT NUM.	383483868888888888888888888888888888888	100

ALL L VALUES CREATER T: 41. 5x10-6 ARF ESTIMATEC VALUES KACHING THAT THESE DEVICES ARE GROSS LEAKERS.

4. MOS DIP Helium L Values Variable Condition (Sheet 2 of 2)

PACKAGE TC100 - HELIUM L VALUES ELIUM VARIABLE CONDITION EVALUATION ALL CATA X10-8 ATM-CC/SEC

4 FOURS	4044 4000							•																		•		10.0
90 PS1G 2 HCURS	6.4	w • • •	2.0	w -0 :	2 W W	, r. r.	0.6	3.9	1 60 .	. o	in a	12.0	4 N		. φ.	26.0		F. 9	17.0	2.0	3000.0	0.00	-	55.0	200	3000	4 6	10.01
9 1 HOUR	9.4 10.0 7.6	9.6	4.0	9.0	2.4.4	3.0	0.00	9.0	13.0	13.0	0	4	7.6 8.2	4.0	7.6	100.0	2.5	4.6	22.0	10.0	30000	5.5		67.0		3000.0	4.6	4.6
4 HOURS	0 4 4 4 6 4 4 4 6 4 4 4 4 4 4 4 4 4 4 4	~ "		44.	40.0	4 6	6.43	4.4		4 4	4.	3.7	4.4	72.0	7.7	79.0	33.0	9.0	13.0	4.4	15.0	33.0	4.4	63.0	110.0	3000.0	7.8	36.0
75 PS 1G 2 HOURS	6.5.0 6.00	5.5		11.0	9 0 0	4 0	4.00	4	7.2	7.2	4.0		0.4	18.0	12.0	63.0	2 4 6 2 4 6	7. B	4.0		1.0	2.5	8.2	54.0	77.0	30000		4
7 1 HOUR	10.0	0.00	, w w	0.0	11.0		0	01	13.0	9.8	23.0	22.0	11.0	4.	12.0	87.0	v &	4.0	16.0	4.0	20.2	0,0	9:19	70.0	130.0	3000	9 9	1000
4 HOURS	4 14 4 14 4 14 4 4	44.	0 4	44	00.4	14.0	4 6	200	14.0	4.0	22 • 0	170.0	37.0	140.0	170.0	150.0	140.0	30.0	25.0	0.46	3000.0	0.0	26.0	150.0	3000.0	3000.0	3000.0	30000
PSIG 2 HOURS	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7.0	 	7.0	1 W C	9.0	, w c	12.0	12.0	13.0	8.5	190.0	8.2	46.0	13.C	57.0	110.0	2,0	34.0	10.0	180.0	0.44	9.4	44.0	30000	30000	120.0	3000.0
60 1 HOUR	15.0 6.5 6.5	12.0	0.4 0.4	7.9	13.0	900	14.0	12.0	13.0	11.0	15.0	33.0	7°.4	100.0	15.0 8.6	110.0	43.0	9.6	23.0	11.0	36.0	68.0	6.5	90.0	170.0	3000.0	78.0	0.0069
6 HOURS	4844	8.40	75 c	2.9	10.0	. w.		8 6	10.0	3.9	2.9	44.0	1500.0	130.0	3.4	70.0	360.0		24.0	17.0	0.06	000	5.5	86.0	160-0	3000.0	130.0	0.00
PSIG 3 FOURS	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8.5	0 W W	4.0	9 9 9		9 6	0 0 0 0 0 0 0 0 0 0 0 0 0	9.0	5.7	9	72.0	5.7	120.0	17.0	100	986	9 6	29.0	0.9	78.0	980-0	5.7	82.0	200.0	3000.0	100.0	150-0
45 1 HGUR	L- N. V. 4	11.0	000	9.9	44. 0.54.	4 4	0.00	100	13.0	2.3		120.0	0.4	300.0	22.0	120.0	120.0	9 9	42.0	0.6	49.0	100.0	11-0	88.0	160.0	0.000	100001	10001
8 HOURS	4446 4046	14 m	0 KI 4	3.3		2 4 4	9	93000	 	3.0	4.6	25.0 57.0	9.6	160.0	22.0 7.0	110.0	120.0	8 6	33.0	5.5	94.0	98.0	11.0	94.0	180.0	300000	130.0	150.0
PS IG 4 HOURS	3 K 4						,	•																	•			3000.0
30 F 1 HOUR	8 4 4 4 0 4 4 4	19.0	13.0	10.0	15.0	0.9	6.6	0.91	6.5	12.0	9.5	110.0	25.0	150.0	38.0	110.0	3000.0	22.0	35.0	8.0	90.06	75.0	17.0	110.0	150.0	3000.0	150.0	210.0
WEIGHT	0000																											
INITIAL	3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5													-														
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ALL L VALUES GREATER THAN 1X10-5 ARE ESTIMATED VALUES KNOWING THAT THESE DEVICES ARE GROSS LEAKERS.

5. TO-100 Helium L Values Variable Condition (Sheet 1 of 2)

PACKAGE TOLOO - HELIUN L VALUES HELIUM-VARIABLE COMDITION EVALUATION ALL CATA X10-8 ATM-CC/SEC

The state of the state of the engineer of the state of th

4 HOURS		
90 PS1G 2 HOURS		
1 HOUR		
4 HOURS		
75 PSTG 2 HOURS		
7 1 HOUR	1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200 1200	-
4 HOURS		
PS 1G 2 HOURS		
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45 1 HOUR	11111111111111111111111111111111111111	
8 FOURS	00000000000000000000000000000000000000	
PSIG 4 HGURS		,
30 1 HCUR		•
WEIGHT GAIA		
INITIAL VEECO		0.000
UNIT NUM.		2

ALL L VALUES GREATER THAN 1X13-5 ARE ESTIMATEC VALUES KNOWING THAT THESE DEVICES ARE GROSS LEAKERS.

5. TO-100 Helium L Values Variable Condition (Sheet 2 of 2)

PACKAGE CCRM - MELTEM I, VALUES
ELIUM VARIAGLE CONDITION EVALUATION
ALL PARA STOLA ATMICESTE

A response to the second secon

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	P HOUSE	#	
	4 HUUH 4		
	5 6516 2 HEURS	4	
	7 HOUR 7	2.	
	4 110URS	2	
י ני	PSIG 2 HCURS	2	
) K K P P	60 1 1:00R	20000000000000000000000000000000000000	
01 × 110	6 HCURS	2	200
•	PS IG 3 ECUPS	\$28000000000000000000000000000000000000	i.
	45 1 HFUR	\$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5000 \$5	
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ALL L VALUES GREATER THAN 6X10-5 ARE ESTIMATED VALUES KNOWING THAN THESE DEVICES ARE GRUSS LEAKERS.

6. Ceramic Helium L Values Variable Condition (Sheet 1 of 2)

6. Ceramic Helium L Values Variable Condition (Sheet 2 of 2)

ILIUM L VALUES DITTON EVALUATION ATM-CC/SEC	
PACKAGE CERM - HELIUM L VALUES HELIUM VARIABLE CONDITION EVALUATION ALL CATA X10-8 ATM-CC/SEC	

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30 1 HOUR	3000.0 113.0 31.0 1220.0 50000.0 50000.0 50000.0 1800.0 1800.0 1500.0 1340.0 1340.0 1350.0 150.0
MEIGHT	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
INI TIAL VEECO	3000.0 (55.0 (43.00.0 (43.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0 (40.00.0
NON.	20000000000000000000000000000000000000

ALL L VALUFS GREATER THAN 6X10-5 ARE ESTIMATED VALUES MAGNING THAT THESE DEVICES ARE GROSS LEAKERS.

ACKAGE TO-3 - HELIUM L VALUES
.104 VARIABLE CONDITION EVALUATION
ALL DATA X10-3 ATM-CC/SEC

4 HD RS	3006.0	550°0 550°0 550°0	3000.4	35.0	0.01	200.0	280.0	3000.0	3000	0.000	3000	 	0.0	6.5	13.0		0.7	•	, e	7.0	0.6	2.0	75.0		8.0	Q*0*	0.00		0.0	240.0	~ 0	3000	30000
72 o SIG 2 HOURS	3000.0	360.0	3000.0	36.0	23.0	0.6	7.0	3000.0	3000	3000	3000	8	2.0	8.0	18.0	12.0	12.0	0.6	0	0.0	12.0	0	0.0		9.00	70.0	0,00	2000	45.0	210.0	12.0	0.006	30000
י אטטא נ	3000. 0	380.0	68.0 3000.0	12.0	20.0	360.0	480.0	3000.0	3000.0	0000	30000	12.0	13.0	16.0	21.0	12.0	13.0	200	15.0	16.0	13.0	12.0	60.0	200	0.0	68.0	95.0		20.05	270.0	0.4	\$50.0	30,00
4 HDURS	0.0	380.0	3300.0	7.8	2.5	4.0	10.0	3000.0	3000.0	3000.0	3000	P. 6	200	13.0	0 0	2.0	9.6	0 u	14	0.0	0.4	2.6	33.0	• •	27.0	i.1.c	0.00	9 4	82.0	160.0		260.0	>-
75 PSIG 2 HJURS	13.0																																
, HUOH 1	13.0	30.00	3203.3	23.0	13.0	22.9	210.0	3000.0	1000	3000.0	3000.	23.0	73.0	16.0	27.0	19.0	24.0	18.0		18.0	22.0	37.0	20.02	0.0	17.0	24.0	6.6	200	52.0	300.0	0.0	780.0	A.0.2
4 HOURS	7.97	410.0	17.0	13.0	72.0	190.0	30.0	3000.0	3000.0	3000	30000	0,0	6.8	9.9	12.0	7.2	8 .	,,	8.8	1.4	8 0	16.0	88.0	22.	120.0	22.0	140.0		140.0	180.0	0.61	220.0	2.01
PSIG 2 HUURS	50.0 150.0 20.0	360.0	78.0	30.0	23.3	22.0	90.09	3000	3000	0.000	3000	0.0	19.3	17.0	25.0	29.0	47.0	2.00	4,0	57.0	19.0	41.0	43.0		160.0	12.0	98.0	26.02	190.0	210.0	0.0	210.0	20.0
09 1 HOJ3	78.0	523.0	39.0	34.0	67.0	3.65	20.0	3000	3000	3000	3000.0	34.0	37.0	17.0	0.00	37.0	D. C.	2.5	26.0	40.0	48.0	35.0	103.0	2,4	150.0	160.0	80.0	000	180.0	260.0	20.0	180.0	34.0
6 HOURS	18:0 12:0 8:0	380.0	160.0	80.08	80.0	34	12.0	3000.0	3000	3000	3000.0	8	5.0	8.0	2.0	12.0	12.0	200		30.0	000	12.0	0.6	200	180.0	25.0	4. 0.4		130.0	150.0	င v	180.0	α ••
PS15 3 HOURS	1.5.0	510.0	0.0	120.0	14.0	12.0	55.0	3000.0	3000.0	3000-0	30000	4	ر د د د	0.0	0.0	12.3	12.0	12.0	12.0	21.0	12.0	14.0	210.9	200	310.0	0.0	160.0	200	240.0	340.0	14.0	330.0	7.4.5
45 1 HOUR	55.0	430.0 340.0	3000.3	70.07	0.0	12.0	14.0	3000.0	3000.0	3000.	3000	12.0	25.0	38.0	52.3	20.0	16.0	27.0	16.0	34.0	14.0	40.0	6.02		240.0	0.0	2°6	200	220.0	380.0	6,0	310.0	2.02
8 HOURS	13.0	270-0	160.0	160.0	12.0	70.0	30.0	3000-0	3000.0	0.008	30000	13.0	1.0	32.0	23.0	0.0	19.0	200	8.2	0.6	12.0	10.0	120.0	0.21	120.0	55.0	210.0	0.017	160.0	200.0	49.0	200.0	(.71
PSIG 4 400RS	22.0	30.0	450.0	103.3	7.0	75.0	65.0	3000.0	3000.0	3000.0	3000	0.01		3.0	30.0	.0.	22.0	,	72.0	2.2	0.0 0.0	0.6	173.0		95.0	5.6	0.00	72.0	100.0	520.0	90.0	300.0	3.6
33 1 HOUR	150.0 25.0 280.0	20.0	15.0	285,3	20.0	25.0	46.0	3000.0	3000-0	3000.0	30005	20.0	20.02	6.5	25.0	21.0	23.0	20.0	20.0	20.0	20.0	29.0	280.0	0.00	3030.0	140.0	0.000	20.00	3000.0	470.0	120.0	470.0	78.0
VE 1641	0000												200	0.0	0.0	0.0	o-0	0.0		0.0	30	2.0	0.0	•		0.0	0.0	•		0.0	0.0	20.	٠.٠
VEFCO	120.0	190.0	65.0	3,000.0	10.0		55.0	3000.0	3000.0	3000	3000.0	9.6	13.0	16.0	15.0	7.7	9.7	8.5	0.0	14.0	16.0	16.0	160.0	200	190.0	140.0	3000.0	20000	3 300.7	320.0	280.0	350.0	2.81
UNIT I		* rv <0	rα	9 2	112	2:	2 2	91	<u>«</u>	<u>ئ</u> د	5 7	25	2 %	\$2	2;	28	62	ín i	35	33	* *	*	37	r c	£ 3	4.1	2,5	71 4	45	44		4:	,,

7. TO-3 Helium L Values Variable Condition (Sheet 1 of 2)

PACKAGE TO-3 - HELIUM L VALUES ILIUM VARIABLE CONDITION EVALUATION ALL DATA XIO-8 ATM-CC/SEC

4 HOURS	200.000.000.000.000.000.000.000.000.000	3000.0
90 PSIG Z HOURS	84 889000	3000.0
1 H002	150.0 3000.0 3000.0 3000.0 3000.0 3000.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 1	3000.0
4 HOURS	100.000.000.000.000.000.000.000.000.000	3000.0
75 PSIG 2 HOURS	13000000000000000000000000000000000000	3000.0
T. HOUR	240.000.000.000.000.000.000.000.000.000.	3000.0
4 HOURS	120 120 120 120 120 120 120 120	3000.0
PSIG 2 HOURS	170 170 170 170 170 170 170 170	3000.0
60 1 HOJR	180 180 180 180 180 180 180 180	3000.0
6 HOURS	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	3000.0
PSIG 3 HOURS	1000000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3000.0
45 1 HOUR	210 210 3000 200 200 200 200 200 210 210	3000.0
8 HOURS	300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 300000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 30000 3000	3000.0
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UNIT NUM.	944654466666666666666666666666666666666	

7. TO-3 Helium L Values Variable Condition (Sheet 2 of 2)

8. Glass Standards Helium L Values Variable Condition

	4 HOURS	19.0	16.0	25.0	2.1.2	3000	28.0	18.0	1600.0	3000.0	0.00	2000.0	160.0	2100.0	160.0	75.0	200.0	290.0	3000.0	210.0	150.0	3000.0	160.0	3000.0	210.0	0.00	~		200.0		240.0		20	:		140000.0	30000	130000.0	140000	120000.0	130000.0	
	40 PS16 2 HOURS	200.0	24.0	360.0	0.00	0.0001	28.0	36.0	2100.0	3000.0	3000	1 800.0	1500.0	2100.0	0.000	300.0	180.0	250.0	3000.0	2002	160.0	3000.0	3000.0	3000.0	450.0	2000	3000.0	170.0	240	30000	3000,0	3000.0	3000	3000.0	3000.0	140000.0	3000.0			130000.0	130000.0	
	1 HOUR	38.0	42.0	45.0	35.0	0.000	30.0	32.0	1900.0	900	2,000	1900.0	1 000 0	2100.0	1000	220.0	220.0	550.0	3000.0	0000	300.0	3000.0	3000.0	3000.0	360.0	520°C	3000.0	180.0	220.0	3000	3000.0	3000.0	250.0				3000.0		1 40000.0	130003.0	0.000041	
	4 HOURS	33.0	18.0	0.41	0.91	0.000	24.0	130.0	2000.0	1700.0	0.000	1900.0	1400.0	2100.0	20002	140.0	130.0	190.0	30000	200	1,60.0	3000	3000.0	3000.0	200.0	3000	0.000	160.0	3000.0	3000.0	3000.0	3000.0	220.0	3000	3000.0	120000-0	3000.0		130000.0	140000.0	120000.0	
	75 PS1G 2 HOURS	2000		35	Š.		2000	16.0	2500.0	1800.0	2500.0	2100.0	1600.0	2000.0	2500.0	180.0	450.0	240.0	3000.0	180.0	130.0	3000.0	3000.0	160.0	250.0	3000.0	3000	180.0	3000.0	3000	3000.0	3000.0	160.0	30000	3000.0	140000.0	3000.0	00000	1,40000.0	140000.0	140000.0	
	1 HCUR	35.0	30.0	22.0	25.h	0.61	•			26.0		-		•	~	200	200.0	280.0	3000.0	0.00	300.0	3000.0	3000.0	3000-0	350.0	3000.0	3000	180.0	3000.0	3000.0				0.0000	85000.0	140000.0	3000.0	0.0000	140000	140000.0	140000.0	X-0000+X
	4 HOURS	18.0	3000.0	15.0	20.0	3000.0	0.000	12.0	15.0	60.0	12.0	3000.0	3000.0	2200.0	2200.0	0.000	3000-0	120.0	3600.0	120.0	160.0	3000.0	3000.0	3000.0	160.0	3000-0	3000.0	1300.0	3000.0	3000.0	3000.0	3000.0	140000.0	0.0000	3000	140000.0	3000.0	0.000041	0.0000	140000.0	140000.0	.0.0000*1
c/sec	PSIG 2 HAURS	32.0	3000.0	12.0	28.0	3000.0	0.000	30.0	40.0	3000.0	3000.0	17000	1200.0	2000-0	2000.0	0.000	3000	30000	3000.0	350.0	0.006	3000.0	3000.0	0.000	400.0	3000-0	3000.0	4000	3000.0	3000.0	3000	3000.0	130000.0	0.000001	3000	130000.0	3000-0	1300001	120000-0	120000-0	95000.0	130000*0
0-8 AT#-C	60 1 HOUR	2000.0	3000-0	40.0	14.0	41.0	30000	40.0	2900.0	850.0	3000.0	1600.0	2000	1700.0	2100.0	29000	3000	340.0	3000.0	360.0	180.0	3000.0	3000.0	3000-0	310.0	3000.0	3000-0	190.0	3000.0	3000-0	3000.0	0.000E	1 60000.0	0.000021	3000	140000.0	3000.0	0.000061	140000.0	130000.0	110000.0	1 40000 0
ALL DATA X10-8 ATM-CC/SEG	6 HOURS	15.0	3000.0	15.0	14.0	3000.0	0.0000		2800.0	3000.0	2400.0	2200-0	1200-0	1300.0	1400.0	100	30000	85.0	3000.0	90.0	1000	3000.0	3000-0	3000.0	100.0	3000-0	3000-0	95.0	3000.0	3000.0	30000	3000.0	140000.0	0.00006	3000.0	140000-0	3000.0	140000	120000-0	130000-0	130000.0	130000*0
AL.	PS16 3 HOURS	24.0	26.0	23.0	28.0	3000.0	3000.0	34.0	1800.0	2000-0	1800.0	1600-0	1400-0	2000-0	2400.0	280.0	0.0005	230.0	3000.0	200-0	1900	3000	3000.0	3000-0	350.0	3000.0	3000.0	190.0	3000.0	3000.0	3000.0	3000.0	130000.0	0.000001	3000	130000.0	3000.0	0.000021	10000	10000	110000.0	130000*0
	45 1 HOUR	3000.0	35.0	44.0	35.0	50.0	3000	34.0	1800.0	950.0	220.0	2100.0	1400.0	2000-0	2000.0	600.0	1600.0	0.024	3000.0	2000	1000.0	230.0	3700.0	3000	530.0	3000.0	3000.0	3000	3000.0	3000	3000-0	3000.0	11000001	1200021	0.000	110000.0	3000.0	130000-0	3000.0	110000-0	110000.0	85000*0
	8 HOURS	18.0	0.05	20.0	18.0	3000.0	=	0.75	•	0	ED.	1900.0	, i	۰.	2000-0	150.0	2000	~	30000		3000.0	• 0	3000.0	3000.0	·	0	3000.0	140.0		3000					3000	120000-0	3000.0	120000.0	130000-0	38	130000.0	130000.0
	PSIG 4 HOURS	2000-0	0.000	25.0	14.0	3000.0	3000.0	0.45	3000	30000	2000*0	1800.0	1,000	2200.0	2100.0	200.0	0.000	280-0	3000.0	160.0	1200.0	3000	3000	3000.0	250.0	3000-0	150.0	120.0		3000.0					0.000	130000-0	70000	130000.0	1100001	130000	140000.0 1300	140000-0
	30 1 HOUR	28.0	2000.0	24.0	25.0	3000.0	3000.0	20.00	2400.0	3000.0	2400.0	2200.0	2600.0	2500.0	2500.0	400.0	180.0	2002	3000.0	370.0	1760.0	3000.0	3000.0	3000.0	320.0	3000.0	270.0	3000.0	3000.0	3000.0	0.0005	3000.0	130000.0	3000.0	3000	146000.0	_	0	130000.0	40000-0	300000	_
	WFIGHT GAIN										1000.0	1003.0	00001	0.00001	100001						0.0		1000.0	1000.0	0.0001	1000	1000.0	1000	100001			10000		0.000001	3000.0109000.0	0.00000	0.20000	0	1000001	00000	0.000001	1 000000
	INI TIAL VEFCO	28.0	2000.0	24.0	75.0	3000-0	3000.0	25.0	2400.0	3000.0	2400.0	2200.0	2,000,0	2500.0	2500.0	400.0	180.0	200.00	3000	370.0	1700.0	0.000	3000.0	3000.0	320-0	30000	270.0	3000.0	30000	3000.0	0.000.6	3000.0	130000.0	3000-01	10.0006	140000-01	3000.0	133500.0	140000.0100000.	1000001	130000.0100000.	140000-01
	UNIT	-	~ ~	٠ 4	10	£	_	œ c	<u></u>	=	12	Ω:	* u	22	17	2	61	3 5	22	23	24	5 %	27	8	2 8	3.5	35	33	3.5	36	37	3 %	6,0	3	ر د د د د د د د د د د د د د د د د د د د	4	45	46	7.	9 9	20	2

Mary Contract Contrac

PACKAGE 1084 - HELIUM R VALUES HELIUM VARIABLE CONDITION EVALUATION ALL DATA X10-9 ATM-CC/SEC

	4 HOURS	2.0071	**	~.			0	0.1	2.0	130001		0.2	2.0	2.00.0			2800.0	• 6	20071	?;	2900.0	2500.0	0.0	000	0.1	0.3	320.0	160.0	450.0	3000		0.5	0°0	0 0	2.0		0.1	1 700.0	- ·	0.009	2.2
	O PSIG 2 HOURS	1000.0		2.0					۲۰۰۰	0.00	0.7	0.1	0.0	0.00	0	4.0	1500.0	0.0	2007		800.0	0		0.008	950.0	0.2	350.0	500.0	180.0	0.009	1200.0	0	E 0	2.0	. "	7.0	0.7	5.0	0.0	0.050	m.c
	1 HOUR	700.0		4.0			0.5		6.0	1000.0		0.5	2.0	00001		0.2	0.1	0	900.0	7.0	3000.0	0.1		2004	1200.0	0.1	3000	1.00.0	180.0	1200.0	o c		0	0.0	4 4		7.0	10001	• •	500.005	6
	4 HIMPS	30000		0.2			::	0.1		3000	0.2	0.0	0.0	1200.0	200	0.2	0.1	0	0.021	0.00	3000	0.1	0-1	000	2401.0	3.2	1,0.0	. 0	2.0	0.1	200	0.5	6.3	°°°	000	2	0.0	1300.0	۰۰ د د د	200.0	0
	'S PS16 2 HOURS	3200.0	0	0.2	•	• •		c	0.3	550.0		0.2	0.7	1200.0	Y	0.0	0.5		450.0	7.0007	1200.0	.0	0.1	2000	0.006	0.1	180.0	2001	180.0	390.0	~ ~	200	0.1	0.0	0 0		0.2	0.1		350.0	
	7. 1 HQUR	800.0		9.1		7.0		2.0	4.0	1000.		0	0.0	1600.0			1100.0	0.1	400.0	700.1	1300.0	0.4	 	9.0	0,0021	0	290.0	1.0	350.0	550.0				0.1	۰.۰		. ~ .	0.1		7.00	2.00
	4 HOURS	200-0	. 0	0.1	3000	0.0			3000.0	10.0		0.10	200.0	3000.0	-	0	0.0	0.0	3000.0	3000	30000	0.0	0.1	3000.0	3000	200	3000.0	3000.0	3.000	300.0	3000.0	0.00	0	0.0	0.0	200	0	0.0	0.0	0.00	0.00
7367	PSIG 2 HOURS	1600.0		0.1	0.3	**			0.5	1800.0	2 6		0.4	1200.0	200	0.0	2200-0	0.1	450.0	1900-0	2000-0	0.1	0.1	000	2,00.0	2600.0	0.5	7.000	160.0	2000-0	e .		0.1	0.1				0.1	0.1	7.0	
7-3 A IM=(-	60 1 HOUR	1.0	200	0.3	0.2	0.0	- c	0	0.0	450.0		0.0	0.0	1100.0	900		3000*0	0.2	0.009	550.0	3000	0.1	0.0	0 0	3500.0	0.004	0.3	1.00	0.000	3000.0	7.00	•	•	0.1				0.2	0.1	0.0	0.1
UAIA XI	6 HOURS	1400.0	-		0.1		2 6	0.1	0•1	120.0	2 -		0.2	720.0			1500.0	0.2	8.0	0.0001	30002	0.1	0.5	1.0	400.0	850.0	0.3	2.0	0.0001	420.0	2,00	7.000		0.1	- °	2.0		0.3	~ · ·	2.0	
ALL	PSIG 3 FOURS	400.0	F 0	4.0	7.0		\$ d	9.0	0.3	120.0	7.0	200	3.0	400.0	9.0	2.4	1,600	2.4	350.0	500.0	0,004		3.8	5.0	2000	550.0	180.0	1.5	2000	6.0	0.2	2.0	9.0	0.3	0.0	•	1.6	0.5	0.2	0.0	1.0
	45 1 HOUR	1.0	0.0	9.0	0.2	9.0	٠. د		0.5	350.0	•••	0.1	0.0	520.0	200	0	250.0	5.0	100.0	1800.0	0.0045	0.0	0.1	0.3	350.0	0.09	7.0	0.0	1200.0	2.0	0.3	200		9.6	7.0	•	0	0	0.2	0.0	*.°°
	8 HCURS	0.7	0	0.2	10.0	1.7		n In	0.3	3000	, v	-	0.5	1500.0	0.0	0	2000-0	0.0	0.2	0.0001	20001	0.2	0.1	1.0	1200.0	10.0	0.5	0.1	200.0	0.00	1.0	***			1000.0	2.0			0.1	0.0	0
	PS IG 4 HOURS	0.3	0.0	0	3.6	1.0			0.1	20.0		2.0	0.5	3000.0			2.0		0.1	3000-0	7.000		0.2	0.1	3000.0	2.7	3000.0	14.0	3000.0	3000.0	0.1			0.1	0.1	•		ċ	1.0	1.0	0.1
	30 1 HOUR	70.0	• • •	0	180.0	0.1				2600.0			0.1	320.0		~ - • •			0.1	1300-0	1.0	2000		-0	350.0	320.0	530.0	100	1530.0	650.)	1.0	2.0	; c	2.0	0.0			0	0.0	0.0	0.0
	WEIGHT GAIN	0.0	0.0	0	0.0	0.0	0.0	90	0.0	o c	3.0	2 0													c (90	0.0	0.0	C (000	0.0	٥ ، ن		0.0	0.0	o o	0.0		0.0	0.0	1000.0
	VECCO	6.000			3000.0	۲,	0.0	0 0	3000.0	12.	0.0	0 0	200.0	2017.7	0.1	9,0	3		3703.0	3000.0	2000	2000	0	3000.0	3000	0.000	3000.0	3000.0	2000	3000.	3000.0	3.5	Ċ	0	0.0	0.0	ָרָיָר פיי		0.0	1	0.0
	UNIT NOW.	-1	~ 6	n 4	ď	æ	^	er o	2	Ξ	15	<u>~</u> ~	. 2	12		<u> </u>	2 5	: 2	55	۲ :	22	5 %	27.	82	5,6	g :	32	33	34	£ %	37	38	6 4	4	45	43	7 7 7	7 4	47	4.8	20

9. TO-84 Helium R Values Variable Condition (Sheet 1 of 2)

PACKAGE TO84 - HELIUM R VALUES ELIUM VARIABLE CONDITION EVALUATION ALL DATA X10-8 ATH-CC/SEC

4 HOURS	000000000000000000000000000000000000000	7-622
90 PS16 2 HCURS	60000000000000000000000000000000000000	7.4.1 1.0.0 1.0.0
1 HOUR	00000000000000000000000000000000000000	00-00
4 HOURS	014 1 0000 000 000 000 000 000 000 000 0	7.1 1.5 1.5 1.5 1.5
75 FSIG 2 HOURS	4 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	00000
7 1 HOUR	00000000000000000000000000000000000000	00000
4 NOURS		00000 444mm
PSIG 2 HOURS	000000000000000000000000000000000000000	00100
60 L		00000
6 HGURS		00000
PSIG 3 HOURS	000 - 300 000 000 000 000 000 000 000 00	0.0 0.0 0.0 0.0 0.0 0.0 0.0
45 1 HOUR	40000100000000000000000000000000000000	0.0 0.1 0.1 0.1
8 HOURS	00000000000000000000000000000000000000	0000
PS16 4 PCU.15	00000000000000000000000000000000000000	00000
30 1 HOUR		00.2
HEIGHT GAIN	0.000000000000000000000000000000000000	0.4100000.0 0.4100000.0 0.4100000.0 0.3100000.0
VEECO		00000 444.64
NOW WENT	\$\tag{\tag{\tag{\tag{\tag{\tag{\tag{	9999

9. TO-84 Helium R Values Variable Condition (Sheet 2 of 2)

10. C-PAK Helium R Values Variable Condition (Sheet 1 of 2)

PACKAGE CPAK - HELTUM R VALUES Heltum vantable compition fvaluation all data X10-8 atm-cc/sec

4 HOURS	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2500.0 2500.0 2500.0 2500.0 2200.0 1400.0 1800.0 1800.0 1800.0
PSTG 2 HOURS	1100.0 1000.0 1000.0 65.0 750.0 750.0 750.0 750.0 1200.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1700.0 1	1500.0 57.0 57.0 57.0 60.0 1000.0 1000.0 1000.0 700.0 1000.0
90 1 HOUR	10000000000000000000000000000000000000	1500.0 1500.0 1500.0 1000.0 1000.0 2000.0 2000.0
4 HOURS	1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000	12000 12000 12000 12000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000
5 PS16 2 HOURS	4,4,4,1,0,1,0,1,0,1,0,1,0,1,0,1,0,1,0,1,	28000 28000 28000 28000 28000 28000 10000 150000 150000
1 HOUR	10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 100000 10000 10000 10000 10000 10000 10000 10000 10000 100000 10000 10000 10000 10000 10000 10000 10000 10000 100000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000	25000 25000 25000 25000 25000 25000 25000 25000 25000 25000
4 HOURS	00000000000000000000000000000000000000	3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 100.0
2 HOURS	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1000.0 2400.0 2400.0 1000.0 1000.0 600.0 600.0 1000.0
1 14008	20000000000000000000000000000000000000	2001.0 2006.0 3000.0 1000.0 1000.0 1000.0 1000.0 1000.0
6 HOUNS		300.0 240.0 240.0 240.0 240.0 240.0 240.0
asig 3 Hours	1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000 1000	2000-0 3000-0 3000-0 1500-0 3000-0 3000-0 701-0 701-0
45 1 HOUR	24 00 00 00 00 00 00 00 00 00 00 00 00 00	3000.0 2000.0 700.0 700.0 4.0 800.0 14.00 14.00 14.00 16.00 76.0
9 HOURS	0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000 0000	12000 3500 2500 2500 2500 2500 1200 4500 5500 7500 7500 7500 7500 7500 75
30 PSTG 4 HOURS	100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 10000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000	30000 30000 30000 30000 30000 30000 30000 30000 30000 30000
30 1 HGUR	0.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
WEIGHT		1001
INITIAL	3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0	
UNIT NUM.	1284844444666228622862286286666666666666	8 8 9 4 4 4 4 4 4 4 4 6 8 8 8 8 8 8 8 8 8 8 8

PACKAGE CPAK - HELTUM R VALUES FLIUM VARIABLE CONDITION FVALUATION All DATA XIO-8 ATW-CC/CEC

4 HAIPS	1200.0	650.0	2.9	5.5	9.0	۲۰۰	250.0	1200.0	0.0071	0	650.0	2007	2200.0	0.1	e :	240.0	0	9.0	e .	- 000	260.0	12000	0.0	1 500.0	1.5	0000	1200.0	0.00	1000	2000.0	4.0	0.0001	2000	2900.0	E-1	0.000	300.0
90 PSIG 2 HUURS	0.029 0.03	*	3.5	1.1	0.7	0.5	240.0	1000	0.09	1.0	200.0	4.000	320.0	35.0	Ξ,	120.0	9.0	9.0	e •	2.1.2	130.0	820.0	0 0 0 0	0.00	1000	220.0	0.0005	2000	1200.0	450.0	0.0	0.0001	9.0	3000.0	\$ 0 0 0	900	21.0
9 1 HPUR	750.0	300.0	1.6	0.1	0	1.0	0.4	3000.0	2000.0	0	1000.0	e c c c c	650.0	0.6	1.2	2002	4.0	2.5	0.2	1.5	0.2	550.0	m. 0	0000	2200.0	1000.0	700.0	2000	2000-0	2500.0	0.2	1000.0	3,000.	3000.0	r.0	2001	1000
4 HOURS	1100.0	7.0	2900.0	• •	::		r. 0	750.0	- 6	2.3	1100.0	0,0	200-0	0.5	1.9	0.001	2.0	1.6	4.0	2000	1900.0	2300.0	5.000	380.0	4.2	1200.0	750.0	26001	1300.0	1800.0	29.0	950.0	30000	550.0	0.1	22000	220.0
5 PS1G 2 HOURS	1003.0		470.0	0.5	0.2	0.7	~ 9°0	2100.0	350.0	0.3	43.0	9.00	0.009	0.3	3.2	0.00.0	0.0	3.0	4.0	35.0	0.0	1300.0	6.0	3000-0	4.0	350.0	850.0	0.00	1:00	150	**0		7:0-5	3000.0	200		1300.0
7 1 HOUR	500.0	450.0	0.3	. o o	-	0.6	160.0	550.0	75.0	0.7	850.0	1.0	0.006	170.0	2.0	250.0	0.0	1.0	7.1	- 6	0.0	100.0	4.0	300.0	0.5	350.0	1500.0	20051	650.0	750.0	0.0	2.0	3000	400	4.0	0.00	2500.0
4 MOURS	140.0 3000.0 3000.0	0.000	24.0	3000	1.4	1.0	.00	0.1	120.0	500.0	3000.0	3000.0	2002	0.4	100.0	0.87	0.1	0.8	0.86	120.0	100.0	2.0	3000.0		3000.0	9.0	3000.0		0.00	3000.0	9.0	0.001	3000.0	300.0	3000.0	2000	100.0
PSIG 2 HOURS	1000.0	250.0	3000	120.0	9.0	1000.0	3000.0	700.0	0009	1 90.0	0.04	2000.0	1800.0	3000	1200.0	200	0	2.0	3000.0	3000.0	0.004	1.5		0.0021	3000.0	140.0	1000.0	2000	350.0	30.0	1200.0	20.0	1800-0	3000.0	3000.0	1200	1500.0
60 1 HOUR	850.0 35.0 550.0	220.0	0.0	200.0	380.0	450.0	300.0	75.0	120.0	40.0	1200.0	750.0	1100.0	1700.0	200.0	1400-0	3.2	1.0	320.0	2000	620.0	9.0			2000-0	58.0	780.0	1300.0	120.0	0.5	650.0	100.0	250.0	1000.0	520.0	0.00.1	1700.0
6 HOURS	3000.0	5.6	247.0	360.0	0.3	3000.0	3303.0	3000.0	3000.0	320.0	0.096	3000.0	160.0	9.44	7.7	9 6	9.0	6.0	3000	3000	0.001	0.0	0.00	1.2	3000.0	200.0	3000	0000	520.0	0.6	3000.0	0.009	3000.0	3000.0	3000.0	3000	3000
PSIG 3 HOURS	2000.0 3000.0 780.0	3000.0	100.0	1000.0	0.3	700.0	1500.0	700.0	1500.0	3000.0	3000.0	7300.0	5005	1000.0	1.0	V 6.	9.0	7.0	3000.0	3700.0	150.0	0.2	6.0	6.00	20002	\$00.0	3000.0	0.000	0.004	4.0	3000.0	30000	3000.0	2000-0	3000.0	0.000	1000.0
45 1 HOUR	1000.0 500.0 3000.0	1200-0	1.2	700.0	900.0	800.0	1400.0	1400.0	1200.0	700.0	200.0	1700.0	3000	2600.0	2500.0	9800	1.2	3000.0	2200.0	2600.0	2,000	3.0	- · · · ·	8.00	3000.0	0.09	1800.0	2200.0	220.0	20.0	1400.0	2000	1000.0	1500.0	1300.0	820.0	2000-0
8 HAURS	1000.0	280.0	120.0	0000	0.0	300.0	300.0	696.0	20.0	100	50.0	0.00	0.00	1200.0	0.0	2.5		0.04	400.0	100.0	00.00	1000.0	0.00	0.00	600.0	200.0	700.0	2000	0.009	6.0	200.0	150.0	180.0	800.0	250.0	0.00	400.0
30 PSIG 4 HOURS	1.0	3000	9	200.0	9.0	3000.0	3000-0	3000.0	3000.0	9.0	0.8	3000.0	0.000	30000	3.2	320.0	0.1	4.0	3000.0	3000.0	3000.0	0.1	3000.0	5.00	3000.0	3000 • 0	3000.0	3000	3000	2.8	3000.0	80.0	3000.0	3000.0	••	3000.0	30000
30 1 HOUR	100.0	300.0	200	125.0	0.1	740.0	200.0	220.0	0 ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °	0.1	30.0	2000	3000	40.0	2005	170.0	0	100.0	800.0	140.0	0.009	0.1	- 0	0.00	6009	60.0	450.0	200.0	200.0	9.0	900.0	0.0,	0.004	180.0	160.0	2000	400.0
KE IGHT GA I N	10000.0	10000.0	10000	10000	10000.0	10000	10000.0	100001	10000	10000	10000-0		0.0000	0.4100000.0	00.0100000.0	28.0100000.0 6.0100000.0	1000	0.00000	0.0000	000000	100.0100000.0	0.00000	0.0000	0.3150000.0	1,000	0.00000	3000.0100000.0	0.0000	0.8100000.0	3000.0100000.0	8.0100000.0	000000	200.0100000.0	300.0100000.0	3000.0100000.0	0.0000	1 00000
TNT TAL VFECO	140.0 3000.0 3000.0	30.0	24.0	3000.0	1.4	1.0	10.0	0.1	120.0	5000	3000€	3000.0	200-01	0.41	100-01	10.82	1.0	0.81	95.01	120.01	100.001	2.01	3000.01	0.31	3000.0	19.0	3000.01	10.041	18.0	3000.01	8.01	10001	3000.01	300.01	3000.01	20.00	100.01
UNIT VUM.	25.52	4 v 4 v	\\$\	5.4	2 %	09	3	63	4.4 8.4	9	67	89	2 2	=	22	7.3	75	42	7.	2 2	2 &	8	85	6 %	82	8	۶,	n c	6 6	16	35	93	4 6 4 6	8	4	200	100

10. C-PAK Helium R Values Variable Condition (Sheet 2 of 2)

11. C-DIP Helium R Vaines Variable Condition (Sheet 1 of 2)

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11. C-DIP Helium R Values Variable Condition (Sheet 2 of 2)

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5 PSIG 2 HCURS	-0 w 4 -	.wood	100-000 100-000	#000000 #000000	, , , , , , , , , , , , , , , , , , ,	0 4 4 4 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
, HCUR	40-04		00 100 4000 00 100 4000	~00~0m~00	20	00W 40 40 40 4 4 5 4 6 4 6 4 6 6 6 6 6 6 6 6 6 6 6 6
> HUlib &	64700	44.000	0 a 4 a a a o l	2,007 2,007 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000 2,000	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
PS IG 2 HAURS	~~~~	0 + v 4 0 v + c	466-0400-	120 C C C C C C C C C C C C C C C C C C C	000001100001	4400000
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A HOURS	-0000			, c c c	000021 m 00000	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
P\$16 3 Hn [.] JoS	-0.00 -0.00 -0.00 -0.00		6 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		00-00-00-00-00-00-00-00-00-00-00-00-00-	00000000000000000000000000000000000000
1 40HB	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				344444400046	
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12. MOS DIP Helium R Values Variable Condition (Sheet 1 of 2)

ILIUM VARIABLE CONDITION R VALUES
ILIUM VARIABLE CONDITION EVALUATION
ALL CATA X10-8 ATM-CC/SEC

4 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.		٠. د	000	1.0		3000	3	3000	;	0	4:5	1300.0		90		3.C	1.0		3	3000	3.0008	30000	30000	650.0	0.000	v. 0	£•3		1000	0.000	30000	0.069	3000	3000	3000	30000	3000				2.0	•	•
90 PS16		3	000	2	4.0	250C.C		750.0	;		C.2	0.006	֓֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓		3	0.4	e.0	C.2	4.0	3000	2800.0	3000	850.0	120.0	2400.0	20	£-3			0.00	180.0	500.0	2000	2500.0	250.0	15CC. C	3000	4.0	•		S-2	٠ د د	,
- and a		 											ָּטְיּע מיילי		9.0	0.2		~	-	700.	3400.0	3000	500.0	10001	30006	2.3	0.1	B • 0	• • • • • • • • • • • • • • • • • • • •	2000	500.0	3000.0	20002	0000	2600.0	1 €00 · C	2500.0	000	•	9	1.6		
¥ dich					3.5	3000.0	9.0	3000.0	•	1.0	2 · C	0.1	-	9.0		9.0	6.0	5.0	0.1	3000	3000.0	3000	3000.0	÷.0	3000	0.0	0.3	0	3.0	0000	30005	3000.0	3000	10000	30000	30000	3000		•		1.5	~. •	•
75 PS16		e .		907	0.5	30000	0	1400-0			0.0	266.0	 		0	0.3	1.0	0-2	e.	3000	3000	3000	2500.0	4.0	2500.0	2.0	0.3	1.5	300.0	0.000	2000-0	30000	2000.0	3000.0	3000	3000-0	2500.0	2.0	; -	3000.0	0.1	9.0	•
7	•	0,0		9	4.0	2800.0	0.0	950.0	•	9	0	0.1	-	4	•	0.0	0.0	0.5	**	3000	0.0000	2700.0	2500.0	0.1	2200.0	0.0	0.1	0-5	40.0	30000	3000	30000	3000	3000	30000	30000	3000.0	9-1	;	7.5	4.0	0 9	
S SHOPE 4		0-	3000	150.0	0.1	3000.0	2005	2.0	0000	200.0	0.2	3000.0	9	1.	0.1	0.2	1.0	•	0.0	3000-0	3000	3000.0	3000.0	3000.0	0.000	7.0	7.0	9.0	1.00%	3000-0	3000€	180.0		220.0	3000.0	220.0	0°00 °	0.0		0	0.2	1.0	;
PSIG 2 HOURS				0.1	0.2	3000	0.00	ם פרות היים מות היים		9	0.0	3000	0 4	0	0.3	0.0	1.0	0.2	4.0	3006	3000	3000	3000	0	00000	0,3	0.3	- 0	9 00 00	3000.0	3000-0	2800.0	0000	3000	3000-0	3000	3000			1.2	0.5	9.0	;
990H I	•	0.0		0.2	0.0	1600.0	0.0	1200-0		0	0.1	1.0	5 6	0	0.0	4.0	0.2	•	0.0	3000	2400.0	2000.0	1000.0	0.0	2500-0	4.0	0.0	0.0	2000	420-0	2600.0	3000	1300	3000	2300.0	1 700.0	1800.0	9 6		9	0.3	• ·	•
S HOURS		0,0	7.0	0.0	0.0	28.0	0.0	1800		0	0.0	2400-0		0	0.1	0.1	0.0	0.0	0.0	2800.0	3000	3000.0	20002	1.0	3000.0	0.1	0.0	4.	1.000	3000.0	3000.0	0.000	0000	3000	3000.0	3000	3000	7 9 0	0	0	S . 0	m 4	•
PSIG 3 HCURS		C .	0		0.2	2500.0	**0	20002	,	9	0.3	30000		0	0.1	9.0	4.0	B (0.3	30000	3000.0	3000.0	2200.0	1.0	3000.0	8.0	0.7	9.0	0.000	3000	3000.0	3000	0.000	3000.0	3000-0	1800.0	3000	9 0	2	0.1	1.0	2.7	:
45					7.0	2200.0	4.0	10001	-	•	1.2	0.3			0.3	0.4	••	v. 1	1.1	30005	2800.0	3000	1500.0	1.6	1500-0	2.1	0.1	9.	000	3000	30000	2000-0	3,000	3000	3000.0	3000.0	3000	2.0	, ,	0.0	1.0	0.4) •
A CLIBS	•	0.0		0	0.1	1400-0	0	820-0		0	0.0	•		0	0.0	0.2	0.1	0.2	9.0	000	2800.0	3000.0	2100.0	3000	1400.0	3.1	0.1	m •	10000	3000	3000.0	1800.0	2000	1200.0	2000.0	1500.0	2800°C	0 0		0.2	1:5	0 0	;
PSIG 4 HOURS				0	0.0	3000-0	0.0	3000			0.0	C+2	7.0		0	0.0	0	0.0	9.6	300056	30005	3000	30000	3000	3000	9°0	1.0	٠ ن	0.000	3000	3000.0	3000.0	00000	3,000	3000	3000	3000.0	7.7		0 12	C•5	٠ • •	;
30	•	•	<u>.</u>		•	1000	•	8												120	280	300			3,000.0	•			•					3000		3000	2200	0-	:,	; «	-	~; ~	•
WEIGHT		1000		1000	1000.C	1000	10001	00001		10001	1000	1000.	0001	1000	1000	10001	10001	1000	10001	1000	10000-0	10000	1CC00.C	100001	30000 0 10000 0	0-000001	1 CCC00. C	0.000001	0.000001	1000001	1000001	2.00001	0.000001	00000	0.000001	0.000001	1000001	0.00001		0.000001	1000001	0.000001	•••••
INITIAL																																											
TIND		25	2 5	5,7	53	26	52	ω :	7	6.5	9	63	40	9	67	69	69	2	Ξ:	72	2 7	25	2	77	78	. 8	£1	85	5	.	£ 6	67	80 0	6 6	76	85	93	% d		9.2	85	25	3

12. MOS DIP Helium R Values Variable Condition (Sheet 2 of 2)

PACKAGE TO100 - HELIUM R VALUES
HELIUM VARIABLE CCNCITION EVALUATION
ALL DATA Y OLD ATM-CC CEC

	4 HOURS	6.1	-	~~	-:				2.7	2.0			1.5	4.	•••		1.4	5.0	1.6			, .	2.0	1:4			320.0		6.0	, ,		* -	200		65.	~	2				7.7	0
	90 PSIG. 2 MOURS	9,0	. 6		1.2	~ .	0	0	0.5	ب د د د	7.	. 0	1.7	••	2	9.00		2.5	9.0	1.4	•		.0	1.2	9.1	9.0	2005	4.5	•••	• •	10.01	4.5	0.000	5000	25.0	1:0	0.00	9.0	0000	-	0.7	S
	90 1 FCUR	4.6		•	3.0	•	7 4	9.0	0.7	e .			2.0	3.0	1.6	0.000	1.4	3.0	9.0	3.0	7.			1.2	2.5	200	150.0	6	9.0		8		200.0	4.00	16.0	٠ ٠	0.02	,007	ייים טייני	~.0	1.2	•
	4 HOURS	2.1	1.3	?:	8.0	6 ·			1.0	2:5	, ,	9.1	0:-	c. 5	1.000	2.000	65.0	1.2	1.4	1.4	0.	- e		::	260.0	4.6	2000	60.04	4.0		10.01	1.2	220.0	2	25.0	:	2002	0.054	0.000	. m	70.0	71.0
	S PSIG 2 HCUPS	8 4		2.	3.6	9:0	 		3.5			, c	1.3	3. B	7.1.2	1.000.0	2,6	. 5	1:6	1.5				1.6	ن د د	0,0					1.2	1.9	90.0	n C	10.0	6.4	80.0	1000	2000		١.٥	
	1 HOUP	- c	0	2	3.0	5.0		6.1		· ·	- 0	•	α.	v • •		9	-		1.4	<u>-</u>	s .		-	ć, c	٠ :		0.001	C.				1.3	70.0		10.0	5.0	55.0	210.0	0.000		1.8	5.2
	4 HCURS	0.1		1.7	1.0	0.1) C	1.0	1.0	0.1	0 4	1.0	10.0	20.0	0.000	12.0	200	7.0	0.1	1:	0.00	0.009	20.05	30.0	2005	0.004	700.0	3000.0	2000	2000	120.0	50.0	7007	2002	120.0	30.0	700.0	3000		3000	30000	3000.0
:/sec	PS 1G 2 HOURS	1.8	0	4.0	2°8	7.1		0.0	1.6	~ .	,,,	7.	2.C	1.0	æ. (2.6	4	3.6	3.2	7.0	5. 7.	0.009	1.6	 	0.44	2 4	70.07	70.0	240.0	28.0	24.0	7.4	280.0	0.04	20.0	2°C	2.04	3000	30000	240.0	94.0	24.0
D-8 ATM-CC	60 1 HOUR	0.0	000	0.5	3.5	0,0	9.0	0.3	0.5	· ·	2.0	2.1	5.0	0.8	7.2.7	8.4	1.5	2.0	1.4	5 · 0	0,0	13.0	4.0	2.1	100.0	200	120.0	75.0	20.0	, v	0.9	1.4	400.0	0.05	6.5	6.5	85.0	250.0	0.000	65.0	1000.0	35.0
. DATA X10	6 HOURS	2.5	4 4	1.2	0.4	0,0	2 4	0.0	0.4	2.0	0 0	9.0	1.6	3.0	200		2.5	5.5	7.0	5.4	5,00	20.0	1.2	12.0	2000	26.0	2000	180.0	1800.0	24.0	28.0	15.0	0.009	2,000	25.0	1.6	280.0	0.00	1300	500.0	780.0	400.0
ALI	PSIG 3 POURS	0.1	1.2	0.8	1.2	2.0	0 1	7.0	1.2	7.	-	. 0	0.e	1.3	1.3	0.000	7.	0.1	ڻ• ئ د	0.5	0.4	120.0	8.0	9.0	300.0	0.0	220-0	200.0	200.0	22.0	20.0	1.0	280.0	0.000	14.0	0.8	150.0	0.000	0.000	250.0	5.4	400.0
	45 1 HOUR	2.0																																					_	•		
	8 HOURS	9.0	0.0	v.	1.0	0.0	- 9-0		0.2	0.5	2 v	0.0	G. 5	0.5	200	200		5.6	6.5	1.0	 	120.0	4.4	1.0	510.0	23.0	7 016	380.0	310.0	2,00	45.0	1.3	290.0	230.0	27.C	5.2	250.0	0.009	1100.0	410.0	2000	500°C
	30 PSIG 4 HOURS	5.0		0	2.0	œ٠		0.0	9.6	7.2	7 0	1.0	1.2	0.7	9.9	2.000	5.4	2.1	1.2	1.2	3.0	0.00	1.5	0.2	720-C	42.0	1 0 5 7	480.0	420.0	7.4.0	42.0	1.3	300.0	0.00	14.0	0.6	300.0	8.0	3000	380.0	150.0	3000.0
	30 1 HOUR	9,0	0.0	, v.	0.3	o.,	0.0	6.2	0.5	0.7	4.0	350.0	0.2	0.4	0.5	1.5	0	0.2	0.7	0.3	v .	26.0	3.6	2.0	100.0	2.5		3000.0	90.0	9 0	9	0.3	20.0	200	8	1.5	55.0	100.0	260.0	100.0	120.0	190.0
	WEIGHT GAIN	٥ د د	0.0		0.0	0.0		, ,	0.0	٠ ن	,,	90	0.0	0.5	¢ • •	် ပ	0	0	ر. ن		0.0	9	0	0.0	0-0	0.0	، ر د د	0.0	0.0	90	0.00	0.0	0.0			0.0	0.0	0.0	٥ د د		0	c°°
	INITIAL VEECO	2.6		2 . R	٠.٠	0.0	, c		6.0	2.6	2.0	2 6 6	15.0	63.0	æ. (, o	31.0	15.0	2.4	4.4	91.0	0.000	147.	53.0	30000	6.000	0.000	3000.0	3000.0	0.000	3007	220.0	3000.0	9,000	30000	130.0	3000.0	3773.0	3000.0	3000.	3000.0	3333.0
	UNIT NUM.	(v «	4	ď	· .	~ α	0	10	= ;	21	<u>.</u>	. 2	19	7	<u>.</u>	20	212	22	23	5,5	, ,	2.5	58	53	č.	15	3.6	36	5 1	37	38	8	Ç :	42	43	55	45	9 ;	4 4	67	5,

PACKAGE TUIOO - HELIUM R VALUES HELIUM VARIABLE COMDITION EVALUATION ALL DATA XIO-8 ATM-CC/SEC

SHILLS 7	2000.0	2000 2000 2000 2000 2000 2000 2000 200	100 000 000 000 000 000 000 000 000 000	4000 4000 6000 6000 6000 6000 6000 6000	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
ON PSIG PHOURS	550 550 0.00 5.00 5.00	30000 30000 30000 30000 30000 30000	2000 2000 2000 2000 2000 2000 2000 200	20000000000000000000000000000000000000	2500.00 2500.00 2500.00 2000.00 2000.00 2000.00	
NOUP (3502	00000	3000 825.00 30000 30000 30000	300000 300000 300000 30000000000000000	2000 2000 2000 1000 1000 1000 1000 1000	000000000000000000000000000000000000000
4 HCURS	0.000 0.000 0.000 0.000 0.000	166000 166000 1660000 16600000000000000	1000 1000 1000 1000 1000 1000 1000 100	000 0000000000000000000000000000000000	25 25 25 25 25 25 25 25 25 25 25 25 25 2	300000000000000000000000000000000000000
75 PSIG 2 MOURS	004	30 00 00 00 00 00 00 00 00 00 00 00 00 0	3500 42.6 12.2 15.0 1600.0	200 200 200 200 200 200 200 200 200 200	12000 12000 13000 13000 18000 18000 2500 25000	300000000000000000000000000000000000000
7 1 HOUR	250 270 200 200 200 200 200 200 200 200 20	20074 20074 20070 20070 20070 20070	2,000.0 2,000.0 2,000.0 2,000.0	C.000E	2000 2000 3000 4000 2000 2000 2000 2000	32000 30000 30000 30000 30000 30000 30000 30000 30000
4 HOURS	300000	300000 300000 300000 1.1	000000000000000000000000000000000000000			
PSIG 2 HAURS	1600.0	300000 300000 300000 1.00	3000.0 64.0 360.0 3000.0	MW W W W W W W W W W W W W W W W W W W	34440 34600 34600 34600 5400 5400 5400 6600 6600 6600 6600	200.0 200.0 2000.0 1,600.0 3000.0 3000.0 3000.0
60 1 HOUR	400.0 300.0 120.0 300.0	24000 34000 24000 24000 18000	3000 12000 30000 30000 50000	30000 30000 30000 30000 30000 30000	1200.0 3000.0 1400.0 1200.0 1200.0 1600.0 1600.0	3500.0 3000.0 3000.0 3000.0 3000.0 3000.0
6 HOURS	1400.0 1600.0 700.0 3000.0	120000 140000 300000 00.3	3000.0 220.0 3000.0 1800.0 500.0	180000 180000 10000 10000 12000 12000 12000	3000.0 3000.0 3000.0 3000.0 1600.0 1750.0 300.0	20000000000000000000000000000000000000
PSIG 3 FOURS	100°C 530°C 620°C 1600°C		150000 150000 170000 30000 30000	2000.0 2000.0 2000.0 3000.0 3000.0 2000.0	250000 250000 250000 250000 250000 250000 250000	
45 1 HCUR	250.0 140.0 170.0 200.0	2000.0 2000.0 2000.0 2000.0 230.0	3000.0 1000.0 2200.0 270.0 380.0 2300.0	2400.0 2300.0 270.0 450.0 3000.0 400.0	1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 1200-0 12	266.0 3000.0 700.0 2500.0 3000.0 3000.0 3000.0 2500.0
8 HCURS	790°0 900°0 1000°0	100000 1100000 300000 300000 120000	3000-0 400-0 1200-0 1500-0 100-0	3000.0 3000.0 1360.0 2300.0 1500.0 1900.0	30000 16000 30000 19000 23000 15000 15000 3000 15000	12000 30000 23000 30000 30000 30000 30000 30000
PS 16 4 HOURS	3000.0 3000.0 3000.0	# # # # # # # # # # # # # # # # # # #	750-0 3000-0 3000-0 3000-0	00000000000000000000000000000000000000		
30 1 HOUR	100.0 120.0 220.0 270.0	30000 30000 30000 30000 30000 30000	3000.0 100.0 3000.0 3000.0 3000.0 3000.0	3000.0 3000.0 3000.0 8000.0 200.0	3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 3000.0	30000000000000000000000000000000000000
WEIGHT			000001		1000000 1000000 1000000 1000000 1000000 1000000	
INITIAL	32000.0	30000 30000 30000 30000 30000	3000 4000 4000 4000 4000 4000 4000 4000			
UNIT NUM.	20 67 50 50 50 50 50 50 50 50 50 50 50 50 50	6 6 5 9 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	66 65 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		999 999 999 999 999

13. TO-100 Helium R Values Variable Condition (Sheet 2 of 2)

PACKAGE CERM - HELIUM R VALUES HELIUM VARTABLE CONDITION EVALUATION ALL DATA X10-8 ATM-CC/SEC

4 FOURS	240.0 240.0 30.0 450.0	1300.0 1300.0 1500.0 60.0	200.0 200.0 3000.0 2500.0	30000 30000 30000 30000	30000000000000000000000000000000000000	3000.0 3000.0 450.0 100.0 100.0 3000.0 3000.0 3000.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 120.0 1
O PSIG 2 HCURS	0.00 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	250.0 250.0 250.0 70.0 100.0	0.001 0.007 0.000 0.000 0.000 0.000	2000 2000 2000 2000 2000 2000 2000 200	30000000000000000000000000000000000000	350.0 120.0 120.0 120.0 120.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0
1 KOUR	20000000000000000000000000000000000000	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	100.0 52.0 52.0 3000.0	300.00 300.00	3000 3000 3000 3000 1000 1000 1000 1000	3000.0 1 900.0 1 900.0 2 0.0 2 0.0 3 0.0 4 0.0 1 3 0.0 1 3 0.0 1 3 0.0 1 5 0.0 1 5 0.0 1 5 0.0 1 5 0.0
4 HOURS	0.0000	00000000000000000000000000000000000000	100.0 200.0 200.0 100.0 150.0	390.0 390.0 130.0 1400.0	3000 8 1 2000 1	3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 260.0 260.0 1100.0 350.0
75 PS IG 2 HOURS	35.0 35.0 1.65.0 25.0 1.65.0	22.00 22.00 22.00 22.00 22.00 15.00	150.0 150.0 150.0 100.0 100.0 100.0 100.0	240.0 65.0 110.0 700.0 80.0	30000 13000 30000 4200 30000 30000 30000	3000.0 200.0 1000.0 250.0 300.0 300.0 100.0 50.0 240.0
1 HOUR	34.0 24.0 24.0 8.0	20.0 20.0 20.0 20.0 17.0	15.7 55.0 85.0 35.0 3600.0 260.0	100.0 100.0 110.0 75.0	21000 18000 210000 3500 5000	3000.0 1000.0 1000.0 1000.0 300.0 300.0 300.0 400.0 400.0 400.0 400.0 400.0 400.0 400.0 400.0 400.0 400.0
4 HOURS	10.00 10.00 10.00	200 1200 3000 1500	22000000000000000000000000000000000000	0.00 0.00 0.00 0.00 0.00 0.00	0000 0000 0000 0000 0000 0000 0000	20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000 20000
PS1G 2 HOURS	70.0 17.0 17.0 14.0 180.0	16.0 12.0 10.0 27.0 10.0	25.00 25.00 25.00 25.00 25.00	100.0 100.0 78.0 220.0 31.0	3000.0 37.0 3000.0 38.0 80.0 41.0	38.0 1000.0 1000.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250.0 1250
60 1 HOUR	34.0 8.0 12.0 12.0	150.0 120.0 120.0 120.0 120.0	7,4 m m m m m m m m m m m m m m m m m m m	20000000000000000000000000000000000000	3000.00 3000.00 3000.00 3000.00 3000.00 180.00	30000 1700 1700 1700 1700 1700 1700 1700
6 HOURS	55.0 60.0 25.0 4.5 100.0	17.0 33.0 30.0 100.0 10.0	26.0 26.0 26.0 26.0 26.0 26.0 26.0	2,04,0 2,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,04,0 1,	3000-0 100-0 100-0 100-0 100-0	300000 12000 12000 12000 30000 30000 5000 6000 6000 12000 7000 7000 7000 7000 7000 7000
PSIG 3 HOURS	11.0	000000000000000000000000000000000000000	2000 2000 3000 3000 3000 3000 3000 3000	100 100 100 100 100 100 100 100 100 100	300000 300000 60.00000000000000000000000	28000 48000 8600 8600 8600 30000 5500 90000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 800000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 800000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 800000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 800000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 800000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 800000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 800000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 80000 800
45 1 HOUR	30.0 6.0 21.0 30.0	0000 000 000 000 000 000 000 000 000 0	25.00 25.00 25.00 25.00 25.00 25.00	2,000000000000000000000000000000000000	200.0 200.0 3000.0 100.0 22.0 80.0	300000 10000 12000 12000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000 14000
8 HOURS	2000 1000 1000	18000 18000 18000 18000	200000000000000000000000000000000000000	120.0 120.0 25.0 40.0 30.0	2600 2600 2600 2600 2600 1600	300000 10000 10000 10000 30000 2400 1500 10000 10000 10000
PS 1G 4 HOURS	27.0 27.0 12.0 19.0	001 004 008 008 008 008	85.0 85.0 100.0	200.0 200.0 120.0 120.0	3000-0 15-0 3000-0 15-0 15-0 15-0	3000.0 15.0.0 15.0.0 3000.0 3000.0 3000.0 3000.0 18.0
30 1 HOUR	100.0 10.0 1.3 62.0	2.4.7. 2.4.0.8. 2.4.0.8. 3.4.0.8.	11.00 22.00 22.00 22.00 22.00	855.0 12.55.0 12.55.0	200 200 200 7.9 200 780 190 110 300	30000 10000 30000 30000 1000 1000 1000
WE 1GHT SA I N	750.0 0.0 0.0 0.0	565.000.000.000.0000.0000.0000.0000.000	758.0 0.0 0.0 0.0 0.0 0.0	0.0 0.4 0.0 0.0 710.9	849.1 849.1 841.0 842.1 810.5 729.2 818.1	7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
VEECO	18.0 20.0 17.0 10.0	000 K T K K	20.00	% % % % % % % % % % % % % % % % % % %	3000 3000 3000 3000 3000 4000	30000 1000 1000 1000 1000 1000 400 400 500 500 500 1000 10
UNIT NUM.	⇔⊘ ₩ψ≥₩	0	245 27 8 27	25 25 25 25 25 25	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	% % L & & & 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4

14. Ceramic Helium R Values Variable Condition (Sheet 1 of 2)

PACAAGE CERM - HELIUM R VALUES HELIUM VARIABLE CONDITION EVALUATION ALL DATA X10-8 ATM-CC/SEC

4 HOURS	3000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 1
90 PS1G 2 HQURS	6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
9 1 HOUR	2000.0 2100.0 3000.0 500.0 500.0 650.0 700.0 110.0 130.0 130.0 100.0 100.0 100.0
4 HOURS	2000 1000 2000 2800 2800 2800 2800 2800
75 PSIG 2 HOURS	3000 55.00 107.00 1000 1000 1000 1000 1000 1100 11
7 1 HOUR	2000 3000 3000 3000 5000 5000 5000 5000
4 HOURS	3000. 300.0 300.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 10
PSIG 2 HOURS	30000 533.00 662.00 862.00 1100.00 1100.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 120.00 1
60 1 HOUR	30000 42.0 600 200 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1300 1
6 HCURS	25.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1,000.0 1
PS 1G 3 HOURS	2000 2000 2000 3000 4000 3000 3000 3000
45 1 HOUR	2000 2000 2000 2000 2000 2000 2000 200
8 HOURS	30000 60000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000
PSIG 4 HOURS	30000 4000 18000 18000 12000 2200 2200 2200 220
30 1 HOUR	3000.0 833.0 433.0 433.0 300.0 330.0 445.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0
REIGHT GAIN	00 98 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
INITIAL	30000 3000 3000 1200 3000 1200 1200 1200
WUN.	12000000000000000000000000000000000000

14. Ceramic Helium R Values Variable Condition (Sheet 2 of 2)

15. TO-3 Helium R Values Variable Condition (Sheet 1 of 2)

HELIUM VARIABLE - CHELTYPON EALDER TON ALL DATA X10-8 ATM-CC/SEC

9	200 200 200 200 200 200 200 200 200 200	30000	0 0	3000	1500.0	10.0	2000	9.00	0,7	9.0	0.7	250.0			3000	3000	3000	3000.0	3000.0	000	0 0		100	0	0.3	0,0	0	0.0		0.0	0.3	0.0	20.00	3000-0	4.0	10.0	1.8	3000-0	9.0		0.0	0.5	3000.0	
90 PSIG	2	3000	2.0	3000.0	750.0	380.0	12.0	0.4	10.01	4.0	6.0	2.0		3000	3000.0	30000	3000.0	3000-0	3000.0	200	2	0.2	1.0	0.3	0•3	0,0	, r	1	200	0.3	4.0	0.0	2 6	3000.0	0.5	15.0	2.5	3000.0	0	140.0	9.0	6•0	2100.0	
, ale	•																																										3000.0	
7 N N N N N N N N N N N N N N N N N N N	200	4.0	9 6	0	650.0	0.0	3000	0.0	0.3	4.0	 0			2000-0	3000.0	3000.0	3000.0	3000.0	3000	200		8.0	0.4	0.1	•	•				0.7	0.3	0.5	7.0	11.0	3.5	9.0	1.3	22.0	200	130.0	0.1	9.0	300.0	
75 PS16	•																																										400,0	
T HOUR		600		0.2	550.0	~ .	3000	9.0	12.0	000	2.0		110.0	3000	3000.0	3000.0	3000.0	3000.0	0.000		9.0	0.3	0.0	0.5	4.0	0.0	9 4	0.0	4.0	0.3	9.0	20.1	0	7.0	0.4	9.2	2.0	200	, v	180.0	0.0	4.0	0.00	
4 HOURS		7.0	200	2.0	0000	0.00		20.02	2.0	20.0	200	0		3000	3000.0	3000.0	3000.0	3000	0000	2.5		•0	0.5	7.0	0.0		7 0	0	8.0	0.3	**	100	2	50.0	20.0	6 : 1	2.0	75.0	25.57	120.0	1.4	2000	0.4	
PS IG		A. 6	0.8	2.4	240.0	200	4.5	1.8	6.5	0.4	0,00	•	9.9	3000.0	3000.0	3000.0	3000.0	3000-0	0.000		0.7	9.0	1.2	5.5	9•1	4.2	5,5	0	0.0	9.0	0.	7 r	0.05	15.0	45.0	0 9	18.0	• •	65.0	80.0	0.2	0.0	83.0	
1 HOUR		9	9.7	1.2	240.0	30.0	1.5	1.2	2.8	\$ · \$	7:7	4 -	2.0	3000.0	3000.0	3000 •0	3000.0	3000-0	2000	2	4.1	0•3	1.6	1.6	1.			0	1.6	2.3	1.	100	2.7	50.0	22.0	24.0		† «	30.0	0.09	2.5	2.0	1.0	
6 HOURS		3.6	0.0	0.0	260.0	200	0	0.4	28.0	2.0	200	200	9.0	3000.0	3000.0	3000	3000.0	3000	2000	5-1	0	6.0	1.0	e • 0	9.0		9	0	0.4	0.1	0	9 4	16.0	15.0	120.0	2.6	3 c		20.07	0.06	0.0	7. 0	120.0	
PSIG 3 HOURS		0 0	0.0	0.0	180-0	0.2	0	10.0	2.8	0.2		5	3.0	3 000 0	3000.0	0.0000	3000.0	2000	2000		0.1	0.0	0.2	1.0		7.00	170		0.3	1.0	8 6 0	9 0	0.0	50.0	0.59	0	18.0	900	0,00	80.0	0.1	14.0	0.4	
45 1 HOUR		2.5	0	0.0	130-0	18.0	3000 00	0.2	3.5	0.0	2.0		0.5	3000.0	3000.0	3000 -0	3000-0	3000	2000		0.0	1.0	1.9	0.9	, ,	2.5	8.0	0.0	0.8	0.2	0.0	7.8	9.0	9.1	40.0	0.0	7.	•	32.0	10001	0.0	4.0	0.0	
8 HOURS		0.0	0	10.0	250.0	• •	0	100.0	140.0	9.0	2 0		3.5	3000.0	3000.0	3000.0	2000.0	2000	2000	4.0	1 0	0.4	2.0	0.0	0.0	1.0	4.0	0.2	0.3	9.0	m .	0.0	9.0	0.09	0.09	12.0	0.00	100	0.00	150.0	0.6	80.0	0.00	
30 PSIG 4 HOURS		2.0		1.0	360.0	330.0	6.0	21.0	0.069	0.0		2.0	7.5	3000.0	3000.0	3000.0	3000.0	0.000	0000		9.0	0.1	1.9	0.0		7.6		0.0	0.1	0.2	0.0	3 4	0.5	45.0	18.0	0.0	2 6		21.0	450.0	1.8	42.0	300.0	
30 1 HOUR	<u>.</u>	0.0	35.0	3.0	180.0	2.5	2.0	35.0	2.2	0.5	0.0		7.0	3000.0	3000.0	3000-0	3000.0	0000	0.000	7.0	9.2	1.0	0.3	0.2	0.5	2	2.0	0.2	0.2	0.2	0.0	3 0	1.2	30.0	3000.0	8	9,00	7.7	3000	100.0	7.0	55.0	0.001	
WE IGHT GAIN		0 0	0	0.0	0,0		0	0.0	0.0	0.0			0.0	0.0	0.0	0.0	0.0	•		0	0.0	0.0	0.0	0.0	0.0	0 0	0	0.0	0.0	0.0	0 0	9	0	0.0	0	0.0	9 0		. 0	0.0	0.0	0.0	90	
thi tial		84.0	0	28.0	200.0	30.0	120.0	220.0	3000.0	9.0	7.0	2,6	280.0	3000.0	3000.0	3000.0	3000.0	2000	200	0.0	0.1	1.6	1.4	6.0	, o	0.0		1.0	1.2	1.6	· ·	0.051	60	0.044	200.0	120.0	0.000	0.00	3000.0	540.0	420.0	360.0	36.0	
UNIT TON		۰.	ı m	4	· v	۰ ۵	· co	σ	2	=:	2 :	7 7	: 23	2	17	8 2	<u>.</u>	₹ 7	3 6	3 2	52	52	5 9	27	829	5, 5	3 7	32	33	36	3	2 2	38	33	9	7	7:	£ 4	45	46	47	æ :	2 %	

PACKAGE 10-3 - HELIUM K VALUES HELIUM VARIABLE CONDITION EVALUAT.ON ALL DATA XIO-8 ATM-CC/SEC

4 HOURS	220.0	0.8	3000	0.000	3000-0	3000.0	300.0	3000*0	o w	0 0	400	3000.0	3000.0	750.0	0,0	2.0	2000	0.000	7		3000	3000	40.0	3000	0.000	0.000	3000	3000	3000•0	1.5	7000		3000	1800.0	2400*0	180.0	350.0	750.0	0000		3000	1.5	3000.0
90 PSIG 2 HOURS	120.0	9.0	3000-0	0000	3000	3000.0	600 00	2500-0	5.0	2000	4	3000.0	2500.0	550.0	26.0	0	200	2.5		0.00	1400.0	3000	75.0	3000.0	1000	0000	00000	3000	3000-0	1000.0	1.1	0000	3000	850.0	1100.0	0.3	240.0	20.0	190.0	0000	3000	0.7	3000.0
1 HOUR	40.0	0.3	3000.0	0000	30000	3000.0	2000-0	850.0	0.0		1.8	1000.0	1000	1 80.0	2.0	5.0		000	200	0000	450,0	3000	22.0	1000.0	500.0	3000	3000	3000	3 000 • 0	250.0	0.00	0000	3000	300.0	1.4	1.0	100	160.0	0.00	0000	3000	9•0	3000.0
4 HOURS	50.0	0.3	~ 000	4.0	0.3	3000.0	1.8	1300.0	9 4	°	0.7	3000.0	1000	170.0	200	5,0	100	,	2 2	000	1800.0	3000.0	500.0	2000-0	800.0	00000	3000	3000	3000.0	3000	0.00	0000	3000	900	3000-0	3000.0	3000.0	450.0	2220	0000	3000	1.2	3000.0
'5 PSIG 2 HOURS	45.0	2.0	5000	2000	1	3000.0	0.7	800.0	n (9.0	100	2600.0	2000	450.0	0.12	200	0.00	000	0.00	2000	0000	30000	100.0	1000.0	650.0	3000	30000	3000	3000.0	1000.0	3000		3000	450.0	800.0	440.0	120.0	150.0	100.0	0000	3000.0	4.5	3000.0
7 1 HOUR	6.5	0.3	~ °	4.000	0.3	3000.0	0.0	1207.0	0.0	0	1.5	2900.0	100.0	220.0	28.0	0,0	0.00		2 4	000	900	3000.0	120.0	1500.0	750.0		3000.0	3000.0	3 000 0	1.8	6.1000	0000	3000	700.0	1000.0	• 1	100.0	160.0	110.0	0.000	3000	0.1	3000.0
4 H0JKS	55.0	2.0	0.04	4.0	0.0	3000 .0	130.0	0.0001	• ^	7.0	300.0	0.00+	800.0	100.0	1000		0000	2000	2007	3000	2000.0	3000.0	300.0	2000-0	3000-0	0000	3000-0	3000	3000.0	3000.0	2.000		30000	1000	0.5	30000	3000	80.0	0000	0.0004	3000.0	12.0	3000.0
PS1G 2 HOURS	55.0	2.0	V . C	8 -1	2.4	3000.0	0.6	200	200	0	180.0	170.0	350.0	120.0	2000	180		0.00	20.0	3000	1000	3000.0	1204.0	1800.0	9000	0000	3000	3000.0	3000.0	3000*0	12.0		30000	550.0	0.3	3000.0	3000.0	0.001	2000	1300-0	3000.0	9•0	3000.0
60 1 HOUR	31.0	0.6	2000	4.0	2.0	3000.0	1.7	170.0		7.4	78-0	110.0	120-0	70.0	0.0	200	,	26.45	70.0	3000	20000	3000.0	160.0	650.0	250.0	30000	3000	2900.0	30000	2200.0	5.0		3000-0	300.0	1.4	30000	3000.0	0.89	0.00	2000	3000	2.9	3000.0
6 HOURS	90•0	0.0	0.00	0.000	*	3000.0	20-0	480.0	2.5	0.0	240.0	240.0	4,60.0	140.0	0.08	1000	0000	2000	200	3000-0	3000.0	3000	120-0	3000.0	3000-0	2000	3000-0	3000-0	3000	3000.0	7555	00000	3000	3000	2.0	3000-0	3000-0	100.0	280.0	0000	3000.0	2•0	3000.0
PS IG 3 HOURS	0.004	4.0	14.0	200	0	3000.0	30.0	120.0) r	0.0	0.001	2000	250.0	82.0	0.07	0.001	100			0.000	750.0	3000	100.0	1000	2400-0	2005	3000	3000	3000-0	3000.0	1.0	2000	3000	500.0	0.2	3000.0	3000.0	200.0	3000		3000	1.0	3000.0
45 1 HOUR	31.0	0.0	1.0	2000	0	3000.0	0.5	1.0	::	-	55.0	88.0	180.0	55.0	0.0	80.0	200	2004		0.00	2000	3000	100.0	800.0	180.0	3000	0.000	3000	2800.0	2600.0	7-7	2000	3000-0	2000	0.3	3000-0	3000.0	53 •0	0.00	0.000	3000*0	0.2	3000.0
8 HOURS	120.0	25.0	140.0	3000	200.0	3000.0	220.0	400.0	0.00	120.0	300 • 0	100.0	400	180.0	120.0	280.0	240.0	0.0021	0.007	0000	1400-0	3000	1000.0	2200.0	3000-0	3000	0.000	3000	3000-0	3000.0	260.0	1800-0	0.000	2002	3000	3000.0	3000.0	2001	350.0		3000	1.0	3000.0
PSIG 4 HOURS	72.0	30.0	30.0	30000	2.1	3000	30.0	720.0	3000.0	0.024	270-0	450.0	390.0	39.0	390.0	210.0	600.0	200	0.000	2000	3000.0	3000	0.0	3000.0	3 000 • 0	3000.0	3000.0	3000-0	3000	3000.0	3000-0	3000.0	0.000	3000-0	3000	3 0000	3000.0	39.0	3000.0	3000	30000	0.3	3000.0
30 1 HOUR	76.0	0.8	0.09	0.004	0.0	3000	100.0	280.0	1.2	0.00	140.0	18.0	240.0	100.0	80.0	160.0	0.09	350.0	2001	0.001	0.000	0.000	350.0	800.0	1 4 00 • 0	3300.0	1800.0	2000	2000-0	2400-0	160.0	700-0	2000	0.004	3000+0	3000-0	3000.0	70.0	120.0	3000-0	0.00	1.0	3000.0
WEIGHT	0.0	0.0	••	•	9	0	0.0	0.0	0.0	•	0			0.00000	00000	00000	00000	000000	0.0000	0.0001	3100.0 1000.0	1000	1000.0	1000.0	1000.0	1000	10001	0001	100001	100001	100001	100001	10000-0	10000	10000	16000.0	100001	10000.0	10000	100001	10000	1 0000-0	10000.0
INI TIAL VEECO	64.0.0	440.0	3000.0	3000	0,046	3000	3000.0	3000.0	8.0	3000.0	900	3000.0	3000.0	3000-01	3000.010	3000, 01	2000-01	3000.01	10.026	3000.0	3000	3000	3000.0	3000.0	3000.0	3000.0	3000		3000	3000.0	30000	3000.0	3000	2000	3 000 6	3000.0	3000.0	280.0	3000.0	3000.0	3000	2.0	3000.0
UN 11	ř	25	£ :	4 4	2 4	, r	28	23	9	1 9 \$	7 6	3 3	9	99	67	63	69	۶;	;	21	5 2	<u> </u>	2	11	78	42	8 :	- C	8 6	98	82	86	87	÷ 6	8	16	25	66	46	%	£ 6	86	6 6 6

15. TO-3 Helium R Values Variable Condition (Sheet 2 of 2)

16. Glass Standards Helium R Values Variable Condition

4 HOUR	1100.00	3000.	3000.0	190.0	3000	2002	3880 3880 210 100 1500	2200 220 220 1 200 3000	3000	2 4 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
90 PSIG 2 HOURS	1200.0 3000.0 .5.0 100.0	3000.0	3000.0 3000.0 3000.0	200°0 50°0 180°0	200°0 70°0 150°0	100.0 100.0 3000.0	3000.0 3000.0 450.0 3000.0	3000.0 140.0 2000.0 3000.0	300000000000000000000000000000000000000	30000 30000 30000 10000 40000
9 1 HOUR	3000.0 3000.0 75.0 80.0	35.0	1000.0	650.0 700.0 120.0	55.0 320.0 3000.0	45.0 45.0 100.0 3000.0	3000.0 3000.0 150.0 3000.0	3000E 0.000E 0.000E	3000.0	30000 30000 10000 15000 15000 4550 4650 4650
4 HOURS	15000	3000.0	0.000	300.0 45.0 55.0	70.0 55.0 140.0 3000.0	160.0 45.0 100.0	3000.0 3000.0 150.0 3000.0	3000.0 3000.0 3000.0 3000.0	19000 19000 30000 30000	3000.0 1800.0 160.0 160.0 100.0 140.0 35.0
75 PSIG 2 HOURS	31.0	3000.0	100.0 100.0 35.0 75.0	180.0 65.0 19.0	55.0 350.0 100.0 3000.0	55.0 82.0 31.0	3000.0 3000.0 48.0 120.0	3000.0 3000.0 3000.0 50.0	3000°0 1000°0 3000°0	3000.0 3000.0 45.0 1000.0 75.0 100.0 52.0
7 1 HUUR	38.0 2900.0 30.0 18.0	1800.0	27.0 100.0 75.0 30.0	35.0 20.0 40.0	23.0 40.0 72.0 3000.0	90.0 38.0 85.0	3000.0 3000.0 120.0	3000.0	00000000000000000000000000000000000000	2200 0000 0000 0000 0000 0000 0000 000
4 HOURS	3000.0	3000.0	20000	3000.0 32.0 30.0 80.0	3000.0	3000.0	3000.0 3000.0 3000.0	300000000000000000000000000000000000000	3000-0	0000 00000 00000 00000 0000 0000 0000 0000
PSIG 2 HOURS	55.0 3000.0 3000.0 8.0	3000.0	3000.0	300.0 50.0 50.0	3000.0 3000.0 130.0	1400.0 1400.0 70.0 3300.0	3000.0 3000.0 120.0	3000.0	3000.0 120.0 60.0 3000.0	150.0 3000.0 150.0 1000.0 130.0 130.0 1000.0
60 1 HOUR	1500.0 75.0 3000.0	3000.0	48.0 650.0 3000.0 100.0	78.0 78.0 40.0 65.0	3000.0 3000.0 80.0	85.0 1200.0 25.0 3000.0	3000.0 3000.0 3000.0 75.0	300000000000000000000000000000000000000	3000°0 300°0 300°0	3000.0 3000.0 85.0 100.0 50.0 140.0 300.0
6 HOURS	28.0 20.0 3000.0 30.0	3000.0	300000	20°0 16°0 32°0	3000.0	28.0 3000.0 16.0 3000.0	3000.0 3000.0 3000.0 3000.0	3000.0	3000.0 3000.0 16.0 560.0	3000. 3000. 50.0 50.0 50.0 24.0 40.0
PSIG 3 HOURS	30°0 30°0 40°0 32°0	3000.0	1600.00	250.0	3000.0	60.0 1500.0 55.0	3000.0 3000.0 3000.0 150.0	300000	3000.0 3000.0 55.0 3000.0	3000.0 3000.0 1000.0 200.0 52.0 120.0 150.0
45 1 HOUR	3000.0 3000.0 26.0 38.0	3000.0	23000 23000 23000 2000 2000 2000 2000 2	33.0 25.0 25.0 25.0	80.0 1400.0 130.0	200°0 70°0 30°0	3000.0 3000.0 160.0	2000 2000 2000 2000 2000 2000 2000 200	3000°0 3000°0 83°0 200°0 3000°0	3000.0 210.0 3000.0 85.0 3000.0 57.0 100.0
8 HOURS	30.00 90.00 90.00	3000.0	3000.0	36.00	3000.0 3000.0 100.0	3000.0	30000.0	9000° 0 9000° 0 9000° 0	3000.0 3000.0 76.0 100.0	3000.0 3000.0 70.0 100.0 48.0 60.0
PSIG 4 HOURS	1200.0 78.0 1500.0	3000.0	3000.0 3000.0 32.0	20.0 20.0 16.0	3000-0 3000-0 120-0	22.0 3000.0	300000	3000.0 3000.0 3000.0 3000.0	3000.0 3000.0 50.0 150.0	3000 1500 1500 1500 1500 1500 1500 1500
30 1 HOJR	10001	3000.0	3000.0	10.0	1700.0	20°0 20°0 3000.0	3000.0 3000.0 3000.0	3000°0 3000°0 3000°0 3000°0	3000.0 3000.0 3000.0 3000.0	m m
KE1GHT GAIN							0.00001		0000.0 10000.0 0000.0 10000.0 40.0 10000.0 000.0100000.0	3000.0100000.0 24.0100000.0 300.0100000.0 63.0100000.0 20.0100000.0 20.0100000.0 20.010000.0 20.010000.0
INITIAL VEFCO	10.00 1000.0 3000.0	0.000£	300		7		' '			3000.01 3000.01 60.01 40.01 20.01 20.01 20.01
THON NOW	WE 4	w 3 r ∞	62122	25222	2222	1822	32868	2 M M M M M	85613	744444

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EVALUATION
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	A N ◆	•						•	•	•	•	•	3000.0	٠	٠		٠	٠	•	٠	٠				•	•	٠	٠	•	•	٠	٠	٠	٠	•	•	٠	•		•	٠	٠	7.0	٠	y.	•	2.0	•	٠	0000		0.1
114-117	A CON	•		, ,	•			•	•	٠	٠	٠	٠	٠	٠	٠	•		•	٠	•	•	9.0		•	٠	•	٠	٠	٠	٠	٠	٠	٠	٠	٠	٠	٠	2.0	•	٠	٠		•	٠	٠		•	•	•	2.0	3000.0
8-014 ¥	RQN N	- 7	•		• 7	•		•	•	•	٠	٠	0.6	٠	٠	٠	٠	•			•	4			•	•	•	•	•	•	٠	٠	•	٠	•	٠	٠	•	•	٠	•	٠	٠	•	•	٠	•	•	٠	•		
ALL DA	NON 1	6						•		•	0.2	0.3	3000	••	•		1.0	3000.0	••		۰				• .	•	٠	•		•	•	٠	٠	٠	•	•	•	•	٠	٠	٠	•	•	•	٠	•	2.0	•	•	•	•	
	NON.	-	• ^	1 (٠,	יש	٠,	o r	- :	0	C	67	7	12	13	7	15	70	11	81	19	20	7.5	: :	3 0	S	7 1	Ç,	91	72	28	53	9	31	35	33	34	32	2 1	200	200	, ,	9	.	7,	4	*	٠,	Ç!	* .	9 0	2

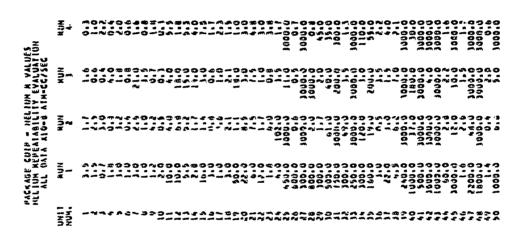
17. TO-84 Helium Repeatability R Values (Sheet 2 of 2)

5	AUN 4	•	•	0.2	٠	•				100.0	•	ċ	3000.0	•	ċ	•	٠	•	•	٠	٠	•	٠	٠	٠	•	•	٠	•	٠	- 6	•				•	•		٠	•	٠	٠	•	8.0	٠	•		٠
T EVALUAT	RUN	0.1	0.0	0.1		•	۰				•	•	3000.0	•	•	•		•	•	•	٠	•	•	٠	•	•	•	•	•	•	•	•	•	, ,		•	•	-	•	•	•	•	•	•	•	•		•
EAIABILII A X10-8 A	นถุก ร		•	7.0	•	•				•		ċ	3000.0	•	ċ	٠	٠	٠	•	•	٠	٠	٠	•	٠	٠	٠	٠	٠	٠		•				•	•		•	٠	٠	٠	•	0.1	٠	•		•
ELIUM KEP ALL DAT	รูก เ		0,1		7.0					100.0		်	•	•	ċ	٠	٠	٠	٠	٠	٠	٠	٠	٠	٠	•	٠	•	٠	•	::	•				•	•		•	•	٠	0.7	٠	٠	ο ·	•	9 6	•
Ĩ	NON.	15	52	53	54	55	26	5.5	85	20	09	.;	62	63	99	65	99	67	68	69	20	7	72	73	4.	۲;	2;	2 i	9	2 6	2 ~		4 6	9 6	85	98	87	88	83	90	16	95		96		3,5	× 8	?

18. C-PAK Helium Repeatability R Values (Sheet 1 of 2)

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S 2	0.3	٠	ċ	•	٠	ċ	•	٠	•	٠		-	٠	•		9	•	٠	•	•	•		1.0		•	٠	•	- 8	•	3	000	000	00	٠	••	ં	8	3000	•	•	;	000	•	•	200	0.000	9	
NO.	3000.0	ċ	000	000	000	8	ġ	000	0.3	2002	000	000	•		•	5	3	٠	8				ဆီ	50.	000	000	8		3	ġ	160	9	8	-	3000.0	000	•	9	•	3	•		•	9	•	٥ (000	
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CKAGE MOS EL IUM REP ALL DAT	RUN		200.0 200.0 200.0 200.0 200.0 200.0
PAG	UNIT NUN.	221103826554010382654821038210382104482104446664666466666666666666666666666666	144444 1440-800

LUES TION	RUN,	•	0.3	•	N	ं	3000.0	• 5	30000	1.0	0.5	*	٠			•	•	•	•	• •	8	000	80	3000.0			ċ	•		000	000	000	200	•	000	000	000	000	•	٠	- α - α	9.0	0.8	5.6
LIUM R VAL TY EVALUAT ATM-CC/SEC	NO.	m	0.0	•	; •	=	•	٥	0.00	0.0	9.0		•			•	•	0.0		3000.0	:	000	000	3000.0		000	ċ	•	4.5	000	00	000	240	3000	000	000	000	000	٠	•	9 0	2.5	0.5	•
SD1P - HEL PEATABILIT TA X10-8 /	KUN.	~	1.0	•	3	ò	•	٥	3000		٠		•			•	٠	•	•	3000	-	900	000	3000		000	0.2	•	,	000		000	210	2000	000	000	000	000	٠	•	3 r		2.0	1.4
CKAGE MO ELIUM RE ALL DA	S.	_	0.2	0 9	Ö	٠.	000	2	3000			ં		• •		9.0	•	•		700.0	44	8	000	88		9	ö	~ 0	2 4	000	0	200	000	2000.0	000	600	800	200	m .	•	* 6	1.66	4.0	•
Q I	1140	YOU CH	15	2 7	2,7	55	ŝ	7 5	200	9	61	79	2 3	5 41 5 41	99	67	68	3 6	2 2	72	2	14	15	:2 1	8	2 2	80	3	2 6	8 6	85	86	84	D 7	9	76	05	93	4 0	6 6	8 5	.86	66	

21. TO-100 Helium Repeatability R Values (Sheet 1 of 2)

UES 10N	N.4	•	•	• •		•	•	٠	٠	•	•		, ,	•	•	•	•	•	•	•					٠	٠	•	•				•			• •	-		ċ	9	ō.	•		1.3	•	4
IUM R VAL	RUN	0.5		• •		•	•	٠	٠	٠	•					•				•		•					•	٠.				٠	•	•	: 6	ó		÷	18.	ं	3		2.2	٠	7
100 - HEL EATABIL!! A X10-8	RUN 2	•	٠	• •		•	٠	•	٠	٠	•				•	ċ	ံ	٠	•	•			• •			٠	•	•	90			٠	٠		• 7	-	•	•	0	•	- 5		1:3	٠,	7
ACKAGE TO ELIUM REP ALL DAT	AUN 1	•	9:0	• •		•	٠	•	•	٠	•					•	٠	•	•	•		•	;				٠	• ;	79.0			•	•	•		-	6.1	~	17.	3	•	0.000	2.3	1.4	•
άI	UNIT NOW	-	~ ~	7 4	ۍ -	9	٧	60		o:	Ξ:	71	7	15	91	17	18	19	50	22	7.6	576	52	56	27	28	29	2 .	.	33	34	32	36	- 0	9 5	0,4	17	45	43	4.4	42	70	4.	65	

21. TO-100 Helium Repeatability R Values (Sheet 2 of 2)

2	2	,	23.0	-:	4	ċ	•	ċ	ē	٠.	1.2	•	1	•		22.	ģ	270.	•	000	14.0		8	8	ġ	٥	190.0		3000.0	~ :	•		80	å	25		3000		000	8	000	ċ		3000
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ALL DAT	٠.	•	•	٠	•	3	\sim	ċ	=	•	8.0	:	0.11			27.	45.	000	3000.0	200	•	i	8	ā	900	÷	0.000	3	•		• -	d	110	9	30.			000	000	000	000		200	3000.0
٠ ,		•	25	52	53	ž	55	96	57	28	50	3:	70	63	49	65	99	19	89	7 0	2 =	12	7.3	7.4	15	92	<u>.</u> 82	262	80	81	7 6	7 6	85	98	87	D 0	A C	6	92	66	76	32	96	÷ 86

ACKAGE CERM - HELIUM R VALUES HELIUM REPEATABILITY EVALUATION ALL DATA XIO-8 ATM-CC/SEC

RUN 4	30000000000000000000000000000000000000	, , , ,
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r L	77.0 24.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0	
UNIT NUM.		\$ 0

22. Ceramic Helium Repeatability R Values (Sheet 1 of 2)

22. Ceramic Helium Repeatability R Values (Sheet 2 of 2)

ues 110N C	RUN 4	3000.0 3000.0 3000.0 3000.0 3000.0 3000.0 400.0 400.0 118.0 118.0 118.0	
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ACKAGE TO 3 - HELIUM R VALUES IELIUM REPEATABILITY EVALUATION ALL DAIA X10-8 ATM-CC/SEC

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23. TO-3 Heijum Repeatability R Values (Sheet 2 of 2)

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LASS - HEI PEATABILI TA X10-8	KUN 2	110000 110000 12450 12450 12450 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 12600 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126000 126
ACKAGE G ELIUM RE ALL DA	RUN 1	1
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25. TO-84 Radiflo Q Values Variable Conditions (Sheet 1 of 2)

PACKAGE TOB4 - RADIFI,O O VALUES RADIFIC VARLARIE CCADITICN EVALUATION ALL CATA XIO-8 ATH-CC/SCC

RH3 3-WASH	36.0	2.2	9.	, (9	9.6	5.2	9	m	93.0	19.0	0.5	٠.	٧ ;	2000	3 5	0.00			2	340.0	0	170.0	29.0	0.0	220.0	180.0	2.0.0	0.00	0.0	530.0	310.0	0.094	75.0	84.0	0.0	•	٠	0 0		9 6	•	•	•	•	·
IV SYSTEM RH2 1-WASH	12.0	2.6		7.0	:	9.7	0.0	7.8	12.0	140.0	19.0	1.7	6. 4	7.5	200	0.00	200	- 6	20.0	0.064	340.0	0.0	380.0	33.0	0.8	210.0	0.009	430.0	0.061	0.00	500.0	22.0	460.0	77.0	84.0	0 0	» «	0.0	0 0	•	600	•	» c	•		90
MARK RH1 O-WASH	130.0		0.	•	2		5.2	8.7	•	220.0	\sim	~-	0.1	- (2000	200	150.0		0.000	2002	270.0	0	310.0	35.0	1.7	240.0	1100.0	550.0	330.0	25000	580.0	2	450.0	29.0	6.9	000	9 0	0.0	œ 6	0	0.0	200	2 0	200	9	0
RD3 3-WASH	150.0	3.0	6.3		•	• 6		2.9	10.0	160.0	•	•	m,		•	•	2.0		2 0			0.0	270.0	31.0	0.0	150.0	360.0	450.0	0.004	0.001	340.0	2.5	160.0	5•3	0.9	0.0	• • •	0.0	0.0	0.0	٥. د د	•	9.0			0
RD2 I-WASH	140.0	3•3	6.9	0,0	9 9) r		2.0	10.0	216.0	1.8	0.0	4.5	0.0	0.024	200	0,1		0.00	250.0	250.0	0.0	270.0	30.0	0.0	250°C	320.0	400.0	450.0	0.0	250.0	37.0	0.0	58 • 0	0.0	0.0	0,0	0.0	0.0	0.0	<u>د</u> د	200	0.0	0.0	•	20
2451C SYSTEH RD1 O-WASH	0.00	3.0	4.		•	0.0	10.0	6.7	10.0	230.0	18.0	1.3	8 9	1.4	310.0	2.6	0.00	13.0	2000	0.00	250.0	3.0	380.0	30.0	1.2	67.0	320.0	380.0	150.0	* 0	140.0	13.0	3.5	58.0	67.0	0.0	•		٠	0	•	•	•	5.0	9.0	1.2
ROI O-WASH	250.0	4.6	16.0	0.01	2:	200	12.0	14.0	27.0	410.0	40.0	0.0	7.5	2.8	620.0	0.012	0.061	200	280.0	0.00	20.70	0.0	790.0	67.0	0.0	250.0	540.0	840.0	920.0	2	0,040	350.0	750.0	150.0	240.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	o (0.0	0.0	ċ
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PACKAGE T084 - RADIFLO Q VALUES RADIFLC VARIABLE CCNDITION EVALUATION ALL DATA XIO-8 ATM-CC/SEC

		3-WASH	0.0	0.0	0.0	0.0	0.41		0,0	0.0	350.0	170.0	0.4	0.004	•	7.0	•	-		•) ·			0.0	0.0	0.0	0.0	0.5	0.0	0.0	0.0		200	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		••
	IV SYSTEM	I-WASH	0.0	0.0	0.0		0.041	0.0	0.0		340.0	0.061	0.041	220.0	• • •	0.22	200	2 4		•	; ;	: (90	 0.0	0.5	0.0	0.0	0.0	0.0	0.0	0,			0.0	0.0	0.0	0.0	8.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	•
	MARK	O-WASH	0.0	0.0	0.0	0.0	150.0	0	0.	3.5	270.0	160.0	120.0	24.0	•	2.0	9	•	•		•	•	9 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,1	0.0		8.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	æ •	0.0	0.0	•
AIM-CC/SEC	4	RD3 3-WASH	0.0	0.0	0.0	0.0	1.0.0	0.0	0.0	0.0	260.0	63.0	150.0	0.74		200	•	•	, ,	•	•	•	•	0	0.0	0.0	0.0	0.0	0.0	0.0	o •	0 0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.	9.0	•
L DATA X10-8		KDZ I-WASH	0.0	0.0	0.0	0.0	70.0	0	0	0.0	23.0	34.0	160.0	28.0	•	0,0	•	•		٠,٠	• •	, ,	200	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	•
ALL	24510 SYSTEM	HSMM-0	0.0	0.0	0.0	0.0	34.0	0	0.0	0.0	0	15.0	160.0	28.0	•	7		·, -	•		7•1	•	2 -	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0	-	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0	5	0.0	0.0	~, c	••
		NUI O-WASH	0.0	0.0	0.0	0.0	200.0	0.0	0.0	0.0	280.0	380.0	513.5	200	0.0	0.0	•	•	•	•	9			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.01		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.0	•••
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	RUI O-WASH	140.0	ė	220.0	33.0	95.0	0.1.0	25.0	=	2000	:		200		Š	0.0		93.0	70.0	0.0	\$6.0	30.0	0.46		200	200	20.0	40.0	100.0	0.00		24.0	12.0	300	è		130.0	5	20.0	0.00		9	2.0	25.0	00.
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PACKAGE RADIFIC V	2451C SYSTEP HD1 O-WASH	0369093900404003-64400000000000000000000000000
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27. C-DIP Radiflo Q Values Variable Conditions (Sheet 2 of 2)

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28. MOS DIP Radiflo Q Values Variable Conditions (Sheet 1 of 2)

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	IV SYSTEM	I-WASH	0.0	0,0	•	•	0	0.0		0.0	9	2-	.0	×.	~	m.,	7.	0.5	2	2		.0		9.		r.	∴ .	-	200	2,5	1.2	140.0	o-	7.7	0.84	3.3	1.4	0.00	*;	9			0.004	73.0	73.0	0.091
U	HARK	0-WASH	1.0	0.0	9.0	2	.~	0.0	0.		× •	3.0	0	9.0	~		•		•		, e		0.0	0.5	0.0	4.0	n c	2 •			0	62.0	0.0	- e	9	8.0	0.5	16.0	s.	0 •	2	2	0.09	0.5	£.5	20.0
-8 ATM-CC/SE		3-KASH	0.0	0,0	9 6	2 -	0	0.0	0.0	0,0	50	9 6		4.9	3.2	0	• ·	- 0	5	9	2		0	2.0	0.0	 	0.0	9,	200	, –	0.0	16.0	0	2.5	37.0		4.2	0.0			24.0		90	1.6	20.05	100.0
ALL DATA X10-8		1-WASH	0.0	0	9.5	2	0	2,0	ó.	o,	9:	20.4	,	4.4		35,0	o,	٥.	•	•	-		9.0	2.0	0.0	7.7	9.	0,0	0.00		. 7	16.0	o .	200	37.0	7.7	4.7	5.9	F. 6	30	25.0		2 -	0	20.0	160.0
•	24524 SYSTEM	O-WASH	0.0	0,0	0.0	1100.0		9.0	0.0	æ (0.	1.4		2.5		1.2	٠. -	3 6				, lu			1.5	5.0		5.0	130.0		. 2.0	6-3	o.		30.05	3.0	12.0	0.0	9.0		200) ~	0	19.0	152.0
	-	O-WASH	0.0	0,0	90	•	0	0.0	0.0	0	0.	0 C	5,5	0	1.6	0.0	F.	٠. ت	•	* 0	2 4	, ,	~	9.	1.6	2.0	0	3.	250.0	2.4	0	15.0	0.0	2 5	200	3.1	0.9	0.0	3.4	12.0	20.00		•	0	20.0	1,60.0
		NOW.	_	~	m <	f ur	ے ،	~	æ ·	σ :	≘:	::	:::	3	~	2!	_	æ	2 5	3.5	, ,		5.5	2	92	2.2	స్ట	5,	0.	, C	33,	34	£.	9 5	- e	9	ŝ	7	3	7	3 4	Ç 4	,	.	ş	Ş

28. MOS DIP Radiflo Q Values Variable Conditions (Sheet 2 of 2)

	5	3-WASH	0.0	0.8	3.00	0-	.0.18	0	30.0	0.0	900	2.4	0.17	0.0	0	0	•			9.0	1200.0	٥:	25	35	280.0	8	ဇ္ဇ	0.0	200	0	380.0	2.0	25	0.00	គ	860.0	0°0	0	96		•	0.0	0,	00
	IV SYSTEM	1-WASH	0.0	0.0	260.0		0.034	0	260.0	0.0	300	9	360.0	1.3	0	•	9 0	50	200	0	1000.0	0.0	000	0.004	300.0	910.0	0.099	0		0	0.000	20.0	230.0	710.0	4.80.0	710.0	300.0	000	000	0	0.0	0.0	•	
VALUES EVALUAT 10N SEC	PARK	O-WASH	•	ċ	•			ċ	•	ė,	•				•	•		•	- 4			•.	٠.	: :		:	•	•			ė	å,	•	9	31.	ċ	33	5.	•			•	•	•••
- RADIFLO 9 V CCHOITICK EVA 0-8 ATM-CC/SE		3-WASH	0.0	0.0	0.24	0 0	340.0	0.0	250.0	0.0	220.0		0	0.0	0	0	0,0	0 0	•	0	1100.0	0.0	0.0	000		300.0	920.0	0.0	9 6	0	840.0	220.0	340.0	250.0	840.0	100.0	2.004	0000			1.6	0.0	0	00
CSDIP LIABLE (600	1-HASH	4.7	0	34.0	900	320.0		250.0	0	210.0		•	0.0	0.0	•	0.	•	20	9.9	82.0	0	0.0021	200	?~	230.0	ខ	D (8	8	40000	20	3	8	ខ្ល	2 8	3.		0	9:	0.0	.0.
PACKAGE A	24510 SYSTEM	3 3					•														4			3.	•		<u>ــ</u>				•			800.0	0,040	700.0	570.0	0.00	200	- ^ -		0.	0.0	1.1
يت ريونو کاليون	وم	0-wt SH	e S	ů	0 0	90	294.0	, o	0-152	0	26.0	, (2) (2)	0.0	9 92	0.0	200	000	- C	774		0.00	0	0.00		0	3220.0	930.0	0	. O	10.0	95.0	20000	1600.0	, -	·w	•	~	0.0001	200		0.0	0.1	0.0	00
	T T T	NO.	5.1	25	m,	, r	30	57	28	26	9:	3 %	63	40	9	9 !	6	9 9	200	7	72	5	2 ;	2 2	2.	7.8	6	080	2 0	83	94	85	9 6				5	25	n .	5	96	6	9	200

The wind the state of the second state of the

29. TO-100 Radiflo Q Values Variable Conditions (Sheet 1 of 2)

	PH3 3-WASH		0		•					200		2.8	10.0	2.5	0.0	•	•		0.0	•) M	0.0	0	0	0.0	2.0	0.9	0 0	90	200	39.0	26.0	:) ·	8	0.0	40.0	22.0	0.1	F. 6	3		0.5	200		23.0	25.0
	IV SYSTEM RH2 1-WASH		0.0	•								7.5	9.5	•	0.0	0.0	0		0.00	•) r		2.5	0	4.7	0.0	0	0.0		200	55.0	32.0		•	0.01	6.0	53.0	23.0	0.4	0.0	3.5	200	0.80	200	٠.	23.0	28.0
JES JAT 10N	HARK RH1 O-WASH	,	0.0	•			•					0	9.4	1.4	0	o.	.	ė	0.0	•••	4.	***	0	6.	4.5	7.7	91	۴.	• • •	0	37.0	ė,	, c	•	. 60	6.0	26.0	÷	13.0	•	š.	Ž.	٠,	i	2	;	÷
- RADIFLO O VALUES CONDITION EVALUATI	RD3 3-WASH		0.0	5.0	,	,	•	9	•		200	0	6.3	0.0	0.0	0	0.0	٥	0.07	7,0			0.0	200	•	0.01		0.61	- 0	200		30.0	06	200	15.0	_	S.	16.0	•	2.6	∾.	о 1		7	25	, –	27.0
T0100 -	RD2 1-WASH		9.0	•	0.0) ·			, 0	0	4.7	0.0	0.0	0.0	0	۰,	0.046	9,0	70.0	•	0	0.0	5.0	2.0	0	12.0	Э(200	-	22.0	۰.9	9,0		9.	33.0	0		s.	о.	∞ •	01	õ	7 C	3	16.0
PACKAGE RADIFLO V	24510 SYSTEM R01 0-WASH		•			•			•	• •				•	•	•	•		•	•					•		÷,	•	٠,		; ;	•	å,	•	7.		•	÷	•	•	ċ	ě.	ġ.	•	5	: :	13.0
	RDI C~WASH			- ·			•	•	•	7.0		2.0	6.	8.0			5°0		113.0	~.					14.0	31.0	6.2	e	27.0	24.0	0.44	45.0	20.0	0	2.0	6.9	45.0	45.0	14.0	12.0	o.	31.0		104.0	200	0.00	0.69
	UNIT NUM.		, مــ	N (m -		۰,	۰.	. •	E 0	۶ ۲	:=	12	13	<u>*</u>	15	ş	11	æ :	<u>-</u>	85	;;	; ;	2	52	2	27	88	5 6	2 5	35	33	4	2	0 6	88	36	ç	7	<u>۲</u>	43	;		ç:	-	. 0	, ç

THE RESIDENCE OF THE PROPERTY
29. TO-100 Radiflo Q Values Variable Conditions (Sheet 2 of 2)

		3-KASH							0.04		0.0	0.0	ė	3000	0	100	0.06	31.0	300	2000	0.00	35.0	0.06	130.0	0.00	0.001	1 70.0	150.0	210.0	220.0	18.0	000	20.0	1,40.0	630.0	73.0	800.0		0.00	620.0	700.0	0.016	670.0	2001
	2	L-WASH	130.0	23.0	2000	0,50	65.0	ġ	00.0	200	ċ	0.0	2	0.000		50	120.0	38.	င္ဆဲ	220.0	٤		8	140.0	င္က်င္	כל	270.0	ģ	270.0	2	5.	210-0		8	ė	9	ខ្លុំខ្ល	38		30.	ė	ė	S S	ġ
G VALUES EVALUATION C/S EC	MARK	HSM-0	0.96	57.0	0.0	7.0	57.0	0.96	130.0	1000.0	0.0	0.0	8,0	0.000		72.0	0.066	38.0	170.0	2000	0.066	37.6	72.0	120.0	282.0	30.0	150.0	170.0	0.061	220.0	0.0	000	150.0	150.0	340.0	67.0	410.0		0.00	530.0	570.0	630.0	390.0	2000
CONDITION EVAL		3-445H	100.0	73.0	0.04	0.00	70.0	97.0	130.0	3000	0.0	0.0	20.0	17.0	0	0.62	100.0	20.05	320.0	0.00	250.0	0.29	83.0	130.0	0.044	0.04	160.0	160.0	0.00	210.0	0.0	20.0	40.0	130.0	110.0	83.0	0.000	0.001	0.00	6,00.0				ο .
GE TO100 - Variable Ll data X1	ć	1-KASH	83.0	20.0	25.0	0.85	50.0	30.0	130.0	3000	0	0	ខ្ល	2000	0,0	67.0	84.0	2	ဗ	180.0	35	3	2	8	S	?	22	2	260.0	25	0.0	130.0	120.0	130.0	110.0	67.0	10001	0 0 0 0 0 0	140.0	6.70.0	700.0	0.56	180.0	•
PACKAGI RADIFLO	24510 SYSTEM	O-WASH	74.0	20.0	27.0	002.7	47.0	74.0	0.76	3000.0	0.0	٠. د د د	28.0	0.000	, 0	0.04	81.0	34.0	340.0	0.01	270.0	0.24	78.0	97.0	0.044	0.00	110.0	110.0	0.051	160.0	0:0	120.0	120.0	110.0	10001	0.09	0.000	0.00	1300.0	670.0	0.069	780.0	470.0	2.010
		D-WASH	71.0			0.45			0.961		-			20.00		143.0	126.7	104.0	394.0	124.0	335.0	124.0	143.0	133.0	355.0	104.0	247.0	148.0	143.0	148.0	147.0	148.0	133.0	169.0	340.0	111.0	3000.0	0.000	0.0005	C. COOF	3000.0		•	2000
	•	NOW.	51	25	r 4	55	26	57	£ 5	7 0	; , ,	65	63	, v																												8	6 5	2

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ACKAGE CERM - RADIFLU Q VALUES IDIFLU VARIABLE CONDITIUN EVALUATION ALL DATA X10-8 ATM-CC/SEC

RH3 3-MASH	2.0	2.5	•					•	•	•	•				2	7		;"			2.5	2.5	_	0.01	1300.0	1300-0	4	200	0.5		0.0011	15.0	150.0	9.5	4.2	9.2	5.5	5.5		٠		25.0	7.7	3 4		8,7			
IV SYSTEM RHZ 1-WASH	•	2.5	4.2	2.0	٠. د. د.	•	0 1	٠	~•9	•		2.4	•	20.0	2					ή,		2.5	200	20.02	3000.0	3000.0	5.8	15.0	0.0001		0.60	0.000	17.0	0.4	6.1	21.0	5°.8	8,4	8.	18.0	3000.0	16.0			• •	- 0	*	2:	
MARK RH1 O-WASH	2.1	. 6	0.7	8.0	•	0.0	B • 0	0.5	0.1	8.1	1.2	0.5	9.0	8.0	9.0	-:	0.5	3000.0	6.0	8.0	7.2	0.11	7.1	2000	0.0004	3000.0	2.1	2.0	8.0	6.0		3000.0		7.0	8	3.1		6.0	٥.7	7.6	3000.0	5. 8	•			σ·	2.0	7.7	
RD3 3-WASH		•			0.0	0	0	0.0	0.0	0.0	0.0	0.0	0	0	0.0	0.0	0.0	830.0	0.0	0.0	1.6	0.0	0	240.0	•	2000.		1.3	0.099	0.0	3.8	1300.0	9:	0.0	,				0.0	0.0	89.0	0.0	0.0	0.0	0.0	•	0.0	0.0	
R02 1-WASH	•	- 0	3	•	•	0.0	• •			0.0								0.0001		0.0	3.0	0.0	0.0	380.0	2.4	230.0	3000	, v	0.004	0.0	5.4	3000.0	1.6	0.001	2.0		7.0	•		•	200	200	0	0.0	0.0	0.0	0.0	2.0	
24510 SYSTEM RD1 0-MASH	,	2.8	0.1	2 0	•	200	30	•	•	, u		» «	•	2,0	200	•			9 0	•	9 6		0,0	0.0	6.3	9.1		33.0		200	2	0	3.0	300.0	2.0	0.0	* -1	e	0.0	0	0.45	• • • • • • • • • • • • • • • • • • •	9	•		•	•	•	•
2 108 108	E .	3,3	0.0	0.0	e .	0	0.0	0	0	0.0	 0	0.0	0	0	0:1	0.0	0.0	- 1	1300.0	200	o •	•	? ~	340.0	8.5	1200-0	3000.0	0.0	5.5	150.0	0.0	2000	3.6	77.0	4.1	0.0	5.0	0.0	o.°0	0.0	5.9	210.0	0.0	0	0 :	9	٠ • •		•
TINO		_	~	٣	4	ç	٥	~	80	σ	2	=	12	13	2	15	91	11	2	6	50	7	7;	3 8	, ,	2 2	27	28	53	30	<u></u>	e .	3	* u	, «	37	96	33	0,	7	45	43	4	45	40	7.	49	49	2

30. Ceramic Radiflo Q Values Variable Conditions (Sheet 1 of 2)

30. Ceramic Radiflo Q Values Variable Conditions (Sheet 2 of 2)

	SYSTEM RH2 RH3 -MASH 3-MAS		-															
	ARK IV																	
ALUES EVALUATION /SEC	RH1 0-MASH																	
RADIFLO Q VALUES E CONDITION EVALU X10-8 ATM-CC/SEC	RD3 3-WASH	000	000	1.3	000	0.0	0.0	0	0	7:1	0.0	0.0	0.0	0.0	0.0	••	0.0	0.0
PACKAGE CERM — 1 Radiflo variable All data X	R02 1-WASH			~														
PACK, KADI FI	24510 SYSTEM RD1 n-wash	260.0	000	0.0	38.0		1.2	5.5	9.0	2.0	1.2	1.6	0.0	0.0	0.0	0.0	0.0	0.0
	RDI O-WASH	2.5	000	390.0	0 0	0	0.0	2.1	000	1.6	0.0	٥. د	0.0	0.0	0.0	0.0	0.0	0.0
	UNI T	52	23	25	56	8	29	9	19	63	40	9	99	29	68	69	2	z

31. TO-3 Radiflo Q Values Variable Conditions (Sheet 1 of 2)

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	RH3 3-4ASH	48.0	1.3	~:	0.0	3000.0	2.2	4.7	3000.0	٠٠,	6.6		0	1.7	0.0	5.8	1:3	0.0	0		7.7		200	0.0	1.7	220.0		220.0	73.0	110.0	35.0	0.41	2000	0.0	250.0	3000.0	30.0	800.0	100.0	0.000	2000	0.0	480.0	31.0	3000.0	22.0
	IV SYSTEM RHZ I-WASH			3.5	23.			۲.	3000-0	ġ,	3	> <		0.0	0.0	0.0	0.0	0.0	0.0	•				0.0	0.0	220.0	7 4 6 7	230.0	90.06	100.0	57 ·C	12.0	0.00	0.04	220.0	3000.0	32.0	2002	180.0	200	000	4	680.0	35.0	3000.0	27.0
VALUES V EVALUATION CC/SEC	MARK RHI O-WASH	5.0	9.1	2.0	÷	3000.0	0.3	_:	3000.0	٠	•	-	8.0	2.9	1.3	11.0	1.2	0.0	~ 0	ກຸດ	0 0	0.0	0.0	0.9	ď.	31.0	•	27.0		13.0	3.8	≟,	24.0	٠.	:	190.0	'n	٠,	2.0		,		22.0	;	•	6.3
- RADIFLO O VALUI LE COND. TION EVAI X10-9 ATH-CC/SE	RD 1 3-WASH	35.0	0.0	ن 0	0.0	500.0	0.5		3000.0	0.0	,	000	0.0	0.0	0.0	0.0	0.0	c.	0.0	•			0	0.0	0.0	89.0	, c	78.0	35.0	45.0	20.0	0.00	230.0	35.0	100.0	200.0	23.0	240.0	2,00	0.000	,	37.0	160.0	22.0	0.016	18.0
TO 3	R02 1-MASH	18.0		0.0		130.0	6.1	ġ	3000,0	0.0		200	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0	1.1	0.0	0.04	0.22	0.14	85.0	13.0	22.0	, c	٠.	34.0	.:	11.0	ໍ່	'n,	٠,	÷۰	,	36.0	57.0	20.0	260.0	9•3
PACKAGE RADIFLO'V	24510 SYSTEM RD1 0-WASH	٠	0.0	9•I	o;	٠	•	9	3000.0	٠	•	9		•	٥.0		٠	٠	•			0	0.0	•	•	•	0 7 7 6				23.0	::	•	32.		-	50		0.00		8		Ġ	٠	480.0	15.0
	RDI 0-WASH	۲.0	0.0	0.0	-;	78.0	2.8	ж •	4.6	0,0) ·	0.0	0.0	0.0	0.0	0.0	0.0	0.0	• •	•		0	0	0.0	0.0	25.0	200	36.0	14.0	110.0	20.0	•	0.70	30.0	55.0	76.0	16.0	20.0	20.0	0.000	16.0	32.0	3000.0	150.	200.0	48.0
	UNIT NUM.	-	~	m ·	.	v.	91	-	æ (- :	2 :	: 2	2	<u>*</u>	15	91	_	8	<u>.</u>	3 7		23	54	52	92	27	9 0	30	. E	35	33	* *	5 6	2 6	38	33	0,	Ţ:	7 7	77	54	46	4.1	48	64	Š

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31. TO-3 Radiflo Q Values Variable Conditions (Sheet 2 of 2)

	;	3-WASH	130.0	460.0	700.0	3000	3000	870.0	200	3000	1000	S. 2	3.0	7.5	M.		0000	3000	3000	3000.0	3000.0	170.0	3000	0000	0,049	3000.0	630.0	3000.0	3000.0	3000	3000	3000	1000.0	3000	3000	3000.0	000		000	•		•	3000.0	45.0	3000.0	3000*0
	IV SYSTEM	L-VASH	150.0	430.0	830.0	3200-0	1000	÷.	: .	: :	• •		;	٠	ė.								3000		7007		580.	å.	•	å,	3000.0	:	å		3000				å		3000-0		3000.0	=	3000.0	•
IES LLUATION C	HARK	AHI O-WASH	17.0	0.019	110.0	220.0	3000	130.0	0.55	0.00	30000	1.3	3.4	2.5		C 0002	0.000	3000	3000	3000.0	3000.0	97.0	3000	0000	74.0	3000*0	6.009	3000.0	3000.0	3000.0	3000.0	3000.0	17.0	3000.0	3000.0	3000	3000	3000-0	3000	0.041	0.000		3000.0	3.2	3000.0	30000
RADIFLO Q VALUES E CONDITION EVALUATION XIO-8 ATM-CC/SEC	;	703 3-¥ASH	95.0	200.0	310.0	430.0	0.087	280.0	210.0	0.0001	430.0	2.0	9.0	21.0	0,0	٤			000	000	000	230.	3000.0	0.000	2002	1400.0	300.	000	000	000	3000-0	130	65	1200.0	200	330	9	3000.0	000	250.0	0.000	90	1100:0	-	3000.0	
PACKAGE TO 3 - RJ ADIFLO VARIABLE C ALL DÄTA XIC		RDZ 1-WASH	95.0	110.0	95.0	130.0	0.062	0.011	2000	0000	310.0	0.0	4.2	0.0	F	7.7	0.000	3000	3000	3000.0	3000.0	95.0	920.0	0.000	110.0	730.0	85.0	3000*0	0.006	3000.0	3000.0	1000	68.0	2000	3000	300.0	62.0	់	8		0.0041	0.054	3000.0	÷	3000.0	
PACKA Radifl	24510 SYSTEM	KOI O-WASH	92.0	130.0	200 • 0	230.0	410.0	2002	0.021	130.0	0.004	0.0	ċ	•	•	18			3000	000	000	160	00000	3000	1 50	1000.0	250.	000	000	000	3000-0	100	68.0	330	3000	80	160.0	3000.0	3000.0	160.0	0.000		3000.0	16.	3000.0	3000.0
	į	NDI 0-WASH	100.0	92.0	ŝ	130.0	3	40.0	2 9	2	3000.0	3.0	1.4	2.5	0.0	0000		3000.0	000	000	000	88.0	3000	0000	200	000	000	3000.0	000	000	3000-0	3000.0	120.	3000-0		000	000	900	3000.0	;	3000		3000.0	5	88	3000.0
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32. Glass Standard Radiflo Q Values Variable Conditions

	RH3	3-WASH	40.0	260.0	9	0	2.0	480.0	5.9	11.0	0.6	0	200	23.0	13.0	3.3	3.3	18.0	3000	30005	3000	2	920.0	ċ	3000.0	3000	0.000	16.0	3000	3000 •0	3000	5.000	16.0	8	3000.0	ġ.	7	٠.		. 0	-	15.0	∞ ₁	10.0	i	2.5
	IV SYSTEM	1-HASH	73	•	•			580.0	16.		•	•	200		ď	16.0	٥	٠	3000-0	0.0000	•		ċ		3000.0		16004	: :		3000.0	•	0-11-0	22.0	3000.0			<u>.</u> .			; ;		3	٠	۲۰۶۰	: -	30.0
UES UAT 10N	MARK RH1	O-WASH	2.1	43.0	, o	5	0.0	32.0	1.4	12.0	:	:			0.2	0.0	0.3	1: 8	3000•0	3000.0	3000	0.1		1.3	3000.0	3000	3000	•	3000	3000.0	3000.0	1.1	10.0		•		٠	•	•	• •			•	F	•	
CCNCITION EVALUES CCNCITION EVALUATION 10-8 ATM-CC/SEC	803	3-KASH	250~0	350.0	10.0		0.0	5.00.0	32.0	86.0	4.9	20.0	22.0	2.5	6.4	7.3	0.04	10.0	1500.0	1000-0	0,000	37.0	560.0	4.0	3000-0	3000.0	2000	2000	3000	3000.0	3000.0	19.0	0.04	3000	3000.0	3000.0	÷.	ċ.	32.04	; ;	. ;		٠	14.0	•	25.0
LASS TABLE	802	1-WASH	540.0	9		20.71		630.0	-	19.0	3.1	99.0	47.0	0.2		0.0	14.0	13.0	1400.0	930.0	2000	9000	13.0	3.1	3000•0	3000.0	3000	0.000	3000	3000-0	3000.0	17.0	96699	30000	3000.0	3000-0	m 9	22.0	280.0	200	210.0	15.0	52.0	27.0	24.0	14.0
PACKAGE G Radiflo Var All d	24510 SYSTEM	0-WA3H	30.0	180.0	۴.	0.0) a	360.0	10.01	82.0	10.0	0*6	0.04	0 0	9	5.6	5.6	65.0		1600.0	0000	3	2.4	7.3	4	3000	3000-0	3 5	3000	9.0	3000.0	35.0	760.0	3000.0	3000.0		7.3	ġ	330.0	0	: :	30	N	32.0	N	25.0
		O-WASH	510.0	w	0.4	5	, ,	580.0	, "	86.0	4.8	240-0	0.7	•	• 4	3.5	8.4	5.6	1600.0	3000-0	0.11	20000	0.099	9	8	3000.0	88	₹	3000-0	3000-0	3000.0	4.3	0.00	30000	30000	3000.0	2.6	0.6	2.0	26.41		7.3	5.6	0.01	7.3	12.0
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PACKAGE TOIGO - RADIFLO Q VALUES RADIFLO REPEATABILITY EVALUATION ALL CATA XIO-8 ATM-CC/SEC
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RUN 2			 004044666666
RUN 1			 0040440000000
UNIT NUM.	~~~~~~~	22222222 22222222222222222222222222222	W4444444440 W0-10W4W4F##

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38. Ceramic Radiflo Repeatability Q Values (Sheet 2 of 2)

UES 10N	S 4	#0001000010000000000000000000000000000
FLO Q VAL Y EVALUAT	RUN 3	000000000000000000000000000000000000000
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ACKAGE CE DIFLO REP ALL CAT	RUN	-00000041101100000000000000000000000000
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42. TO-100 Helium R Values Temperature Conditions (Sheet 1 of 2)

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42. TO-100 Helium R Values Temperature Conditions (Sheet 2 of 2)

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Surface Absorbtion Helium Data All Data X 10-8 Atm cc/sec

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Device Type		Time to Read After Conditioning (Minutes)	\fter Condit	ioning (Minu	ıtes)
and Number	I-S	30-35	60-65	90-95	120-125
C-DIP Lids (Sealant)					
	3.0	0.4	0.2	0.05	0
2	2.5	0.3	0.1	0.05	0
m	2.6	0.3	0.1	0.05	0
4	2.0	0.2	0.1	0.05	0
S	6.1	0.2	0.1	0.05	0
Ceramic Lids (Scalant)					
20 A	190.0	120.0	62.0	45.0	25.0
21 A	130.0	38.0	16.0	7.0	3.0
22 A	210.0	89.0	45.0	20.0	10.0
23 D	28.0	3.2	2.0	2.0	1.5
	35.0	6.2	3.5	2.5	1.5
25 D	17.0	4.0	2.7	2.1	0.1
C-DIP Lids					
-	2.8	0.3	0.2	0.05	0
cì	2.0	0.3	0.1	0.05	0
m	8.1	0.3	0.1	0.05	0
4	1.6	0.3	0.1	0.05	0
S		0.3	0.3	0.05	0
Ceramic Lids					
1	8.0	₹.Ci	2.2	S:-	0.8
7	5.0	2.3	2.7	ष्ट. ~	9.0
m	3.2	2.7	2.0	v. (9.0
4	<u></u>	<u>:</u>	<u></u>	1.0	0.5
S	S.5	رع غ.	ci T	<u>प</u> .	0.5
Scalant Strips					
Ω.	30.0	5.0	ć. 0.	5.0	0.1
2 D	18.0	4.5	3.0	1.0	0.5
3 D	17.0	3.5	3.0	0.1	0.5
4 4	50.0	7.0	5.0	2.0	1.2
	65.0	6.0	4.5	2.0	<u></u>
٧9	17.0	3.0	2.5	0'1	9'0

47. Surface Absorbtion Helium

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Surface Absortion Radioisotope Data All Data X10-8 Atm cc/sec

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Device Type		Time to Read After Conditioning (Minutes)	After Condi	tioning (Min	ıtes)
and Number C-DIP Lids (Seaknt)	1.5	30-35	90.09	90.95	120-125
_	7.8	7.0	8.8	5.5	5.1
വ	2.0		9'0	0.3	0.0
m	2.5		2.0	- &:-	9:1
₩	Ξ	0'-	8.0	0.5	0.2
S	O	0	9	0	0
Ceramic Lids (Serlant)					•
20 A	40.0	20.0	0.01	4.0	2.0
21 \	40.0	0.61	9.0	3.0	0.1
22 A	39.0	0'61	0.6	3.0	0:1
23 D	38.0	18,0	9.0	3.0	च <u>्</u>
24 D	40.0	20.0	9.0	(1 (2)	0.1
25 D	41.0	20.0	0.6	3.0	<u></u>
C-DIP Lids				1	!
_	0				
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S	0				
Cerumic Lids					
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য	0				
S	0				

48. Surface Absorbtion Radiflo

	103	00000000000000000000000000000000000000
VALUNTION	10130	
ORFICE E	T084 60/4	
DATA X10	T084 60/4	
HEL TÜM CO	1084 50/2	
	UNIT NUM.	しょうしょう ない とうしょ とうしょ とうしょ とうしょ とうしょ とうしょ とうしょ とうしょ

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VALUATION / SEC	70133 60/1	٠	٠	٠	٠	٠	•			•	٠	•	•	٠	٠	٠		٠	٠	٠	•	•	•	•					•	•	•	٠	•	•	•	•	•	•					•	•		ċ	•	,	•
ORFICE E	T084 60/4	•	٠	•	٠		•			٠	٠	•	٠	٠	٠	٠	٠	٠	•	•		•	•	•	٠	٠	_:	٠		٠	•	٠	•	٠	٠	•	•		• •		8		•	٠	•	٠	٠	3	•
ONTROLLED DATA X10	T084 60/4	•	•	٠	٠	•			•	٠	•	•	•	•	•	•	•	ີ		•	0	•	ċ	•		•		•	•	•	•	•	m i	•	•	3 0	•	•	•		0	2	 -	•	٠	ö,	•		•
HELTUM C	1384 60/2	•	٠	٠	٠	•	•		•	•	•	٠	٠	•	٠	٠	٠	٠	٠		•	•	•	٠	•		٠		•	4		•	٠	•	•	•	•	•		• (•		•	٠	•	٠	•		•
	UNI T																																															, c	

50. TO-84 Weight Gain Data (Sheet 1 of 2)

				WEIGHT GAIN DAT PACKAGE TYPE :	4 DATA PE : TO 84		
	COLU WE 1G	HN.HEADING =	COLUMN.HEADING = BOMB PRESSURE WEIGHT RECORDED IN GRAMS	/ INDICATOR FLUID	FLUID		
UNI T NUMBER	60/PP1 NT GAIN	60/PP2 HT GAIN	60/FC77 WT GAIN	60/FC78 WT GAIN	30/FC78 WT GAIN	90/FC78 WT GAIN	105/FC78 WT GAIN
-	0.0089	0.0173	0.0046	0.0067	0.0092	0.01 44	0.0126
2	0.0	0.0	0.0	0.0002	1000.0	9	0.000
m ×	0.0	0.0001	0.0	0.0	0.0	•	0.3302
t v	•		•	1000.0	20002	٠	70000
N vo	0.000	0.0001		0000	000		0.000
7	0.0	0.0	0.0	0.0	1000.0		0000
æ (100000	0.0	0.0	0.0001	0.0001	•	0.000
o <u>c</u>	0.0001	0.0	0.0	0.0002	0.0001	0.0	0.0003
2 -	0.0150	0.0162	0.000	0.0	2000	2000	0.000
12	0.0	0.0	0.0005	١.	0.0	9	0.0005
13	0.0	0.0	•	0.0	0.0002	0.0	0.000
5 1	0.0001	0.0001	0.0	0.0008	0.0002	500000	0.0
4	0.0	0.0003	2000	0.0003	0.0002	0.0	0.0004
27		60,000	0000	0.00	5000	8410.0	0.10.0
81	0.000	0.0	0.0		0000	20000	
19	0.0	0.0	0.0	0.0	0.0	0.0	0.000
50	0.0	0.0001	0.0001	0.0	1000.0	0.0002	7000.0
21	0.0002	0.0	0.0	0.0	100000	0.0002	0.000
77	9000	5100.0	0.0003	5000	60003	8000.0	0.0013
25	20005	0.0005	0.00		2000	0.000	81000
52	0.0136	0.0218	0.0075	0.0012	2.0207	0.0201	0.0194
26	0.0	0.0	0.0	0.0	0.0	0.0	0.0002
27	0.0003	0.0	40000	0.0	0.0001	0.0	0.0012
23	0.000	0.00	1000.0	0.0004	0.00	0 0	0.0
30	0.0022	0.0075	0.0013	0.0	0.0026	0.0083	0.0027
31	0.0188	0.0203	0.0197	0.0191	0.0194	0610-0	0.0189
35	0.000	0.0021	0.0005	0.0005	0.0008	0.0023	91000
n 4	0.000	1000	1000	0.0	0.0	0.0002	0.0
35	0.0003	0.0001	0.0001	0.0	0.0002	0.0007	0.0002
3.6		0.0007	0.0001	0.0	0.0004	900000	0.0011
~ 0 6	0 0	0.00	0.0	0.0	0.0001	0.0	0.0302
0 0		0.000	•	•	0.0	0.00	0.0
0.4	• •	0	0	0.0002	5000	•	1000
4 3	٥•٥	0.0	0.0	0.0002	0.0	0.0	0.0
45	0.0	0.0001	•	0.0	0.0	0.0	0.0001
φ, ,	0.0	0.0	0.0	0.0001	0.0002	0.0	0.0
* u		•		0.0001	0.0	0,0	0.0
4 4	000			5000		•	0.000
24	0.0	0.0003	0.0003	0.00%	0	0.000	0.0087
8,	0.0	0.0	0.0	0.0003	0.0	o.	0.0
5 0	0.0	0.0	0.0	0.0002	0.0	0.0	
20	sonoo.	6100.0	0.0003	0.0010	0°000¢	600000	0.0312

50. TO-84 Weight Gain Data (Sheet 2 of 2)

Canta dotacione / Bailskage xFde a oniveam

	105/FC78 HT GAIN	0.0	0.0	4000	0.0	0.0003	0.0002	0.0	2000	0.0007	0.0020	0.0015	0.0	******	2900.0	0.0076	0.0001	0.0001	0.0330	٥٠0047	2.0106	0.00	0.0104	7.200.0	4. CO. O	0.0081	0.0078	******	0.0074	0.0138	0.0123	0.0004	6600.0	00000	0.0055	0.0008	0.0	0.0	0.0315	0.0010	90000	0.0	
	90/FC78 WT GAIN	0.0	0	900	0.0	0.0	0.0	0°000	0.0004 0.0004	0.0303	0.0008	0.0003	0.0	79000	0.0035	0.0109	9100.0	0.0	2010.0	0.0143	0.0148	0.0143	0.0152	0.0151	0.0149	0.0144	9410-0	9700	0.0192	0.0135	0.0100	0.0149	95100	00000	0.0152	7600-0	0.0101	0.0102	9010*0	0.0098	0.0103	9900.0	
FLUID	30/FC78 WT GAIN	0.0	0.0	F 000	0.000	0.0	0.0	•	*000°0		0.0	0.0007	0.0	66000	• •		0.0046	•	•	0.0145	0.0154	• •	2.0150	0.0151	0.0149	0.0161	0.0140				٠	0.0151	1010		0.0142			0.0003	0.0099	0.0097	9010.0	0.0070	
/ INDICATOR FLUID	60/FC78 WT GAIN	6000*0	0.0001	0.0005	0.0005	0.0002	0.0001	0.0001	0000	0.000	0.0013	0.0011	0.0003	8600	0.0088	0.0111	0.0065	0.0	0.0109	0.0161	0.01.4	60.0	0.0154	0.0174	0.0159	0.0162	0.0148	0.01.75	0.0194	0.0152	0.0156	0.0156	20102	0.0050	0.0156	960000	0,0107	0.0107	0.0115	0.0101	3 3	0.0116	
ECAB PRESSURE In Grams	60/FC77 WT GAIN	0.0002	0.0	0.0022	0.0005	0.0002	0.0	0.0	90000	0.0002	0.0001	0.0007	0.0001	6600	0.00%	0.0112	0.0003	0.0	0.0112	0.0166	9910-0	0.0202	0.0160	0.0177	0.0163	0.0173	0.0158	0.010.0	0.0195	0.0159	0.0169	0.0158	0.0106	0.00	0.0164	0.0097	0.0108	0.0109	0.0117	0.0103	010	0.0116	
MEADING = RECORDED 1	60/PP2 WT GAIN	4000*0	0.0	0.0003	0.0007	0.0003	0.0004	0.003	0.000	0.0007	0.0001	0.0019	0.0003	5010.0	0.0093	0.0117	0.0064	0.0	0.0119	99100	0.0170	0.020	0.0111	0.0171	0.0167	0.0167	0.0154	0.0156	0-0202	0.0163	0.0164	0.0161	6010-0	5000	0.0163	0.0103		0.0111	0.0119	0.0107	0-0112	0.0108	
COLUIN	60.7PP1 WT GAIN	0.0002	000	0.000	0.0002	0.0	0.0	0.0	0.0003	0.0001	0.0	0.0009	0.0123	5000	0.0076	0.0104	0.0064	0.0	0.0104	0.0155	0.0147	1610.0	0.0151	0.0157	0.0157	0.0159	0.0147	0.010	0.0186	0.0029	0.0150	0.0147	0.00%	0.0103	0.0149	96000	0.0102	0.0102	0.0111	0.0097	8600.0	0.00%	
	UNIT TUMBER	51	25	3,0	55	99	57	8 6	6 0	61	62	63	4 1	64	29	89	69	20	7.	22	5,7	22	16	7.7	78	46	080	10	3 60	8	85	98	200	0 0	06	16	36	63	5 6	_ک ز :	9 6	98	

51. C-PAK Weight Gain Data (Sheet 1 of 2)

UNIT NUMBER	194 194 191	COLUMN HEADING #	BOMB PRESSUR IN GRAMS	E / INCICATOR	FLUID		
NUMBER							
	60/PP1 WY GAIN	607PP2 WT GAIN	60/FC77 MT GAIN	60/FC78 WI GAIN	30/FC78 WT GAIN	90/FC78 WT GAIN	105/FC7 WT GAI
	0.0264	720	7 20	0,0266	020	.026	0.026
• ~	0.0202	0.0064	0.0051	8		0.0207	0.020
m	0.0147	,003	•005	0,0056	9	•015	410.0
4	0.0243	.025	10.	0.0244	000	954	0.024
v	0.0215	.023	8	C. 0218	7	36	770.0
• 1	0.0213	220		0.0212	0.0052	200	0.020
~ 0	0.0203	30	700	0.0100	90	200	00.0
0 7	670.0			0.0	9	000	0000
10	021	. G22	.022	0.0215		.021	0.021
: =	013	• 000	800	0.0186		•018	910.0
12	0.0258	0.0274	.027	0.0262	0.0252	•056	0.025
13	024	70	60.	C. 0201		925	800.0
5 7	0.0268	33	• • •	0.0266	•	920	20.00
. 2	0.0041	ខ្លួន	0.0	2000 5	20	36	200
9 !	0.00	36	÷ 5	3 6	? ?		2000
3 2	0-0210	200	30			921	0.021
2 2	0-0	100	0	8	9	8	000.0
50	0,0003	8	000	0.0		8	00000
21	D.0242	929	•025	C. 0245	•	500	0.022
22	0.0211	770	•027	0.0265	•	950	8.000
23	0.0272	828	0.0285	0.0279	0.0294	028	920.0
4 %	0.0256	30	200	0.0216		022	0.02
6,7	0.00	<u>.</u>		0-0	•	0	200.0
2,7	0.0042	0,000	0.0038	, 8		905	0.001
28	0.0219	0.0229	0	0	•	•022	910.0
53	0.0253	0.0265	•026	3	0.0180	•025	0.024
30	0.0025	0.000	8	0.0	•	200	0000
# £	0.0228	0.0203	0.023	\$ 10 ° 0		220	2000
25	0.0179	0.038	֓֞֜֜֜֟֜֜֝֓֓֓֓֓֓֓֓֜֟֜֓֓֓֓֓֓֓֓֓֡֓֜֟֓֓֓֓֓֡֓֜֡֓֡֓֡֡֡֓֡֓֡֡֡֡֡֓֡֡֡	0,0270		027	0.026
n 49	0.0193	0.0205	050	0.0205		50.	0.018
32	0.0201	0.0217	•015	0.0203	•	020	0.017
36	0.0195	0.0208	250	0.0196		500	910.0
37	•	0.0078	9	9,10,0	•	870	
æ ç	•	•	38	0000	• •	3	5700
6 4 0 4	0.0188	0.0133	0,000	0.0183	0.0121	60	610-0
3 7			8	0,0002	•	8	0.01
45			900	0.0191	•	10.	0.015
43	9	0.0222	•022	0.0216	•	057	210.0
\$	0	9	8	0	0	8	0000
45	?;	220	36	2 C	3 6	36	1000
ę !	36	9 6	9	֓֞֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜			2000
7 4		0.0086		0,0089	0	021	400
9	5	020	020	6	.007	018	0.017
20	8	0.0224	015	0.0310	0.0182	.021	0.021

MEIGHT GAIN DATA PACKAGE TYPE : CPAK

	COLUMN	HEADING	BOMB PRESSURE IN GRAMS	/ INDICATOR	FLUID		-
NI T HB ER	60/PP1 MT GAIN	60/PP2 WT GAIN	60/FC77 WT GAIH	6C/FC78 WT GAIN	30/FC78 WT GAIN	90/FC78 WT GAIN	105/FC78 WT GAIN
22	0.0216	0	0.0225	0.0218		.022	4.00.0
25.52	8	0.0031		00	00	E 000°0	0.0002
3,0	0.0005		0.0132	0.0136	0	.03	0.0043
55	0.0032	-	0.0020	0.0012	0.0012	200	0.0032
ט ג ני	0.002		2000		500	8	0.0020
28	0.0014	0.0004	0.0001	0.0005	90000	8	0.0
29	0.0001		0.0	°.	0.0	0	0.0003
09	0.0191		0.0054	0.0108	0.0075	50	0.0072
79	0.0216		29000	8,	4100.0	5	20.00
79	0.0015	2000	10000	0.00	- COO - CO	1000	0.0177
3 49	0.0133		0.0020	0.0030	0.0023	9	160000
65	0.0208		0.0259	0.0209	0.0053	.021	0.0213
99	0.0108		0.0005	.0.0020	0.0034	900	6,000.0
29	0.0207		0.0214	C. 0206	0.0	250	0.0200
89	1610.0		9200.0	0.000	2,00,0		
2 6	7000		0000			9	0000
2.2	0.0196	0.0206	0.0205	0.0198	0.0110	200	0.0192
12	0.0190		0.0202	5	0.0001	9	0.0108
	•	•	0.0	0.0	•	88	9000.0
2 7	•	0000	5		000	36	0000
0 %	•	000	į				E000*0
2.2			9	0	0	•	400000
78		•	કૃ	0.0114	0.0081	020	0.0195
2	•		8	0.0	0.0	8	8
90	•		99000	5010-5	0.0120	20	20
	•	•	3,	\$ 10.0		7	30
26	0.00		*000		0.0002	0	0.000
4.0		0.0211	•	0.0201	0.0200	070	5
85	0.0	0.0002		0.0	0.0	8	ဒိုး
98	•	0.0287	ö	0.0274	1000 0	200	õ
28	0.0211	0.024	1220.0	0.0014	0.000		0.0256
9 6	0,0001		ĕ		00001	8	18
38	0.0001	0.0002	ĕ		0.0	0	ş
16	0.0210	022	ö	C.0022	0.0211	₹	0.0033
26	0.0	8	0.0	٠,	0	•	0.0032
93	٠	8		9	0.0		5000
46	0.0	0000	•000•0	1610.0	2000	4000.0	000000
0.0	:	3			9500	200	7020.0
9.6	0.000	30	64100	20	0.0		, 3
96		0	8		0.0	3	3
66	.021	0.0224	.413	C. 0149	0.0009	.021	õ
00	•	0	8	•	0.0	•	ŝ

51. C-PAK Weight Gain Data (Sheet 2 of 2)

52. C-DIP Weight Gain Data (Sheet 1 of 2)

				WEIGHT GAIN DATA PACKAGE TYPE :	N DATA PE : COIP		
	COLUMN	HEADING .	BOMB PRESSURE IN GRAMS	/ INDICATOR FLUI	FLUID		
UNIT	60/PP1 WT GAIN	60/PP 2 WT GAIN	60/FC77 WT GAIN	60/FC78 WT GAIN	30/FC78 NT GAIN	90/FC78 WT GAIN	105/FC78 MT GAIN
-	0.0	0.0002	0.0003	0.0	0.0	0.0	0.0
. 2	0	0.0	900000	0.0001			•
m	0.0	0.0004	0.0	C.0003	0.0		•
4 u	0.0	0.0	0 0	0.0001	000	0 0	000
n «	0 0	6000	0.0007	0.0001	0,0001	0	• •
۰,	• •	0	0.0	900000	0.0	0	0
60	0.0	0.0	5000.0	10000	0.0	0.0001	0:
6 5	0.0	0.0	0.0	0.0	0.0	0.0002	0.0
21	0.0001	0,0003	0.0	0.0002	90	0.0002	0.0
12	0.0	0.0	0.0	0.0001	0.0	0.0010	0.0012
13	0.0	0.0	0.0	0.0001	0.0	0.0003	0.0
14 15	0.0	0.0002	1000.0	0.000	3 0	1000	1000.0
5 2	0		0.0	10000	0		0
17	0.0	0.0	0.0	0.0	0.0	0.0	•
18	0.0	0.0	0.0	0.0	0.0	0.0	•
16	0.0	0.0	0.0009	0.0001	0 0	0.0	
2 2	0	1000	0.0		200	0	0.0
22	0.0	0.0	0.0	0.0001	6666*0	0.0	0.0002
23	0.0	0.0001	0.0016	c.0003	0.0001	0.0005	0.0002
47 40	0.0	10000	0.00	410000	0.000	0,0000	0.0007
\$ 2	0.0	0.0002	0.0	0.0	0.0	0.0	0.0
2.7	0.0001	0.0002	0.0	0.0002	0.0002	0.0002	10000
5 5 7 8 8	0.0011	0.0021	9000	2.001.2	50002	0.0020	6100.0
<u>ئ</u>	2000			0.0	• 1		
31	9000*0	0.0007	0.0005	0.0004	0.0001	0.0005	0.0004
32	0.0	0.0003	0.0	0.0	0.0001	0.000	0.0
e c	0.0005	0.0010	0.0005	0.0012	0.0	0.0005	90000
ب بر			0 0		0		0
36	0.0	0.0007	0.0	0.0001	0.0	0.0001	10000
37	0.0	0.0001	0.0001	0.0003	0.0001	0.0	00000
e 6	0.0		50.0	200	0.00	0.00	0.00
4 0	0.0002	0.0010	600000	0.0004	0.0001	0.0005	0.000
41	600000	0.0005	0.0007	0.0005	0.0005	0.0009	0.0011
45	0.0362	0.0379	0.0387	0.0355	0.0312	0-0322	0.0039
M .	0.0001	0,0032	0.0	50000	0.0005	0.0024	100.0
t 4	0.0334	0.0000	0.00	0.000	0.00040	0.0013	0.00
40	0.0001	0.0	0.0	0.0002	0.0	0.0004	0.0
47	0.0019	0.0045	0.0021	0.0022	0.0020	0.0037	0.0026
84	0.0	0.0	0.0	0.0	0.0	000	•
4 G	0.0	0.007	0.0005	0.0005	0.0010	0.00	0.0019
ì			1	1) 	1 	

WEIGHT RECORDED IN GRANS 60/PP 2 60/FC77 60/FC78 30/ MT GAIN WT GAIN WT
0.0010 0.0001
0.0001
0.0
23
0.0032 0.0007
_
0.0014 0.0009
0.0028 0.0017
0.0051 0.0
0.0
202
0.0001 0.0
100
0.0 0.0
0.0
7.2
0.0 0.0
0.0038 0.0013
0.0191 0.0251
0.0265 0.0278
0.0292 0.0282
280
0.0
0.0490

52. C-DIP Weight Gain Data (Sheet 2 of 2)

MEIGHT GAIN DATA Package TYPE : Mosulp

	105/FC78 HT GAIN	1000-0	0.0	0.0	0.0002	0.0	0.0	0.0001	0.0001	9000	0.0012	0.0	0.0001	9	00000		0.0003	0.0001	000	200	0.000	90000	1000	0.0538	0.0013	0.0008	0,0023	0.0012	3.0002	0.0008	0100.0	0.0023	0.0005	1.0003	0.0000	0.0005	0.000	1000.0	3.0004	0.0044
	90/FCT8 WT GAIN	0.0002	0.0003	40004	0.0001	0.0003	5000	0.0001	0.0001	0.000 0.000	0.0022	0.0003	0.0	0.0	2000-0	9000.0	900000	0.0017	0000	0.0003	0.0008	0.0007	90000	7,000,0	6.0023	0.0016	0.0047	60000	0.0	9100.0	0.0010	0.0050	0.0018	60000	0000	0.0008	0.0025	0.0	905	0.0076
FLUID	30/FC78 WT GAIN	0,0005	0.0003	0.0004	0.0054	0.0	1000	0.0003	0.0054	90000	0.000	C.0003	0.0004	0.0001	5000	C.0003	C. 0001	0.0006	5000	C.0002	C.0005	0.0005	4000	0.0808	C.0007	0.0004	0.0011	0.0008	0.0004	0.0006	\$0000	0.0013	0.0007	9000°0	0.000	2,000,0	0.0000	C. C003	0.0500	0.0025
/ INDICATOR FLUID	60/FC78 M1 GAIN	6200.0	0.0	0 C	0	6.0004	0000	0.000	C. 0008	C- 0007		0.0	0.0001	0.0	2002			C. 0004	0.0630	0.0013	0.0	0.0013	50002	0.0679	0.0		0.0	0.0011	J	0.0003	0 4		0.0	C. COC4	2,000	2100.0	C. 0002	C- 0003	0.0	0.0010
BOHD PRESSURE N GRAMS	60/FC77 WT GAIN	0.0082	0.0030	0.0031	0.0159	0.0426	0.0163	0.0175	0.0026	0.0013	6000.0	0.0025	0.0055	0.0002	20019	0.00.0	0.0003	900000	9000	0.000	0.0014	0.0012	0.1018	0.0827	0.0014	0.0008	0.0004	0.0015	0.0050	0.0010	0.0004	0.0003	C.0037	0.0347	6200.0	5100-0	0.0020	0.0008	0.0016	0.0010
HEADING = RECORDED 1	60/PP2 WT GAIN	0.0002		2,000		C. 0002	0003	0.0002	•	0.0004		c. 0003	0.0002	C. 0002	0007		0.0003	6.0007	0000		0° 000 ÷	0.0003	20005	0.0035	C.0007	٠	8000		0.0003	90000	2000	9000.0	c. 0096	0.0004	5000	0.0004	C. 0009	0.0002	0.0007	0.0011
COLURN	60/PP1 WT GAIN	0.0002	0.0004	0.0003	0.0002	0.0002	0.000	0.0001	0.0003	0.0015	0.0016	0.0001	0.0004	0.0003	0,0001	0.000	0.000.0	0,0020	1000	0.0001	0.0010	0.0011	00000	0.020	0.0018	0.0016	0.0032	0.0126	0.0003	0.0018	0.0018	0.0035	0.0013	0.0006				•	000	0.000
	UNIT	- ~	ا مين ا	or ur	۰.	: ~ (2) 0	. 5	11	21.5	7 2	51	9	1.	P 0	£ 02	21	22	ç 7 7	52	26	27	28	۶ <u>۲</u>	3 %	32	33	35	36	37	20 CE	40,	14	45	î	4 1	4 0	1.4	æ (50

53. MOS DIP Weight Gain Data (Sheet 1 of 2)

WEIGHT GAIN DATA PACKAGE TYPE : MOSOI

	•						
	COLUMN WEIGHT	RECORCED	E BUMB PRESSURE IN GRAMS	/ INDICATOR FLOID	FLUID		
INI T IMBER	60/PP1 WT GAIN	60/PP2 HT GAIN	60/FC77 WT GAIN	60/FC78 WI GAIN	30/FC78 MT GAIN	90/FC78 WT GAIN	105/FC78 AT GAIN
15	0.0001	0.0005	000	0.0	0.0015	0.0001	0.0
52	5	0.0004.	~	0.0	0.0002	0,5	ဝှင်
5,5	0.0004	100.0	0.00.0	6000		0.000.0	1100.0
55		0.0003	200				0
20			.00	0.0052	•	.017	9
57	0.0020		_	0.0	33	0.0015	6000°
æ 9	•	38	9100.0	2000	2000	Š	200
7 0	0.00	3 8		5 0		9	
6 2	0.0014	80		0		0.0012	0.0005
62	0.0002	000	000	0.0	•	0	
63	0.0104	200	5100.0	c. 0004	•	•	99000
40,	9	96	_	0.0	-	0.0	1000.0
607		2 5	֪֝֟֓֓֓֟֝֟֓֓֓֟֟֓֓֓֓֟֟֓֓֓֟֓֓֓֟֓֓֓֓֓֟֓֓֓֟֓֓	\$	9000	0.009	0000
200	3	0.0002	3		? ?		0
89	0.0001	0.0002	100	C. 0001	0	•	0.0
69		0.0	0.0002	0.0	00000	•	0.0
2	0.0	0.0001	000	0.0	90	٥	0.0
7.	•	0.1058	20.	C. C761	٠	<u> </u>	0.0771
2 2	0.0022	0.0005	0.0011	6.0	C.0007	0.0013	0.0005
2		0.0240	0.0321	0.0383		960	1050.0
75	0.1002	0.0334	0.0494	038		101	9
76	0.0183	0.0022		C. 0007	.003	.018	9
7.	0.0251	0.0030	0.0032	0.0021	0.0053	0.0275	0.0086
9 0	0.0418	0.000	0.000	7,104	3 6	50	? -
2 8	0.0428	0.1054	• •	0.0684	9	200	: ?
81	0.0974	0.1036	: =	0.0718		0.0986	0.0522
85	0.1053	0.1128	0.1107	0.0596	0.1067	8	٠,
83	0.0978	0.1035	.114	C. 0327	•	0.0983	• १
46	0.000	9960	2760-0	783°0	? -	5	ء و
2 %	0.0505	0.0054	005	0.0057	• •	8	0.0117
87	0.0013	0.000	0.0007	0.0002		800	ŝ
88	0.0279	0	0.0079	1900.0	•	.034	ဒို
68	0.0779	0.0590	0.0734	0.0597	٠	078	S
g ;	0.0043	200	9700-0	0.00	•	35	3 6
. 6	0.0771	0.0821	0.0804	70.00	0.0352	0.0769	Vи
93	081	045	0.0472	0.0445		085	ဒို
94		683	0.0888	0.0692		•085	ş
95	•	0.0955	m	C•0553	.097	60.	0.0588
96	• 089	60.	460	0.0503	099	084	٠,
76	160	٤:	0.1035	0800	٠,	•	٠,
86	60.	2 8	0.1039	0.0710	9	7 0	2.5
560	0.0879	1 460 0	0.0978	0.0751	9 6	8880.0	7.5
3	٠	5	1	•	•		

53. MOS DIP Weight Gain Data (Sheet 2 of 2)

				WEIGHI GAIN DATA PACKAGE TYPE :	N DATA PE : 10100		
	COLUMN	COLUMN HEADING * BOMB PR WEIGHT RECORDED IN GRAMS	BOMB PRESSURE IN GRAMS	/ INDICATOR	FLUID		
UNET UMBER	60/PP1 WT GAIN	60/PP2 WT GAIN	60/FC77 WT GAIN	60/FC78 WT GAIN	30/FC78 WT GAIN	90/FC78	105/FC78 WT GAIN
						•	
 (0.0	0 0	0.0	0.0001	0.0002	1000.0	0.0
ı m	0.0	0.0001	0.0003	0.0102	0.0001		000
4	0.0001	0,0001	0.0001	0.0	0.0	0.0004	0.0002
ď	0.0	0.0003	0.0003	0.0	1000.0	o•0	0.0
9 F	0.0	0.0	0.0	0.0	0.0	0.0	0.0
- α	3000	1000	2000	5000	1000	7000	1000
. 0	0.0		0.0003	0.0005	0.0003	\$000°0	3,0059
01	0.0	0	0.0002	0.0053	0.0002	0,000	0.0
7	0.0	0.0001	0.0	0.0001	0.0001	0.0003	0.0003
12	0.0	0.0	0.0	0.0	ə ·	0.0	0.0
<u>:</u>	0.0	1000.0	2000.0	20002	2000	9000	0.0003
<u> </u>	30	0.0002	1000	70007	1000	7000-0	7000
21	0	0.0002	0.0002	0.000		10000	10000
11	0.0	0.0001	0.0002	0.0003		0.0005	0.0
18	0.0	0.0	0.0	0.0	0.0	0.0	0.0
19	0.0	1000.0	0.0	0.0002	0.0	900000	9000*0
50	ი•0	0.0	0.0011	0.0	0.0001	0.0003	0.0
21	0.0	0.0	0.0	0.0012	0.0012	0.0001	0.0
77		7000	1100.0	70007	7000	70000	•
2,5	1000	0 0		0000	70000	2000	90
52	0.0001	0.0002	0.0002	0	0.0001	0.0002	0.0002
56	0.0003	0.0001	0.0003	٠,0004	\$000°0	0.0005	900000
27	0.0	0.0002	0.0001	0.003	0.0001	0.0102	0.0
28	0.0	0.0002	0.0	0.0	0.0002	9,000	0.0218
50	0.0	0.0003	0.0043	0.0003	0.0003	1000.0	00
90	0.000	1000	1000	0.0002	0.00	1000-0	0.00
32	0.0	0.0	0.0	2000	0.0	0.0	0.0
33	0.0	0.0002	0.0002	0.0006	0.0001	0.0001	900000
34	0-0	0.0002	0.0002	0.0004	0.0002	0.0007	900000
35	0.0	0.0	0.0	0.0002	0.0003	0.0001	0.0
200	•	7000	•	2000	0.0003	9000	90
38	0	00000	0.0002	00000	0.0001	0.0005	0.0002
39	0.0	0.0	0.0	0.0	0.0	0.0	0.0
40	0.0114	0.0306	0.0139	0.0231	0.0257	0.0534	0.0245
41	0.0	0.0002	0.0034	0.0002	100000	0.0003	0.0
75	0.0	0.0001	2000.0	0.0006	0.0002	90000	0.0003
43	3	•	ے د د	10000	1000	1000.0	
• u		***	2000	2000	700	200	0000
100	*000	0.0002	0.0002	00000	0.0001	0.0000	00000
14	0.0048	0.0049	0.0042	0.0084	0.0000	0.0113	0.0027
48	0.0	0.0003	0.0002	0.0003	0.0004	0.0005	0.0
64	0.0	0.0002	0.0002	0.0002	0.0	0.0002	0.0
20	0.0001	0.0001	0.0005	0.0001	0.0	0.0	1000.0

54. TO-100 Weight Gain Data (Sheet 1 of 2)

WEIGHT GAIN DATA PACKAGE TYPE : TOLUO

				PACKAGE TYPE	PE : T0100		
	COLU	JMN HEADING *	COLUMN HEADING * BOMB PRESSURE WEIGHT RECORDED IN GRAHS	/ INDICATOR FLUID	FLUID		
UNIT NUMBER	60/PP1 WT GAIN	60/PP2 WT GAIN	60/FC77 WT GAIN	60/FC78 WT GAIN	30/FC78 WT GAIN	90/FC78 WT GAIN	105/FC78 WT GAIN
51	0.0	0.0	0.0	0.0	0.0	0.0	0.0
52	0.0	0.0	0.0	0.0	٠	0.0	0.0
53	3.0001	0.0003	0.0	0.0005	0.0	0.0005	6.0003
54	0.0001	0.0004	0,0001	9000	٠	0.0006	2000.0
52	0.0	0.0	•	0.0004	0.0	0.0008	0.0003
20	0.0002	0.0004	0.0001	0.0007	0.0004	6000	0000
- 04	2000	0.0003	2000 0	50003	0.000	5000	
0 0				ò c	•	200	900
60	000	000				, ,	0
19	0.0	0.0001	0.0	0.0003	0.0	0.0001	0.0
62	0.0	0.0001		0.0004	0.0003	0.0003	0.0004
63	0.0001	0.0002	0.0010	0.0004	0.0005	600000	0.0004
64	0.0	0.0	•	0.0	0.0	0.0	0.0
65	0.0	0.0004	•	0.0010	0.0003	0.0007	0-0005
99	0.0	0.0001	0.0002	0,0001	•	0.000	•
29	o•0	0.0	•	0.0	0.0	0.0	0.00
89	0.0	0.0004	•	0.001	0.000	0.0004	070000
69 6	0.000	0.0003	0.0030	60000	******	0000	0000
2;	0.00	0000	200	2.00		660	9000
1,1	6000	0000	0000	35.00.0	7100.0	2000	2000
2 6	2100	4100		0.003	•	0.0030	0.0037
27.	0.0002	0.000	• •	0.0005	70000	90000	0.0005
75	0.0002	0.0003	0.0	0.0007	0.000	600000	0.0005
76	0.0	0.0003	0.0001	0.0064	0.0001	0.3007	0.0005
7.7	0.0024	0.0026	0.0018	0.0	0.0024	0.0072	0.0038
78	0.0074	0.0039	٠	0.0077	0.0012	0.0088	0.0112
6/	0.0	0.0	٠	0.0	0.0	200	900
80.	00000	0.0001	•	9.000	5000.0	0100.0	0.000
7.0	7000-0	0000	0000	7000	1000	57000	2000
3.6	0.0	0		0.0001	0.0002	0-0002	0.0001
84	0.0	0.0	0.0	0.0	0.0	0.0	0.0
85	0.0009	0.0012	0.0010	0.0012	6000*0	0.0019	0.0024
98	0.0007	0.0007	0.000	0.0013	0.0012	0.0013	0.0026
87	0.0010	0.0008	00000	7100.0	0.0010	8700.0	0.008
800	0.0001	2000	•	90000	7000	2000	1000
7 0	1000.0	0.000	0.0	0.000	100000	72000	00000
9 5	0.000	0.0004	4000	0.0010	0.0004	600000	0.0007
92	0.0764	0.0809		0.1218	0.0620	0.1324	0.0461
93	0.0144	0.0317	0.0114	0.0297	0.0101	0.0385	0.0305
94	0.0480	0.0462	0.0335	0.0775	0.0420	0.1748	0.0408
95	0.1783	0.1704	0.1283	0.1793	0.1646	0.1795	0.1770
96	0.0012	0.0015	0.0012	0.0027	0.0002	0.0021	0.0033
36	0.0058	0.0053	0.50.0	0.0104	0.00.0	1110.0	2010.0
86	2900-0	0.0073	0.0160	2,0175	0.0442	0.0243	0.0278
7.6	0.0010	7070.0		1	31	+ • • •	,

54. TO-100 Weight Gain Data (Sheet 2 of 2)

				WEIGHT GAIN DATA PACKAGE TYPE 1 C	N DATA Pe i Ceranic		
	COLUMN	N HEADING	BOMB PRESSURE IN GRAMS	/ INDICATOR	וירטוס		
UNIT NJHBER	60/PP1	60/PP2 WT CAIN	60/FC77 WT GAIN	60/FC78 WT GAIN	30/FC78 WT GAIN	90/FC78	105/FC76 HT GAIN
-	0.0001	0.0002	0.0013	0,000	•	9074.0	0.0483
~	900000	900000	ó	0.0005	1000.0	0.0	
m «	00000	9000	0.000±	0.000	•	3,	0000
-	, 000°	2000	•	2000	•	200	Э.
۰.5	0.0003	0.000		2000	• •	10000	30
٧	0.0001	0.0002	0	0.0003		00000	
æ (0.000	0.0003	•	0.1173	•	0.000	0
~ 5	0.0	1000.0	0 8	0.0000	4200.0	2000	0.5
:=	0.0544	0.1668		0.469	• •	0.44.0	0.266
21	0.5	0.0	2	0.6149	•	0,0003	0.530
<u> </u>	1000.0	0.0001	•	2000.0	•	90000	0.0
<u>-</u>	9 6	1000	600.0		•	0100.0	90
9.~	0			0000		0.00.0	0.00
-1	0.0	0.0001	2	00000	•	0.0325	0.000
æ	0.7913	0,0	0.8272	0.7968	•	0.6011	0.1856
2 2	0.0	2000	200	5000	•	666.0	7
21	0.7424	0.73:5	§	0.7510	•	425.0	0.3026
22	0.1412	0.1536	. HO.	0.7726	•	0.7769	0.6150
m <	0.5085	0.000	o i	0000	•	2461.0	0,225
, eo	0.698	2460	35	80.0	-,		3446
92	0.5695	0.3110	. 772	0.7485		0.7467	0.089
7	0.005 0.005	0.1890	916	0.0888	•	0.8833	0.635
5 O	0.874	2000	77.	20.00	•	40°00	0,7849
ន្ត	0.8276	2940	200	0,6416		F 198.0	200
16	0.8367	0.000	076	0.0449	•	9.44	2.0
% r	00000	2000	.47	0.0102	•	0.00°0	361.0
7 M	0,010	0,000	25	0.39.7	•	110.0	6,00,00
3.5	0.000	4.0005	. 63	0.7877		8070.0	
91	0.9033	0.9515	•	0,9196	•	2.0	0.3354
90	0.6900	2000			•	0.400	50
33	0.0	0.0004	0	0.000		0.000	6
0.	0.0	0.0003	•	0.0006	•	2100.0	9
15	0.000	0,0	0	60000	•	0.55.0	a :
v 4	0.7642	0.134		22.0		0.704	::
4 ·	0.6931	0.7371	3,20	0.7043		0.7020	2
ያ ላ	2000	2000	9		•	5000	2:
2 ~	0.0	200000	0.0001	00000	2000.0	2000	0000
84.	0.6370	0.6783	699	0.6467		155910	
20	0.0	0.0000	0.00	0.00.0	9,60	4000.0	2:
						11.74.14	-

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55. Ceramic Weight Gain Data (Sheet 2 of 2)

					PACKAGE TY	PACKAGE TYPE I CERAMIC		
		COLUAN HE	HEADING .	BOHB PRESSURE IN GRAMS	/ INDICATOR PLUTO	FLUID		
NIT	AT GAIN		60/PP2	60/FC77 WT GAIN	60/FC78 MT GAIN	30/FC70 MT GAIN	90/FC78 WT GAIN	105/FC78 WT 0AIR
51	0.8899		0.9474	0.9327	0.9039	0.9045	0.9075	7649.0
25	0.0		1000	0.000	0.0002	0.0003	0.00.0	0000
53	0.0011		6000	0.0013	0700°0	0.0003	9	20000
54	0.7389		7872	0, 1722	0.2466	0.7524	1052.0	0.0345
22	0.6800		7256	0.7131	0.6897	7.6947	0.6401	- 5 - 5 - 6
56	0.8242		8798	0.8655	1.2889	0.8402	0.4361	0.5320
25	0.7042		7519	0.7390	0.7103	o. 71 86	0512.0	0.2433
58	0.8001		9660	9.8679	0.8386	0.0340	2,29.0	~÷~
59	0.7488		7867	0.7882	0. 7546	0.6841	3.6413	6.22.0
9	0.0003		2	0.0003	0.000	0,0001	e. 0	0.0
19	0,0005		1000	0.000	0.0	0.0003	ં	0.000
62	0.0001		0000	0.0005	0.00%	1000.0	~~~~	20000
63	0.8705		9293	0.9268	0.8924	0.8772	0.0514	0.3018
59	0.0003		0	0.0	0.0003	0.001	? •	0.000
65	0.0002		9	0,0002	0.0005	1000.0	0.0	2000.0
99	0.000		2000	0.000	0.000	0.000	?• 0	Q'0001
29	0.0		0	0.0002	0.0004	0.0	0.	0.3303
89	0.0		0	0.0	0,0005	1000.0	0.0	o o
69	0.0003		6000	0.0013	0.00	0.0003	o, o	(000'o
20	0.0001		0	0.0	0.0003	0.0	? •	0,0
=	0.0001		C000	0.0020	\$000°0	0.0	o •	2000°0

60/PP2 60/ WF GAIN WT
115
200
222
2186
200
1000
9500
6100

WEIGHT GAIN DATA PACKAGE TYPE : TO 3

0.0027 0.00191 0.0027 0.4648 1.7557 1.37924 1.37924 1.37924 1.37924 1.37924 1.37924 1.37925 0.00015 0.00015 0.00015 0.00016 0.00016 0.00016 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017 0.00017
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03 11 00 01 00 03 00 03 00 03 00 04 00 04 00 04 00 04 00 04 00 04
00183 0091 0024 0027 00202 0047 0034
2286 2286 0024 00202 0047 0024 0024
2286 0024 0202 0047 0024 0054
0202 0047 0024 0024 0054
00047 0024 0054
0024 0.
0054 0.
0012 0.
0104
0247 0.
1363 0.
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56. TO-3 Weight Gain Data (Sheet 2 of 2)

	GLASS
DATA	_
GAIN D	YPE
WEIGHT	PACKA
-	

	5	0.000	00100000	1 tunication course			
UNIT	60/PP1 MT 6414		60/FC77		30/FC78	90/FC78 MT GAIN	105/FC 78
,	•	,	,				
	0.0720	0.0762	0.0752	0.0732	.01	0.0724	0.0727
~	0.0412	043	5,0	0.0417	.041	0.1115	0.0419
m «	10000	0.0	900	0.0011	0.0		0.0002
t u	שכ	0300	1 0012	77.80.0	•	0.00	30,000
۰.	١c	2100	;	1000	•	0000	0.0
~	0.0	0.0	0.0			0.0	0.0001
60	0.0001	0.0	0.0	0.0001	•	000	_
0	0.5028	1.3728	1.3162	0.5393	.267	1.2679	1.1150
01	100000	0.0	0.0	0.0010	0.0002	000	0.0
11	0.0002	0.0	٥	0,0003	•	0.0	0.0
12		0.0533	021	0.0397	٠	0.0665	0.0334
<u>-۱</u>	0.3631	0.0201	0.0275	1.0621	0.2462	0.0275	0.0067
41	0.0587	0.0621	Α.	0.0594	0.0587	0.0578	0.0218
<u>.</u>	0.000	•	3	7.00°0	2200.0	9890-0	_
9 !	0.0	•	5	200	•	2000	٥ . د د
1		o .	5000	1000.0	•		•
n :		٠ د د	•	1000.0	•	5000	•
51	0.0	0.0		50000	•	200	
02	: : :	3	10001	9100-0	2 -	50000	20000
17	1161-1	1 1706	1.1017	1.1945	667.0	9001-1	0.000
23	1.0000	2		0.000		0.0000	0.0488
2,0	2000	•	200	1 4575	1.1752	1.6524	1 23 24
2.5	1 3867	1.4860	1.4686	45.45	1.4152	2017	0.4261
2,0	ľ	6.8176	• •	0.7824	0.1777	0.7784	0.5399
27	2	0.0569	0.0564	0.0549	0.0541	0.0537	0.0098
28	0.0589	0.0626	0.0646	0.0623	0.0622	0.0618	0.0196
53		0.0451	0.0446	0.0416	940	0.0430	0.0078
30	0.0519	0.0548	0.0539	0.0528		0.0522	0.0111
31	1.2935	1.3708	1.3536	1.3132	1.3039	1.3058	0.1467
32	1.2065	•	1.2600	•	٠	1.2160	0.1315
33	0.0	0.0	0.0014	8	٥.	0.0002	0.0
34	0.0909	0.0963	0.0949	0.0923	0.0915	0.0915	0.0560
35	0.0002	0.0	٥,	0	٠	0.0005	0.0
36	0	0.0731	220	9,5	0.0694	4440	76100
37	,	1.079	0.1380	σ (•	67671	400.00
38	0.0550	0.0282	5.65	50000	0.0557	20000	0.000
6	****	0.0342	0.0130	0.0419	•	90.00	41.40.0
) ·	0.170	•	1.0639	• •		024	0.0857
· ·	1 26 77	•	200	, ,	1.2565	257	0.8041
3 K	,0		1.1247	1.0904	1.0825	1.0845	0.0315
44	•	1.1707	1.1556	0.5197	112	1111	0.2348
45	30	1.3815	1.3621	8	313	1.3142	9
46	0.4033	1.0920	1.0768	1.0434	1.0375	~	8
47	ç	666*	0.9877	• 95	. 950	0.9520	57
84	47	1.0903	1.0767	1.0427	1.0353	1.0372	1.0338
5 (4.	.19		ŝ	900		7
2.0	0.0	0.0		0.0		0.00	0.6597
2,5	V- 3204	0.8443	760.	21000	• 000	700.	

57. Glass Standard Weight Gain Data (Sheet 2 of 2)

				PACKAGE TYPE :	PE : GLASS		
	8	COLUMN HEADING =	BOMB PRESSURE	/ INDICATOR FLUID	FLUTO		
UNIT NUMBER	60/PFI WT GAIN	60/PP2 WT GAIN	60/FC77 WT GAIN	60/FC78 WT GAIN	30/FC78 WT GAIN	90/FC78 WT GAIN	105/FC78 WT GAIN
63	0.0001	0.0	0.0004	0.0035	0.0	0.0002	0.0
7 6	00000	0.0	0.0	0.0001	0.0003	0.0002	2000.0
3 2	0.0	0.0	0.0	90000	0.0001	0.0002	1.0003
+ u	000	0.0	0.0	0.0002	0.0001	0	9
, 4	000	0.0	90000	0.0003	0.0002	0.0	70007
2 0	000	0-0	0.0	0.0002	0.0	0.0	0.0
- 0	2000		0.0	0.0	0.0	0.0001	0.0001
ο (Λ		•	0.0001	0.0005	0.0003	0.0	0.0
66	1000.0	200	0.06.15	0.0516	0.0241	0.0315	0.0213
09	2000	0.00	0.0620	0.0605	0.0398	0.0514	0.0233
19	1750.0	0,000	0.0463	0.0634	0.0614	9190.0	0.0605
29	0.0613	0.00	2+00-0	2000	0.0587	0.0579	0.0442
63	0.0576	0.0605	6660.0	10000		7070	1000
4	0.0693	0.0732	0.0724	0.0	26000	6000	
,	7440	0.0659	0.0691	0.0670	0.0655	6 9 9 9 9	20.0
6 4	0.0639	0.0673	0.0670	0.0657	0.0645	0.0644	0.0439
3	•						

MISSION of

Rome Air Development Center

RADC is the principal AFSC organization charged with planning and executing the USAF exploratory and advanced development programs for information sciences, intelligence, command, control and communications technology, products and services oriented to the needs of the USAF. Primary RADC mission areas are communications, electromagnetic guidance and control, surveillance of ground and aerospace objects, intelligence data collection and handling, information system technology, and electronic reliability, maintainability and compatibility. RADC has mission responsibility as assigned by AFSC for demonstration and acquisition of selected subsystems and systems in the intelligence, mapping, charting, command, control and communications areas.

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